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#### (57) Abstract

The simultaneous multi access reasoning technology system of the present invention utilizes both existing knowledge and implicit information that can be numerically extracted from training data to provide a method and apparatus for diagnosing disease and treating a patient. This technology further comprises a system for receiving patient data from another location, analyzing the data in a trained neural network, producing a diagnostic value, and optionally transmitting the diagnostic value to another location.

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# COMPUTER ASSISTED METHODS FOR DIAGNOSING DISEASES

#### Technical Field

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The present invention relates to methods for diagnosing, screening or prognosing diseases. More particularly, the present invention relates to a method for diagnosing, screening or prognosing diseases in humans or animals, and for determining the severity and cause of the disease.

The present invention further relates to a computer assisted method for diagnosing, screening or prognosing diseases, utilizing one or multiple neural networks to obtain a diagnostic index. In preferred embodiments of the present invention, the method is used to diagnose, and prognose diseases such as osteoporosis and cancers, including but not limited to ovarian, breast, testicular, colon and prostate cancer. In another preferred embodiment, the invention includes a system to receive patient data transmitted from data transmitting stations, to process these data through the trained neural networks to produce a diagnostic value or prognostic value, and to transmit these values to a remote data receiving means.

#### Background of the Invention

As used herein, the term "disease" is defined as a deviation from the normal structure or function of any part, organ or system of the body (or any combination thereof). A specific disease is manifested by characteristic symptoms and signs, including both chemical and physical changes. A disease is often associated with a variety of other factors including but not limited to demographic, environmental, employment, genetic and medically historical factors. Certain characteristic signs, symptoms, and related factors can be quantitated through a variety of methods to yield important diagnostic information. For purposes of this application, the quantifiable signs, symptoms and/or analytes in biological fluids characteristic of a particular disease are defined as "biomarkers" for the disease. Current diagnostic and prognostic methods depend on the identification and evaluation of these biomarkers, both

individually and as they relate to one another. Often the diagnosis of a particular disease involves the subjective analysis by a clinician, such as a physician, veterinarian, or other health care provider, of the data obtained from the measurement of the factors mentioned above in conjunction with a consideration of many of the traditionally less quantitative factors such as employment history. Unfortunately, this subjective process of diagnosing or prognosing a disease usually cannot accommodate all the potentially relevant factors and provide an accurate weighting of their contribution to a correct diagnosis or prognosis.

Generally, the pathological process involves gradual changes that become apparent only when overt change has occurred. In many instances, pathological changes involve subtle alterations in multiple biomarkers. It is uncommon that a single biomarker will be indicative of the presence or absence of a disease. It is the pattern of those biomarkers relative to one another and relative to a normal reference range, that is indicative of the presence of a disease. Additional factors including but not limited to demographic, environmental, employment, genetic and medically historical factors may contribute significantly to the diagnosis or prognosis of a disease, especially when considered in conjunction with patterns of biomarkers. Unfortunately, the subjective diagnostic process of considering the multiple factors associated with the cause or presence of a disease is somewhat imprecise and many factors that may contribute significantly are not afforded sufficient weight or considered at all.

When individual biomarkers do not show a predictable change and the patterns and interrelationships among the biomarkers viewed collectively are not clear, the accuracy of a physician's diagnosis is significantly reduced. Also, as the number of biomarkers and demographic variables relevant for the diagnosis of a particular disease increases, the number of relevant diagnostic patterns among these variables increases. This increasing complexity decreases the clinician's ability to recognize patterns and accurately diagnose or predict disease.

Prostate cancer affects numerous individuals each year and many of them are killed by the disease. The early and accurate diagnosis of prostate cancer has been very difficult to achieve with reliability and accuracy. However, early diagnosis of prostate cancer is essential to maximizing the possibility of successfully treating the disease. Current screening techniques include digital rectal examination (DRE), transurethral prostatic biopsy, and measurement of prostate specific antigen (PSA) in the blood. Reliance on serum PSA levels, especially low PSA levels, as a sole diagnostic measure of prostate cancer often provides unacceptable levels of inaccurate diagnosis. These screening techniques miss many cases of early stage prostate cancer

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resulting in growth of the cancer within the prostate gland and also outside the capsule of the gland. It is essential to diagnose this disease in the early stages, well before metastases have occurred.

In addition, diagnostic methods should be capable of distinguishing between benign prostatic hyperplasia (BPH) and prostate cancer and to distinguish between cases of cancer and non-cancer. What is also needed is a valid, reliable, sensitive and accurate technique that can diagnose or prognose prostate cancer at an early stage and also distinguish the various stages of prostate cancer which can be characterized as T1b, T2, T3 and TNxM1.

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Osteoporosis and osteopenia provide another example of disease with multiple biomarkers, the following biomarkers collectively show characteristic changes in the presence of osteoporosis: calcium, phosphate, estradiol (follicular, mid-cycle, luteal, or post-menopausal), progesterone (follicular, mid-cycle, luteal, mid-luteal, oral contraceptive, or over 60 years), alkaline phosphatase, percent liver-ALP, and total intestinal-ALP. After measuring these biomarkers, a diagnosing clinician would next compare the measurements to a normal reference range. While some of the biomarkers may fall outside the normal reference range, others may fall clearly within the normal reference range. In some circumstances, all of the biomarker values may fall within a normal reference range. Presented with such data, a clinician may suspect that a patient has undergone some bone loss, but will be unable to reach a conclusive and meaningful diagnosis as to the presence of the disease osteoporosis.

The characteristic changes in biomarkers associated with some diseases are well documented; however, the quantitative interpretation of each particular biomarker in diagnosing a disease and determining a prognosis is not well established. The difficulties inherent in formulating a diagnosis from the analysis of a set of laboratory data is best illustrated by looking closer at conventional diagnostic methods for a specific disease. A discussion of the disease osteoporosis follows.

The term "osteopenia" as used herein means any decrease in bone mass below the normal. The term "osteoporosis" as used herein means a specific form of generalized osteopenia characterized by a decrease in bone density, low bone mass, and microarchitectural deterioration of bone tissue.

Osteopenia encompasses a group of diseases with diverse etiologies typified by reduction in bone mass per unit volume to a level below that which is necessary for adequate mechanical support. Osteoporosis is the result of the gradual depletion of the inorganic portion of the skeleton and can be caused by any number of factors. Primary osteoporosis is an age related disorder that is particularly common in women

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and is characterized by decreased bone mass in the absence of other recognizable causes. However, osteoporosis occurs in both men and women. In women it is recognized usually at the 5th or 6th decade, following menopause. In men osteoporosis is often recognized around their 6th or 7th decade of life.

Several demographic parameters are associated with enhanced risk of developing osteoporosis. The following is a partial list of individuals whose demographics and behavior place them at risk for developing osteoporosis:

Post-menopausal women

Cigarette smokers

Heavy users of alcohol

Users of a variety of drugs, such as steroids

Female runners and ballet dancers

Male marathoners consuming too few calories

Bulemics and anorexics

People with poor diets

People allergic to dairy products

People affected with cancer

Fair and slim women

All men and women over the age of 65.

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In addition to being female, the three most significant risk factors are poor diet, lack of exercise, and being postmenopausal. Other risk factors which are associated with osteoporosis include racial factors such as Caucasian or Oriental ancestry, a fair complexion, and a family history of osteoporosis.

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The onset of osteoporosis may be insidious or sudden, following trauma. The most common complaint associated with osteoporosis is back pain. Eventually, the pain may spread to the pelvis, the thorax, and the shoulders. In the spine, the vertebrae can compress, and the back can take on a "bent" appearance. Conditions such as kyphosis (humpback) or scoliosis may occur. If the spine becomes deformed, other body parts can be affected as well. For example, the ribs can be pushed against the pelvis, or the stomach can be pushed into the pelvis. In addition to spinal problems, osteoporosis can also lead to fractures of the hip, wrist, and ribs. These fractures can occur with only slight trauma and sometimes with no trauma at all. Mazess B., et al., "Bone Density of the Radius, Spine, and Proximal Femur in Osteoporosis," J. of Bone and Mineral Research, Vol. 3, pgs. 13-18, (1988); Riggs B. L., et al., "Involutional Osteoporosis", New Engl. J. Med., Vol. 314, pgs. 1676-

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1686, (1986). The changes associated with osteoporosis are gradual so osteoporosis is often not detected in its early stages.

Calcium and phosphorus are the main components of the inorganic portion of the skeleton. Chemical analysis of blood may reveal calcium, phosphorus, and alkaline phosphatase within the normal range. However, an isoenzyme of alkaline phosphatase may be significantly increased. Increased bone resorption seen in osteoporotic patients, which occurs as a result of the action of osteoclasts, usually involves the dissolution of both minerals and organic matrix eventually leading to increased excretion of urinary hydroxyproline. Serum estradiol which is secreted almost entirely by the ovary is significantly decreased in these patients.

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An early decrease in bone mass can be measured by non-invasive assessment of the skeleton by four widely available methods that are known to those skilled in the art, including single photon absorptometry, dual photon absorptometry (DPA), dual-energy x-ray absorptometry (DXA), and quantitative computed tomography quantitative computed tomography (CAT scan). Several of these methods are used to measure mineral content in the bone, and some are relatively selective for certain bones or trabecular versus cortical bone. These methods also provide different levels of radiation exposure.

Magnetic resonance imaging (MRI) and positron emission tomographic (PET) techniques may also reveal information useful in the diagnosis of various diseases including osteopenia and osteoporosis by providing information concerning bone density and vitality.

Radiographic absorptometry (RA) is a method for non-invasive measurement of bone mineral x-rays of the hand. Radiographs, taken with a standard x-ray machine, are sent to a central laboratory for computer-controlled analysis.

Current standard diagnostic techniques, are not effective for early detection of osteoporosis. Changes seen in osteoporosis are very gradual, and often go undetected in the early stages of the disease. Osteoporosis is often not detected in its early stages because bone mass must be decreased by about 30% to 40% before it is apparent using standard x-ray diagnostic techniques. Preventing osteoporosis by detecting early bone loss is far better than identifying the disease at relatively advanced stages and subsequently attempting to prevent its progression. Once major deterioration has occurred and gaps exist between the ends of fractured trabecular, no current treatment can be expected to restore the lost bone. Thus, therapeutic efforts must be directed toward prevention and early recognition of the progressive disease so treatment can be instituted before essentially irreversible structural damage ensues. Cummings S.R., et

al., "Should Perimenopausal Women Be Screened for Osteoporosis?", Ann. Int. Med., Vol. 104, pgs. 817-823, (1986); Courpron P., "Bone Tissue Mechanisms Underlying Osteoporosis," Orthop. Clin. North Am., Vol. 12, pgs. 513-545, (1981); Frost H. M., "Mechanical Determinants of Bone Modeling," Metabol. Bone. Dis. Rel. Res., Vol. 4, pgs. 217-229, (1982). What is needed is a method for early detection and prediction of osteoporosis that considers the multiple biomarker and demographic variables associated with the disease.

One of the problems with the current methods for diagnosing osteoporosis is that the procedures do not give any information about the underlying cause of the osteoporosis, making it difficult to prescribe an appropriate course of treatment for the patient. For example, a common cause of postmenopausal osteoporosis is an estrogen deficit, which x-ray techniques cannot measure. Another problem inherent in the current diagnostic methods for osteopenia is that all of the current methods require expensive, sophisticated medical instrumentation to perform the bone density measurements. Additionally, patients must be exposed to x-rays. This makes a general screening of high risk populations impractical due to the expense and unavailability of the necessary instrumentation to the average clinic.

In view of the difficulties associated with extracting a diagnosis from the laboratory data for a set of predictive biomarkers, and also from demographic data optionally combined with biomarker data, there is need for automated diagnostic systems that are capable of complex pattern recognition. There have been several attempts at using computational models to achieve pattern recognition in diagnostics. One of the most popular computational methods for making diagnoses from multivariate laboratory data has been discriminate function analysis. However, diagnostic systems that rely exclusively on classical pattern recognition technology (geometric, syntactic, template, statistical) are not effective for evaluating the characteristic biomarker patterns of many disease states partially due to the inherent non-linear nature of the problem and a lack of known mathematical structure in the observed data. There is no clear set of rules that accurately describes how to analyze a set of biomarkers to reach a diagnosis.

In recent years, artificial neural networks have been gaining popularity as a means for recognizing and analyzing subtle diagnostic patterns in multivariate laboratory data. Neural networks possess the ability to discern patterns and trends too subtle or too complex for humans and conventional computational methods to identify. While humans can not easily assimilate more than two or three variables at once, neural networks can perceive correlations among hundreds of variables. Examples of

areas in which neural networks have been explored for their value in clinical diagnosis and/or prognosis include:

- psychiatry (See *Mulsant, B.H.*, "A Neural Network as an Approach to Clinical Diagnosis", *MD Computing*, Vol. 7, pp. 25-36 (1990));
- autism (See *Cohen, I., et al.*, "Diagnosing Autism: A Neural Net-Based Tool", PCAI, pp. 22-25 (May/June 1994);

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- pediatric radiology (See *Boone*, *J.M.*, et al., "Neural Networks in Radiologic Diagnosis. I. Introduction and Illustration", *Invest. Radiol.*, Vol. 25, pp. 1012-1016, (1990) and *Gross*, *G.W.*, et al., "Neural Networks in Radiologic Diagnosis. II. Interpretation of Neonatal Chest Radiographs", *Invest. Radiol.*, Vol. 25, pp. 1017-1023 (1990));
- breast cancer (See Astion, M.L., et al., "Application of Neural Networks to the Interpretation of Laboratory Data in Cancer Diagnosis", Clin. Chem., Vol. 38, No. 1, pp. 34-38 (1992); Yuzheng, W., et al., "Artificial Neural Networks in Mammography: Application to Decision Making in the Diagnosis of Breast Cancer", Radiology, Vol. 82, pp. 81-87 (1993); Kappen, H.J., et al., "Neural Network Analysis to Predict Treatment Outcome", Annals of Oncology, Vol. 4, Supp. 4, pp. S31-S34 (1993); and, Ravdin, P.M., et al., "A practical application of neural network analysis for predicting outcome of individual breast cancer patients", Breast Cancer Research and Treatment, Vol. 22, pp. 285-293 (1992));
- ovarian cancer (See Wilding, P., et. al., "Application of backpropagation neural networks to diagnosis of breast and ovarian cancer", Cancer Letters, Vol. 77, pp. 145-153 (1994));
- thyroid disease (See, Sharpe, P.K., et. al.; "Artifical Neural Networks in Diagnosis of Thyroid Function from in Vitro Laboratory Tests," Clin. Chem., Vol. 39, No. 11, pps. 2248-2253 (1993));
- prostate cancer (See *Snow*, *P.S. et al.*, "Artificial Neural Networks in the Diagnosis and Prognosis of Prostate Cancer: A Pilot Study" *J. Urology*, Vol. 152: 1923-1926 (1994));
  - cervical cancer (See U. S. Patent No. 4,965,725 to Rutenberg); and,
- cardiology (See U.S. Patent No. 5,280,792 to *Leong et al.* and *Furlong, J.W.*, "Neural Network of Serial Cardiac Enzyme Data: A Clinical Application of Artifical Machine Intelligence", *Clin. Chem.*, Vol. 96, No. 1, pp. 134-141 (July 1991).

Neural networks are capable of pattern recognition particularly suited to making diagnoses. Unlike current methods for arriving at a diagnosis from a logical

set of rules, neural networks do not require explicit encoding of process knowledge in a set of rules. Neural networks learn from examples. Neural networks learn more efficiently when the data to be input into the neural network is preprocessed.

There are two basic approaches in computer assisted clinical pattern classification techniques. The first approach applies known knowledge and facts (physiological, anatomical, molecular biological, etc.) of a given disease process and attempts to establish links between observed or measured data and one of several possible classification classes. Such existing knowledge and facts are often expressed as rules (e.g. clinical expert systems), certain forms of numerical functions (e.g. statistical distributions in parametric statistical inferences), or even complex models that can only be described with systems of equations (e.g. pharmacokinetic models).

The second approach uses numerical procedures to adaptively construct and modify a numerical classification system based on available training data which are essentially sets of input values paired with known classification results. In this approach, the human expert knowledge is not or can not be expressed in an explicit form. Instead, the knowledge is implicitly provided in the training data with confirmed classifications. The extraction of such knowledge through supervised learning (learning from examples) and the adaptive construction of the classification system are left entirely to the learning algorithm. Classification systems with this second approach include various forms of neural network classifiers such as Multilayer Feedforward Perceptrons.

Both approaches have their shortcomings. The first approach uses explicit knowledge in the subject area to associate observed unknown data with a known class. However, in many practical situations, such knowledge is incomplete, or a portion of it cannot be expressed in explicit and precise terms, so that it can be directly coded into the classification system. On the other hand, the pure numerical pattern classification approach places the burden of constructing the classification system entirely to the adaptive learning process. The performance of the obtained system is limited to the amount and extent of information contained in the training data and the effectiveness of the learning algorithm in extracting such information, despite the fact that there may exist a tremendous amount of prior knowledge about the subject area. In some cases where there is no preprocessing such as preselection or scaling of the patient data, the training of a neural network may be extremely difficult if not impossible since the number of input variables may be too large and the relationship of these variables to a specific disease may be too weak to achieve the desired predictive accuracy.

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Accordingly what is needed is an approach to diagnosing and prognosing disease incorporates an apparatus and a system capable of accommodating a large number of factors, such as biomarker and demographic factors. This system should be capable of processing a large number of patients and patient variables such as biomarker and demographic factors. This approach to diagnosis and prognosis of disease should select factors with high predictive values, preprocess these factors, and input the data into a computer-based neural network or multiple neural networks in order to train the neural network(s) to predict or diagnose disease. These neural network(s) should produce a diagnostic index comprised of one or several output values indicative of the presence (diagnosis) or future occurrence (prognosis) of a disease. The system should possess the capacity to input patient data into the trained neural network and produce an output value to indicate if the patient has or will have the disease.

Furthermore, since clinicians will rarely have such computer-based neural network capabilities at their disposal, what is also needed is a system whereby patient data can be transmitted to a computer-based neural network as described above, which will receive the data, input it into the trained neural network, produce an output value indicative of a diagnosis or prognosis and then transmit the information concerning the diagnosis or prognosis to another location, such as the originating data transmitting station, or perhaps directly to the clinician's office. Such a system would provide access to sophisticated and highly trained prognostic and diagnostic neural networks which would enhance the accuracy of clinician's diagnostic and prognostic capability. This system should be capable of receiving high volumes of patient data and rapidly processing the data through the neural networks to obtain diagnoses and prognoses of disease.

Such a system could be used for diagnosis and prognosis of any disease or condition for which a neural network may be specifically trained.

#### Summary of the Invention

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The present invention is an apparatus and a process for diagnosing, screening or prognosing diseases. More particularly, the present invention relates to a computer-based method employing trained neural networks, and a process for diagnosing, screening or prognosing diseases in patients such as humans or animals, and for determining the severity and cause of the disease. This objective is accomplished by performing the following steps: collecting data about patients, such types of data optionally including biological, physical, demographic, racial, environmental, and

medical historical data; selecting those data that are associated with the diagnosis of a disease; digitizing the data; scaling these digitized values; performing tests to analyze the discriminating power of these data; grouping individual data values; preprocessing these data to make preprocessed values; inputting selected data into a computer-based neural network in order to train the neural network; analyzing the contributions of individual data inputs to the neural network; selecting the optimally trained neural network based on performance, accuracy and cost, the neural network being trained to produce a diagnostic index; and inputting other patient data into the trained neural network to produce an output value which indicates whether the patient may have or be susceptible to the disease.

The present invention also includes an apparatus and process for rapidly diagnosing, screening or prognosing diseases in large numbers of patients, wherein the patient data is transmitted to a central facility from a remote location. At the central facility, patient data is received and introduced into a computer system which performs the following functions: analysis of the patient data to evaluate correctness of the data format; scaling the data to provide values for different types of in similar ranges; introduction of scaled patient data into a trained neural network for computation of an output value; comparison of the output value to a diagnostic index produced by the trained neural network; formulation of a diagnosis or prognosis based on this comparison; transmission of the diagnosis or prognosis to a remote location, optionally the location which sent the original patient data set or the office of a health care provider.

This embodiment of the present invention permits the rapid evaluation of large data sets comprised of patient data including biomarker data and demographic data, formulation of a diagnosis or prognosis for a particular disease or for several diseases, and rapid transmission of the results to the health care provider or facility responsible for the patient. This system not only provides improved diagnostic capability resulting in enhanced health to the patient, but also reduces cost due to wasted time, delayed treatment and incorrect diagnosis. This system provides the capability to screen numerous patient samples for diagnosis and prognosis of disease and enables health care providers to access sophisticated computer-based neural networks specifically trained to diagnose disease with high levels of precision and accuracy.

In one embodiment, the present invention may be used to rapidly and accurately diagnose and prognose prostate cancer, even at very early stages. In this embodiment, large numbers of patient data sets comprised of biomarkers and optionally demographic data, may be screened rapidly and economically to diagnose

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and predict prostate cancer with high precision and accuracy. In addition, this invention facilitates determination of the stage of prostate cancer and distinguishes between benign prostatic hyperplasia and prostate cancer.

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In another embodiment, the present invention may be used to rapidly and accurately diagnose and prognose osteoporosis and osteopenia, even at very early stages. In this embodiment, large numbers of patient data sets comprised of biomarkers and optionally demographic data, may be screened rapidly and economically to diagnose and predict osteoporosis and osteopenia with high precision and accuracy. In addition, this invention facilitates determination of the extent of osteoporosis and osteopenia and provides information about the causative variables.

It is an object of this invention to diagnose and prognose any disease in a patient for which adequate data, such as biomarker and demographic data, exist in a patient population to specifically train a neural network to produce a diagnostic index with a high level of predictive utility, and to accurately and reliably diagnose the disease in new sets of patient data. Large numbers of multivariable patient data sets may be screened for the presence of a disease or to prognose a disease using this system.

Accordingly, it is an object of the present invention to provide a method for diagnosing, screening or prognosing and determining the severity of a disease.

Still another object of the present invention is to provide a system comprised of a method and apparatus comprising a computer-based trained neural network system that will diagnose, screen or prognose and determine the severity of a disease by receiving patient data from another location through a data receiving means, transmitting the data into a computer or through several computers containing a computer-based trained neural network, processing the patient data through the trained neural network, or optionally multiple trained neural networks, to produce an output value, which is a diagnostic value, transmitting these diagnostic values to another location, optionally to another computer for transmission to a remote location, optionally comprising a computer, or other data receiving means. This system may contain one or several computers and one or several trained neural networks.

It is another object of the present invention is to provide an apparatus for diagnosing, screening or prognosing and determining the severity of a disease.

A feature of the present invention is that it provides a method for screening, prognosing and diagnosing prostate cancer.

Another feature of the present invention is that it provides a method for screening, prognosing and diagnosing osteoporosis and osteopenia.

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Still another feature of the present invention is that it provides a method for screening, prognosing and diagnosing breast cancer.

Yet another feature of the present invention is that it provides a method for screening and diagnosing ovarian cancer.

Another feature of the present invention is that it provides a method for screening, prognosing and diagnosing colon cancer.

An additional feature of the present invention is that it provides method for screening, prognosing and diagnosing testicular cancer.

An advantage of the present invention is that it provides a method for diagnosing disease which will provide a better understanding of the probable cause of the disease.

Another advantage of the present invention is that it provides a method for diagnosing cancer which will provide a better understanding of the probable cause of the cancer.

Another advantage of the present invention is that it provides a diagnostic test for cancer which can be used to rapidly and economically screen data sets from large numbers of patients.

Still another advantage of the present invention is that it provides a test for osteoporosis which will also give information as to the underlying cause of the osteopenic condition.

Another advantage of the present invention is that it provides a diagnostic test for osteoporosis which can be used to screen large numbers of individuals.

An advantage of the present invention is to provide a method for diagnosing osteoporosis and determining the underlying cause of the osteopenia without having to subject the patient to radiation.

These and other objects, features and advantages of the present invention will become apparent after a review of the following detailed description of the disclosed embodiment and the appended claims.

#### Brief Description of the Figures

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- Fig. 1 illustrates a feed forward neural network having multiple outputs.
- Fig. 2 illustrates a feed forward neural network having a single output.
- Fig. 3 is an equation illustrating the mathematical relationship between the input and output of a typical neuron.
- Fig. 4 is a schematic illustration of the second preferred embodiment of the present invention.

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Fig. 5 shows the training data used to construct the prostate cancer neural network prognostic system.

- Fig. 6 shows the training data used to construct the neural network ProstAsure<sup>TM</sup> system for prostate cancer detection.
- Fig. 7 shows the test data used to construct the neural network ProstAsure™ system for prostate cancer detection.
- Fig. 8 shows the training data used to construct the QuiOs<sup>™</sup> osteoporosis neural network diagnostic system.
- Fig. 9 shows the testing data used to test the QuiOs™osteoporosis neural network diagnostic system.
- Fig. 10 demonstrates the sensitivity and specificity of the QuiOs™ system in diagnosing osteopenia.
- Fig. 11 is a scatterplot of 726 test samples showing that QuiOs™ values correlate with bone mineral density (BMD) measurements at L2-L4 and Ward's triangle in the form of T-scores.
- Fig. 12 is a schematic representation of the simultaneous multi access reasoning technology.
- Fig. 13 provides an schematic representation of an approach for the construction and training of a computer-based neural network based classifier for the diagnosis and prognosis of disease
  - Fig. 14 shows a configuration of a neural network based diagnostic system
- Fig. 15 is a schematic overview of the ProstAsure™ computer-based neural network system architecture for receiving patient data, analyzing the patient data with a trained neural network and transmitting results.
- Fig. 16 is the system architecture for analyzing patient data input and computation of ProstAsure™ diagnostic values.
- Fig. 17 provides ProstAsure™ reference ranges for normal, BPH and prostate cancer in different age groups.
- Fig. 18 provides diagnostic guidelines for samples in the ProstAsure™ test data set.
- Fig. 19 shows statistically significant ProstAsure™ results in the diagnosis normal, BPH and cancer patients.
  - Fig. 20 demonstrates ProstAsure<sup>TM</sup> results in 193 test cancer cases.
- Fig. 21 is a scatterplot of ProstAsure™ values vs. PSA values in 416 test samples. By non-linearly combining multiple biomarkers, ProstAsure™ effectively separates normal, BPH and cancer patients better than using a single biomarker (PSA).

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Fig. 22 shows receiver-operating characteristic (ROC) curves comparing the diagnostic power of ProstAsure<sup>TM</sup> and PSA alone. The area under the curve is a measure of the usefulness of the test. The Rel.ProstAsure refers to normalization with age-specific reference ranges. ProstAsure<sup>TM</sup> significantly outperforms PSA with statistical significance in separating cancer from normal and BPH.

- Fig. 23 demonstrates ProstAsure™ sensitivities and specificities computed with training and test data.
- Fig. 24 shows the sensitivity and specificity of ProstAsure™ in detecting and discriminating prostate cancer and identifying normal and BPH patients.
  - Fig. 25 is a mathmetical description of the ProstAsure™ algorithm.
  - Fig. 26 is a mathematical description of the QuiOs™ algorithm.

#### **Detailed Description**

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The following patent applications are incorporated herein by reference in their entirety: U.S. Provisional Application Serial Number 60/001,425 filed July 25, 1995; U.S. Application Serial Number 08/472,632 filed June 7, 1995; PCT Application PCT/US95/01379 filed February 2, 1995; U.S. Application Serial Number 08/323,446 filed on October 13, 1994; U.S. Application Serial Number 08/315,851 filed on September 30, 1994; U.S. Application Serial Number 07/990,772 filed on December 14, 1992; PCT Application PCT/US92/10879 filed December 14, 1992; U.S. Application Serial Number 07/964,486 filed on October 21, 1992; U.S. Application Serial Number 07/806,980 filed on December 12, 1991.

As used herein, the term "disease" is defined as a deviation from the normal structure or function of any part, organ or system of the body (or any combination thereof). A specific disease is manifested by characteristic symptoms and signs, including biological, chemical and physical changes and is often associated with a variety of other factors including but not limited to demographic, environmental, employment, genetic and medically historical factors. Certain characteristic signs, symptoms, and related factors can be quantitated through a variety of methods to yield important diagnostic information.

The term "patient" refers to any human or animal.

For purposes of this application, the quantifiable signs, symptoms and/or analytes in biological fluids and tissues characteristic of a particular disease are defined as "biomarkers" for the disease. Current diagnostic and prognostic methods depend on the identification and evaluation of these biomarkers, both individually and as they

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relate to one another. The term "biomarkers" includes all types of biological data from a patient.

The patient data may include a variety of types of data which have some association with the disease. The information may be biological. Such data may be derived from measurement of any biological parameter. Such substances include, but are not limited to, endocrine substances such as hormones, exocrine substances such as enzymes, and neurotransmitters, electrolytes, proteins, carbohydrates, growth factors, cytokines, monokines, fatty acids, triglycerides, and cholesterol.

Other types of biological data may be derived from histological analysis of organs, tissues or cells removed from patients, including histological analyses performed at the light microscopic and electron microscopic levels utilizing any number of techniques including, but not limited to, structural analysis, histochemical, immunocytochemical, in situ hybridization, and autoradiographic techniques.

Biological data may be derived from analysis of cells removed from patients and grown in culture. Various characteristics of these cells may be examined histologically and biochemically. For example, cells removed from a patient and placed in culture may be examined for the presence of specific markers associated with the presence of a disease. Cells may be examined for their metabolic activity or for the products made and released into the culture medium.

Biological data about a patient includes results from genetic and molecular biological analysis of the nuclear and cytoplasmic molecules associated with transcription and translation such as various forms of ribonucleic acid, deoxyribonucleic acid and other transcription factors, and the end product molecules resulting from the translation of such ribonucleic acid molecules..

Also included in the category of biological data are the various structural and anatomical analytical methods used with patients such as radiographs, mammograms, fluorographs and tomographs, including but not limited to X-ray, magnetic resonance imaging, computerized assisted tomography, visualization of radiopaque materials introduced into the body, positron emission tomography, endoscopy, sonograms, echocardiograms, and improvements thereof.

Biological data also includes data concerning the age, height, growth rate, dental health, cardiovascular status, reproductive status (pre-pubertal, pubertal, post-pubertal, pre-menopausal, menopausal, post-menopausal, fertile, infertile), body fat percentage, and body fat distribution. Biological data also includes the results of physical examinations, including but not limited to manual palpation, digital rectal examination, prostate palpation, testicular palpation, weight, body fat amount and

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distribution, auscultation, testing of reflexes, blood pressure measurements, heart and related cardiovascular sounds, vaginal and other gynecologic examinations, including cervical, uterine and ovarian palpation, evaluation of the uterine tubes, breast examinations, and radiograpic and infrared examination of the breasts.

Additional biological data can be obtained in the form of a medical history of the patient. Such data includes, but is not limited to the following: medical history of ancestors including grandparents and parents, siblings, and descendants, their medical problems, genetic histories, psychological profiles, psychiatric disease, age at death and cause of death; prior diseases and conditions; prior surgeries; prior angioplasties, vaccinations; habits such as exercise schedules, alcohol consumption, cigarette consumption and drug consumption; cardiac information including but not limited to blood pressure, pulse, electrocardiogram, echocardiogram, coronary arteriogram, treadmill stress tests, thallium stress tests and other cardiovascular imaging techniques. All of the aforementioned types of biological data are considered as "biomarkers" for the purposes of the present application.

The term "biological fluid" includes, but is not limited to, blood, serum, cerebrospinal, peritoneal, salivary, lacrimal, peritoneal, reproductive, intraocular, digestive, respiratory, pleural, pericardial, lymphatic, urine, intracellular and extracellular fluids, and neural fluids.

The term "demographic data" includes information concerning the patient's race, species, sex, ethnicity, environment, exposure to environmental toxins and radiation, stress level, behavioral patterns, previous occupations and current occupation. Demographic data may also be used to provide patient information that is useful in the diagnosis and prognosis of disease.

The present invention provides a method for diagnosing, screening or prognosing a disease in a patient comprising the steps of measuring the concentrations of a predetermined set of biomarkers known to be associated with the disease; converting these concentrations to digitized values; preprocessing the digitized values to make preprocessed values; and sending the preprocessed values to a computer-based neural network in order to train the neural network to diagnose or prognose the disease, whereby the diagnostic index from the neural network indicates when the patient has the disease or may develop the disease.

The present invention also comprises an apparatus for diagnosing, screening or prognosing a disease in a patient comprising a means for digitizing the concentrations of a predetermined set of biomarkers known to be associated with the disease from the patient; a means for preprocessing the digitized values; and a computer-based trained

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neural network coupled to the digitizing and scaling means for generating network output values; means for comparing the output values from the neural network to the diagnostic index to produce a diagnostic value which indicates when the patient has the disease or may develop the disease.

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In accordance with the first embodiment of the present invention, a trained neural network is utilized to determine a diagnostic index corresponding to the presence and severity of a disease by analyzing a set of predetermined biomarkers or demographic data for that disease. In accordance with the invention, the concentrations of certain biomarkers or demographic data related to the incidence of a particular disease are determined for a patient. These data are converted to digitized values. These digitized values are then preprocessed (scaling, truncation, linear/nonlinear combination, etc.) and the preprocessed values, optionally together with one or several secondary values computed from the original values are then sent to a trained neural network to yield a diagnostic index. Preprocessing of the data occurs at this stage and serves to decrease the burden on the neural network and enhance the accuracy and sensitivity of the neural network for diagnosis and prognosis of disease. A neural network is trained by introducing a population of patients in which a disease state is known, along with the biomarker values or demographic data for those patients and "teaching" the neural network to recognize the patterns in the biomarkers. After the neural network is trained, biomarker values from patients with unknown disease states are introduced to the trained neural network. The neural network then processes the information to produce an output value whereby the output values from the neural network are diagnostic values which indicate whether the patient has the disease or may develop the disease

Although not wanting to be bound by this statement, the inventors propose that the artificial neural network, especially the multi-layer feedforward network, may, through their weight connections, correspond to data patterns that are important for categorizing diseases. Additionally, the neural network can identify unique patterns of data associated with a variety of disorders that may help to classify borderline cases that do not appear to fit into either a malignant or benign pattern.

#### Multiple Neural Networks

The present invention also comprises a method for diagnosing, screening or prognosing a disease in a patient comprising the steps of measuring the concentrations of a predetermined set of biomarkers known to be associated with the disease from the patient, digitizing the concentrations, preprocessing the digitized values to make

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preprocessed values, scaling the digitized values of the analytes, and introducing the preprocessed values to a first trained neural network, and sending the output value from the first neural network and a second set of predetermined biomarkers, which could include one or more of the biomarkers in the first set of predetermined biomarkers, to a second trained neural network, whereby the output values from the second neural network are compared to the diagnostic index to produce a diagnostic value which indicates when the patient has the disease or may develop the disease

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A second embodiment of the present invention involves a two step analysis of the biomarkers by neural network. This avoids the bias created by a dominant predictive variable when training a network. The dominant biomarker or predictive variable is excluded from the first analysis by neural network and is then included in a second analysis by neural network. For example, if age is thought to be the dominant predictive variable in the diagnosis of osteoporosis, that variable is not included in the training of the first neural network, and the training data set is limited to the other selected biomarkers. After obtaining a diagnostic index using the first set of biomarkers, a second neural network is trained using the diagnostic index and the entire set of input variables, including age, to yield another diagnostic index. The final diagnostic index is a composition of an artificial neural network generated index and results from heuristic analysis using other non-numerical patient information.

In another embodiment, the present invention provides a system, including the ProstAsure™ system, comprising an apparatus and method for diagnosing, screening or prognosing prostate cancer in patients. In this embodiment, data obtained from analysis of biomarkers and optionally from demographic information is preprocessed (e.g. scaled) and input into a trained neural network. Prostate specific antigen (PSA), prostatic acid phosphatase (PAP), and three forms of creatine kinase (BB, MB, and MM) are used as the biomarkers in this invention. It is to be understood that other biomarkers and demographic data may be used in this invention. For example, the results of a digital rectal examination in which the prostate is palpated may optionally be combined with other biomarkers or demographic data. The trained neural network provides an output value which indicates whether the patient has prostate cancer. The trained neural network is capable of providing highly accurate diagnoses and prognoses at early stages in the progression of prostate cancer, thereby displaying a high degree of sensitivity and specificity. The stage of prostate cancer is determined, even at very early stages in the disease. In addition, this invention distinguishes benign prostatic hyperplasia from prostate cancer, and distinguishes prostate cancer from non-cancerous conditions.

Another specific embodiment of the present invention includes a system comprising a method and apparatus for diagnosing and determining the severity and underlying cause of osteopenia and osteoporosis in a patient using a computer-based trained neural network. In a preferred embodiment, the method comprises determining the serum level of the following biomarkers: calcium, phosphate, total alkaline phosphatase, an alkaline phosphatase isoenzyme, estradiol, and progesterone. The alkaline phosphatase isoenzyme is preferably t-lymphocyte derived alkaline phosphatase or blood, liver or intestinal alkaline phosphatase isoenzyme. Optionally, the age of the patient or demographic data may be included in the trained neural network. The bone density coefficient that is calculated by the algorithm correlates to a very high degree to bone density as measured by standard methods, such as radiographic absorptometry, quantitative computed tomography, dual photon absorptometry and direct measurement of bone density. The bone density coefficient that is measured is then compared to an osteopenic severity scale.

Another embodiment of the present invention is directed to a computer assisted method for screening, prognosing and diagnosing diseases utilizing a neural network to obtain a conclusive diagnosis. The present invention can be adapted to existing diagnostic devices that have a collection means, a sample detecting means capable of detecting the quantity of an analyte in a biological fluid and a means of either printing or displaying the results of the tests on video display means.

The inventors have discovered that biomarkers collectively alter in response to a disease process, and collectively constitute a new diagnostic biomarker with better disease predictability than the individual biomarkers. When the biomarkers are processed and analyzed as a group in a computer-based trained neural network to yield a single diagnostic index, the sensitivity and specificity of the diagnosis is increased, making it possible for a physician to detect the presence of a disease earlier and with greater precision, or estimate a prognosis with greater precision, than by analysis of the individual biomarkers.

In accordance with one embodiment of the present invention, a biological fluid or several biological fluids are first collected from a patient. Biomarkers associated with a specific disease are measured in the biological fluids using standard laboratory techniques, to determine their concentrations, or in some cases their presence or absence. It is to be understood that this process can be carried out automatically in conventional diagnostic machines. For purposes of illustration, descriptions of the methods for obtaining the values for the biomarkers for osteopenia and also for prostate cancer are provided elsewhere in this section.

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The biomarkers relied upon to diagnose a disease by the method of the present invention must be predictive of the suspected disease and must be statistically significant for analysis by a neural network. The selection of biomarkers that offers statistically significant discriminating power in the diagnosis of disease involves several steps. First an inventory of biomarkers that have shown certain relevancy in the diagnosis of the disease of interest must be conducted. In general, only the biomarkers that reflect different aspects of the disease process or other diagnostic information need to be included. Second, the selected biomarkers need to have a reasonable diagnostic value in terms of sensitivity, specificity, and positive and negative predictive powers. The design and implementation of experimental protocol from which the biomarkers are developed and evaluated should also be considered. Third, if the number of candidate biomarkers is large, a formal discriminating power analysis may be conducted. However, many of the standard statistical analysis methods may not be adequate for highly nonlinear classification problems. Typically, biomarker values and demographic data values are scaled to provide relatively similar ranges of values between different biomarkers or demographic variables. In this manner, the variances due to the different numerical ranges inherent in the measurement of different variables are decreased. Preprocessing of the input variables comprised of biomarkers and other demographic data is an important step in the training of the neural network. If the number of candidates are not too large, they may be all included in the initial attempt of neural network training. If one or several of the input biomarkers to the network are irrelevant to the classification decision making process, it will be reflected in the network connection weights of the trained neural networks. These values may then be removed from the biomarker set for a particular disease. Other methods for evaluating the statistical significance of a biomarker selected for analysis by neural network and selecting biomarkers for training a neural network are well known in the art.

Biomarkers which meet the criteria delineated above, namely, they are predictive of a particular disease and statistically significant for analysis by neural network, are identified below for several examples of diseases including prostate cancer, osteoporosis, ovarian cancer, colon cancer, breast cancer, and testicular cancer. It is to be understood that these biomarkers for the specific diseases described below are examples of the present invention and are not to be construed as imposing any limitation on the scope of the present invention.

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Ovarian Cancer I	Prostate Cancer I	Colon Cancer
LASA-P®	LASA-P®	LASA-P®
CA125	PAP	CA 19-9
DM/70K	PSA	CEA

Ovarian Cancer II	Prostate Cancer II
CA125	PAP
MCSF	PSA
OVX1	CK-MB
LASA	CK-MM
CA7-24	CK-BB
CA19-9	

Breast Cancer	Testicular Cancer	Osteoporosis
LASA-P®	LASA-P®	Calcium
CEA	AFP	Phosphate
HER2/neu in Plasma	HCG-Beta	Estradiol
	CA 15-3®	Progesterone
		ALP
		ALP Isoenzyme 1
		ALP Isoenzyme 2

A key to the abbreviations used above is provided below:

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AFP:	Alpha-Fetoprotein
CA125:	Cancer Antigen 125
CA 15-3®**	Breast Antigens 115D8/DF3
CA 19-9:	Carbohydrate Antigen 19-9
CEA:	Carcinoembryonic Antigen
CK-MM	Creatine kinase, MM subfraction
CK-MB	Creatine kinase, MB subfraction
CK-BB:	Creatine kinase, BB subfraction
DM/70K:	Ovarian marker NB/70K
HCG-Beta:	Human Chorionic Gonadotropin, Beta Sub- Unit
Plasma:	c-erb B-2 (HER2/neu) oncoprotein in plasma
LASA-P®*:	Lipid-Associated Sialic Acid in Plasma
M-CSF	Macrophage colony-stimulating factor
PAP:	Prostatic Acid Phosphatase
PSA:	Prostate Specific Antigen

- \*LASA-P is a registered trademark of DIANON Systems, Inc.
- \*\*CA 15-3 is a registered trademark of Centocor, Inc.

A large number of diseases may be diagnosed in accordance with the method of the present invention. To be suitable for diagnosis by the present method,

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biomarkers and demographic data for the disease must be quantifiable. The biomarkers and demographic data must also be predictive of the disease and must be statistically significant relative to one another. The method of the present invention is equally suited to the diagnosis of any disease in which biomarkers and demographic data can be identified, including but not limited to infectious diseases, and genetic abnormalities.

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After determining the biomarkers for a disease, the biomarker values are digitized, preprocessed and analyzed by a computer-based, trained neural network to yield a single diagnostic value. The most common neural network architecture for pattern classification problems is the feedforward network, which typically consists of an input layer, one or more hidden layers, and an output layer. Figs. 1 and 2 illustrate the arrangement of neurons in two different feedforward networks.

The elements that make up each layer of a neural network are referred to as neurons or nodes. Inputs are fed forward from the input layer to the hidden layers and then to the output layer. The number of neurons in each layer is determined before the network is trained. Typically, there is one input neuron or node for each input variable, and one output node for each output. The inputs to the neural network are predictor variables. These predictor variables can be quantitative or qualitative. Neural networks make no data distribution assumptions and can simultaneously use both quantitative and qualitative inputs. In the present invention, the biomarker values, and the optionally generated secondary values are rescaled during preprocessing to values between 0.0 and 1.0 or between -1.0 and 1.0, constitute the input variables.

The outputs of the network represent output categories. For example, a malignancy may be represented by maximal output of the malignant output neuron and silence of the benign neuron, whereas a benign process is represented by maximal output of the benign neuron and silence of the malignant neuron. A simple arithmetic function combines of the two neurons to yield a single diagnostic index. In the alternative, a single output neuron may be used. An output of greater than 0.5 would indicate a malignancy and an output of less than 0.5 would indicate a benign condition. In this way a diagnostic index is directly obtained. Alternatively, a reversed denotation could be used.

The number of hidden layers and the number of nodes in the hidden layers are configurable parameters that have a significant influence on the performance of the network. In practice, the optimal number of hidden neurons is determined empirically.

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The means for determining the optimum numbers of hidden neurons is well known to those skilled in the art and depends on the complexity of the problem being solved.

In the present invention, one embodiment of the neural network is a multi-layer feedforward perceptron using a backpropogation training algorithm. The number of hidden layers and the number of neurons in each hidden layer was determined to adequately match the level of complexity of the diagnostic problem. With the assumption that the samples in the training set are representative of all possible situations encountered in real applications with no significant contradictions, and the number and stratification of samples in the generalization and cross-validation test are statistically adequate, the criteria outlined below are used to determine if a chosen network configuration is appropriate.

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If the network continues to fail to correctly classify large portions of the samples in the training set, even after many adjustments of training algorithm parameters, the network complexity should be increased.

On the other hand, if the network achieves a high rate of correctly classifying the training set but fails to accurately classify a large number of samples in the testing set, network structure is probably too complex for the problem being solved, i.e. it has sufficient inherent flexibility to fit the training data set, but not sufficient predictive power to classify the test data set. If this is the case, the number of neurons in the hidden layers should gradually be reduced, or, if there are multiple hidden layers, the hidden layers should be gradually reduced.

It is also possible to achieve generalization with a neural network of slightly too many hidden neurons. This is done by periodically testing a partially trained neural network with cross-validation test data during training, and stopping at the moment when the cross-validation error reaches a minumum value and starts to increase.

It is usually not always necessary to have a large training sample set. If the samples in a training set have already represented all possible cases with adequate statistical significance, the addition of new samples generally does not increase the amount of information in the training samples. Instead it may decrease the useful information to noise ratio in the samples. At the other extreme, too small a training set will generally not be able to cover all possible variations in the population. The resultant network often simply memorizes all the cases in the training set and does not generalize at all.

The input and output layers are not directly connected. Every input neuron is connected to every neuron in the following hidden layer and neuron in a hidden layer

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is connected to every neuron in the following adjacent hidden layer or output layer, depending on the number of hidden layers. Each of the multiple connections to a particular neuron is weighted. In the hidden and output layers, each node sums the input activations, multiplied by the respective connection weights plus a bias term. The weighted sum then passes through a non-linear output function, typically a sigmoidal function, which gives the network the ability to represent complex non-linear relationships. A neuron fires if the sum of the weighted inputs to it are greater than a threshold value. As illustrated in Fig. 3, once a neuron is above a threshold, the magnitude of its output is a sigmoid function of the net input. The end result of activity in the neural network is the net output, a complex nonlinear function of the inputs.

In summary and in accordance with the present invention, first the values of the biomarkers or demographic variables for a specific disease are determined and scaled. The biomarkers are fed forward from the input layer to the hidden layer (or layers) and then to the output layer of the neural network. The number of neurons in the input layer is determined before the network is trained and corresponds to the number of biomarkers predictive for a specific disease. The biomarkers are preselected and biomarker values are preprocessed. There is one input neuron for each diagnostic variable or biomarker, and one output neuron for each desired output. Other than the identified biomarkers, diagnostic variables may include demographic information. The number of neurons in the output layer depends on the type of output desired. The number of neurons in the hidden layer is determined empirically during training.

The neural network used for diagnosing a specific disease must be trained to do so. In accordance with the present invention in one embodiment, the neural network is trained by back propagation. Back propagation refers to the technique of training a neural network to accurately model a set of input and output examples by determining the best connection weights between the values, and is well known in the art. Other techniques which may be used to train a neural network for purposes of this invention may include any other non-linear global optimization technique, such as the genetic search algorithm; however, the feed forward, back propagation network is most popular.

At the initial stages of training the neural network, the connection weights in the network are randomized. The training data is then presented to the network one datum at a time. In accordance with the present invention, the training data consists of the biomarker values or demographic values for a group of patients, and the diagnosis

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for each of those patients. The biomarker values, and, optionally, demographic values, are digitized and preprocessed and the preprocessed values are the input variables used to train the network. For each patient, the network uses the patient's preprocessed values to estimate a diagnosis, which is then compared to the actual diagnosis. If the network's diagnosis is correct, then the connection strengths and thresholds within the network are not changed, and the next patient is presented to the network. If the estimate of the diagnosis is not correct, the connection weights and thresholds in both the hidden layer and the output layer are adjusted to reduce the size of the classification error. After adjustments are made, the next patient is presented. Training proceeds until all patients in the training group are correctly classified or some preset stopping criteria are satisified (e.g. a maximum number of iterations).

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When training the neural network, the trainer may set the decision limits regarding the definition of a classification error, i.e. an incorrect diagnosis. The relevant parameter is the error tolerance, which specifies how close the estimated output has to be to the actual output to be correct. For example, if two output neurons are used and the training tolerance is set at 5%, the estimate of malignancy is considered correct if the malignant output neuron fires at 95% of maximum and the benign neuron fires at 5% of maximum. Similarly, a correct estimate of a benign diagnosis means that the benign output neuron first at 95% of maximum, while the malignant neuron fires at 5% of maximum. The methods for determining a classification error are well known to those skilled in the art.

In a preferred embodiment of this invention, if a single output neuron is used, a benign normal diagnosis is set at an output of 0.1 and a malignant or abnormal diagnosis is set at an output of 0.9. Alternatively the reversed denotation can be used. Error tolerance is an adjustable parameter and is significant in determining the success of the network at making an accurate diagnosis.

After the neural network is trained for the desired disease, biomarker values and optionally demographic values from patients with unknown disease conditions and possibly no disease are digitized, preprocessed and introduced to the trained neural network. The neural network then processes the information to produce a value corresponding to a diagnosis of the presence or absence of the particular disease. In accordance with the present invention, this is accomplished by using either one single output neuron or multiple output neurons. If more than one output neuron are used, the output from the neurons are combined to generate a single diagnostic index.

As illustrated by Fig. 4, in a second embodiment of the present invention, the diagnostic value obtained by analysis of the biomarkers by a trained neural network is

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further analyzed by a set of heuristic rules in combination with additional patient information. The additional patient information includes things such as family medical history and demographic information. This data is then processed to yield a second single diagnostic value.

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In another embodiment, the simultaneous, multi-access reasoning technology system of the present invention utilizes both existing knowledge and implicit information that can only be numerically extracted from training data. Use of existing knowledge may be in the form of setting normal reference ranges of biomarkers specific to the patient being diagnosed. The system has four major functional blocks as described in Figure 20:

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1. Input Data Preprocessing In this block, the observed data values of individual subjects go through sequences of transformations and combinations. The purpose of this procedure is to convert the raw input data into a form that preserves useful information in the most explicit form while eliminating much of the irrelevant "noisy" data. In addition, secondary input variables may be generated using the original inputs. The transformations, which are often nonlinear in nature, can also help to lessen the stress on the adaptive learning and classification block.

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2. Mechanistic (Realistic) Modeling and Simulation: In this block, available knowledge and information about a particular disease process are used to establish mechanistic (realistic) models of some of the normal processes (physiological, anatomical, pharmacological, pathological, molecular biological, genetic, etc.) that are relevant to the origination of measured patient data including categories and variables such as but not limited to the following:

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**Electrical Diagnostic Methods** 

EEG EKG EMG

Tomographs

Nerve Conduction Tests

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Imaging Diagnostic Methods X-ray

NMŘ CT Scan PET Scan Fluorography

Mammography Sonography Infrared

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**Echocardiograms** 

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Clinical Laboratory Diagnostic Methods for Determination of Biomarkers in Various Biological Fluids Blood Urine Saliva 5 Gastrointestinal fluids Reproductive fluids Cerebrospinal fluid **PCR** 10 Gene Markers Radioimmunoassay, ELISA Chromatography Receptor assays 15 Histologic Diagnostic Methods Tissue analysis Cytology Tissue typing Immunocytochemistry 20 Histopathological Analysis Electron Microscopy In situ hybridization Pharmacokinetic Diagnostic Methods 25 Therapeutic Drug Monitoring Receptor characterization and measurement Miscellaneous Factors Physical exam Medical history 30 Psychiatric and psychological history Behavioral patterns Behavioral testing Demographic data Patterns of drug, alcohol, tobacco, and food intake 35 Environmental influences (employment, exposure to chemicals, radiation, toxins, etc.)

Gross pathology

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Such models are based on input data with the individual patient under consideration, or information of a class of patents to which the individual patient belongs. The simulation output of these models forms the basis for comparison with the observed patient data and the detection of difference and abnormality in the next functional block.

3. Detection of Differences and Abnormalities: One of the key concepts in this simultaneous multi access reasoning technology system is the utilization of existing knowledge (i.e. CADRS and above diagnostic methods) and facts of normal and disease processes to avoid overloading the numerically oriented adaptive pattern

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classification subsystem with normal variations in observed data due to differences in patient conditions. In this block, the output results of the mechanistic models are compared with the observed patient data. The differences (not necessarily the simple numerical differences in values) are then fed as input into the adaptive pattern classification subsystem to produce the desired clinical indicators.

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4. Adaptive Pattern Classification Subsystem: The classification functions/algorithms in this block, due to the complex nature of clinical problems, are often non-linear in nature which include linear or stepwise linear systems as special cases. The construction of the classification functions and the determination of their parameters are based on known properties of the classification problem and most importantly, the implicit information contained in the available training data. Examples of such adaptive classification systems include various forms of artificial neural networks which classify information.

This invention is further illustrated by the following examples, which are not to be construed in any way as imposing limitations upon the scope thereof. On the contrary, it is to be clearly understood that resort may be had to various other embodiments, modifications, and equivalents thereof, which, after reading the description herein, may suggest themselves to those skilled in the art without departing from the spirit of the present invention and/or the scope of the appended claims.

In some of the following examples which utilize a neural network in the analysis of the data, a Neural Shell 2, Release 1.5 (Ward Systems Group, Inc.) neural network development program was used for the training of the neural network on a Pentium 60 mhz computer (Magitronic, Inc.). In other Examples, different computer hardware is used.

Example 1

The following example describes the training of a neural network to prognose prostate cancer.

A total of 52 samples were divided into 2 groups, a training set and a generalization testing set. The training set contained 40 samples (28 stable and 12 progressing) and the generalization testing set contained 12 samples (9 stable and 3 progressing).

The initial network architecture was selected based on the level of complexity of the classification task. A multi-layer feedforward network was used. Selection of the initial architecture involved the selection of the number of hidden layers and the number of neurons in each hidden layer. Several trial iterations were performed to

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determine an adequate configuration that showed good results on both the training sample set and the generalization test sample set. The present network had one hidden layer, having nine neurons, and two output neurons.

Initially, connection weights among the neurons were randomly set. The neural network had five input neurons, corresponding to five input variables significant for prostate cancer: TPS, PSA, PAP, CEA, and testosterone. The training data are shown in Fig. 5. During training, the five input variables for each patient were first linearly scaled into the continuous range between 0.0 and 1.0. The resultant five numbers were then presented as an input vector to the input neurons of the artificial neural network.

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For each of the input vectors, the network generated an output based on the connection weights among the network neurons. The output can be a single value or a vector of numbers, depending on the number of output neurons used. The network used had two output neurons. The outputs of the two neurons were processed by the following mathematical equation to yield a single diagnostic index:

$$Index = (ANN2-ANN1) + 0.5$$

Each neuron in the network participated in the output calculation by passing the sum of all inputs to the neuron through a non-linear s-shaped function (often a logistic function) and sending the result to each and every one of the neurons in the following adjacent layer. The generated output or each output neuron was compared to the desired "target" output. A value of 0.1 corresponded to a diagnosis of stable and an output of 0.9 corresponded to a diagnosis of progressing. The difference was used to calculate an error term to guide the training algorithm, i.e., the back propagation algorithm, in the adjustment of network connection weights in an attempt to reduce the differences between network outputs and target values over the training sample set.

After training, the neural network correctly classified 100% of the samples.

When presented with the generalization test results, the trained neural network correctly identified 100% of the stable samples and 66% of the samples where the disease was progressing.

#### Example 2

The mathematical description of the ProstAsure™ Algorithm is provided in Figure 25 which is attached hereto. The training data and test data for ProstAsure™

are provided in Figures 6 and 7, respectively. The training data set shows patient data for age, PSA, PAP, CK-BB, CK-MB, CK-MM, total CK, digital rectal examination, and ethnic group.

The ProstAsure™ system displayed the following sensitivities and specificities (expressed as a percentage) for cancer detection in the test data and training data:

Sensitivity for Detecting	<u>Test</u>	<b>Training</b>
Prostate Cancer (PC)	80.3%	84.4%
Stage 2 PC	85.3	85.1
Stages T2, T3 and TNxM1(PC)	87.9	87.9
For detecting BPH as BPH	66.1	68.9
Specificity for Identifying	Percent	
Non-Cancer as Non-Cancer	92.8%	91.8
Presumed Normal as Normal	67.6	69.2

#### \*BPH = Benign prostatic hyperplasia

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These results of the ProstAsure™ system were highly statistically significant when analyzed with a Pearson Chi-Square test. Chi-Square value=128.8, with 4 degrees of freedom and a p value <0.00001. These results demonstrate the sensitivity and specificity of the ProstAsure™ system to diagnose prostate cancer, to distinguish stages of the disease, and to recognize benign prostatic hyperplasia and normals as such.

25 Example 3

This example illustrates the construction and training of a neural network for diagnosis of osteoporosis. The training and test data are shown in Figs. 8 and 9 respectively. The mathematical description of the QuiOs<sup>TM</sup> algorithm is attached hereto as Figure 26. This example illustrates the construction and training of a neural network for diagnosis of osteoporosis.

Fig. 8 provides the data used to train the neural network to diagnose osteoporosis. The biomarkers selected included age, calcium, phosphate, estradiol (ETWO), progesterone, total alkaline phosphatase, total intestinal alkaline phosphatase, and % liver alkaline phosphatase. Fig. 8 further includes the diagnostic index obtained by the neural network.

Fig. 9 provides the data use to test the network trained with the data in Fig. 9, and the neural network diagnostic index obtained.

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In practicing one aspect of the present invention, the severity of disease in a set of humans or animals with varying severity of disease is measured by a standard method or methods. The measurement is then assigned a numerical value corresponding to a severity scale. The scale ranges from humans or animals with no disease, to humans or animals with severe disease. The scale is preferably a numerical scale. For example, one could assign a value which corresponds to normal or slight disease, another value which corresponds to moderate disease and a third value which corresponds to severe disease.

The concentration of a predetermined set of blood constituents in the set of humans or animals with varying severity of disease is then determined. According to the present invention, it is preferable to measure the blood constituents in the same set of humans or animals in which the severity of disease was measured by the conventional method or methods.

#### Osteopenia

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An example of practicing one embodiment of the present invention is a method for diagnosing osteopenia in a patient. The method preferably utilizes six blood constituents. These constituents are calcium, phosphate, total alkaline phosphatase, an alkaline phosphatase isoenzyme, estradiol, and progesterone. The alkaline phosphatase isoenzymes preferred for practicing the present invention include lymphocyte-derived alkaline phosphatase isoenzyme and bone, liver or intestinal alkaline phosphatase isoenzymes. The present invention includes calculating a bone density quotient using the aforementioned six blood constituents by entering the values for the tests into an QuiOs<sup>TM</sup> algorithm which is attached hereto as Figure 26. Age, weight and height are also included in the QuiOs<sup>TM</sup> algorithm.

In addition to diagnosing the osteopenic state of the patient, an indication of the underlying cause of the osteopenia can be determined using the present invention. For example, by practicing the present invention as described herein, one can determine whether the osteopenia in a patient is caused by post-menopausal lack of estrogen or is caused by some other condition, such as cancer. This allows the attending physician to be better able to prescribe the appropriate treatment for the osteopenia.

Five of the serum tests that are used in the present invention are tests that are commonly performed by clinical laboratories. The test for t-lymphocyte derived alkaline phosphatase is experimental only; however, the test for blood, liver and intestinal alkaline phosphatase isoenzymes are also known. The type of test used to determine the six serum constituents is not critical to the present invention as long as

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the tests give accurate blood concentrations of the constituents being measured. The results are shown in Figures 10 and 11 and show excellent sensitivity and specificity in the diagnosis of osteopenia.

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## Example 4

This example provides an explanation of an approach for the construction and training of a computer-based neural network based classifier for the computer assisted diagnosis and prognosis of disease. The lettered subsection headings refer to the lettered labels in Figure 13.

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a. Initial Selection of Inputs Biomarkers and other measures (anatomical, physiological, pathological, etc.) that are relevant to the disease process are selected in such a way that useful information may be extracted for the diagnosis of the disease and the stage of progression of the disease. The selection relies heavily on medical expertise, on current knowledge in biomedical basic science and on advances in clinical research.

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b. Test for Discriminating Power A statistical analysis of discriminating power of the selected inputs, individually, and in linear and nonlinear combinations is performed using test data from the training set. The types of software used include commercial statistical packages (e.g. MatLab<sup>TM</sup> by The Math Works, Inc., Statistira For Windows release 4.5 by StatSoft, Inc.) and programs developed by Horus staff for clustering analysis with nonlinear combination and transformation of input values. Scientific data visualization techniques are used to guide the construction of nonlinear combination and transformation. Inputs that fail to show any discriminating power in separating patient data points of different diagnostic groups in the training data are removed from the pool of selected inputs.

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c. Grouping of Individual Inputs Several of the initially identified inputs may be closely related or simply different measures of the same aspects of the disease process and offer similar yet slightly different values. They are grouped together into subsets of inputs. During the development of neural network based classifiers (which provide a classification system implemented with neural networks), inputs from each subset are used one at a time (ones with higher discriminating power first) to form the list of actual inputs to the classifiers. Biomedical expert knowledge is used in the grouping procedure. For example, two slightly different tests measuring the same biological phenomenon such as CA125 and CA125II might be grouped together. Statistical analyses of interaction, association and agreement between inputs help to identify such groups (e.g., Chi-Square, paired-t test, etc.).

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Preprocessing The preprocessing step includes preparation of input d. values, "preprocessed values" to be used as actual inputs to neural network based classifiers. This step includes linear or non-linear transformation (e.g. re-scaling) of original input biomarker or demographic values which may be digitized values and/or the creation of secondary inputs using linear or non-linear combination of original input values. Software and procedures used in this step are similar to that in step b, "Testing for discriminating power", described above. In step b, the goal is to determine whether or not a particular biomarker or other measurement provides any useful information. In this step d, however, the purpose is to find a set of inputs to the neural network based classifier that in addition to having sufficient discriminating information, should also provide such information in a way that alleviates the burden of neural network training. In this step, statistical, mathematical, and computational tools are used to help "pre-digest" the information. For example, two inputs combined in a non-linear formula provides more explicit information for classification. Add an input that is the computed value using this formula makes the training easier. Expert knowledge in both biomedical and clinical science fields (e.g. whether certain types of transformation or combination is biologically "plausible") and experience in pattern classification are used. For example, by viewing samples in the input variable space, one may be able to estimate the complexity in sample distribution and use this information to adjust the neural network structure. Due to the nature of nonlinear operation and the often large number of inputs used in combination, direct numerical evaluation of the effectiveness of the newly created secondary inputs may be very difficult. Scientific data visualization is extensively used to provide guidance in the construction and the evaluation of secondary inputs. For example, color coding and coordination system transformation allows the viewing of data in higher than 3dimensional space. This helps to understand the distribution of samples in the input variable space and the construction of preprocessing steps.

This preprocessing step is very important. Previous workers in this area assumed that the non-linear nature of the neural network would be able to fully utilize information in the training data in the form of the original input values. (see Astion, M. L. and Wilding, P., "Application of Neural Networks to the Interpretation of Laboratory Data in Cancer Diagnosis", Clinical Chemistry 38: 34-38 (1992) in which there is no mention of preprocessing). However, this step of "untangling" of multi-threaded and inter-related information to facilitate the training of the neural network plays a vital role in the success of developing neural network based diagnostic systems.

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e. Selection of Inputs with Highest Discriminating Power This step involves the selection of input values from original input values, which are possibly transformed, and from newly created secondary inputs, to form a list of actual inputs to the neural network based classifier. The initial number of selected inputs in the list is based on the results from discriminating power estimation in steps b and d and the available knowledge of the complexity of the problem.

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- f. Test/Evaluation and Analysis of Contributions of Individual Inputs In this step, the performances of the trained neural network based classifiers are evaluated with data from the test data set that have not been involved in the construction and training of the neural network based classifier which is a classification system that uses neural networks as its classification decision making component. Because of the nonlinear nature in neural network based computation, direct analysis of contribution of individual inputs in producing the final output of an neural network classifier is often not possible. The following steps are used: 1) inspection of network connection strength initiated from each input; 2) sensitivity analysis that compares the relative change in neural network output with changes in single input values; and 3) more complete analytical methods such as using Monte Carlo sampling methods to construct a sensitivity surface with respect to simultaneous changes in multiple inputs.
- g. Selection of Best Trained Neural Network Classifier The iterative process of adding/deleting input values and construction/evaluation of neural network classifiers produces multiple configurations of neural network based diagnostic systems. The selection of "best" are based on the two primary considerations: 1) the effectiveness of the system in both absolute terms and in comparison with existing methods; and 2) the number of inputs and the cost associated with them.

#### Example 5

Procedure for Construction and Training of Neural Network Based Classifier for Computer Assisted Diagnostic Apparatus

The following list describes the steps used in the construction and training process as shown in Fig. 14.

- 1. If the total number of diagnostic groups equals 2, go to next step. Otherwise, based on known facts about the disease process, organize the separation of groups into a binary classification decision tree. For each pair of groups that requires a binary classification (yes/no, positive/negative, etc.) repeat steps 2 6.
- 2. Develop neural networks in the first level. (ANN 1,1 through ANN 1,M)

- a. Select an appropriate data set for training and testing.
- b. If the total number of recorded neural networks exceeds a preset number, go to step 3.
- c. Configure a new neural network and select a subset from the total input list (done by setting the neural network input selector).
- d. Train multiple neural networks of the same configuration with various initial conditions and training parameters. For each trained neural network, if the results overlap significantly with a previously trained neural network including networks with different network configurations (in terms of patients in each group being classified correctly or incorrectly), discard the one that has the inferior performance. Repeat until no significant performance improvement is observed in newly trained neural networks or all reasonable variations of initial conditions and parameters have been exhausted.
- e. If all reasonable network configurations and their variations have been exhausted, go to next step, otherwise go to step 3.
- 3. Compare performance of all recorded neural networks and purge those with poor or duplicated performance. If two neural networks offer similar results, delete the one with more complicated network structure.
  - 4. Record all remaining neural networks.
- 5. Develop neural networks in the second level (neural networks (ANNs) 2,1 through ANN 2,N). Augment the original list of inputs with output values from remaining neural networks in the first level and repeat steps 2 4.
- 6. Combine output from one or several recorded neural networks into a single classification index using linear or nonlinear methods. Evaluate its performance in separating the two diagnostic groups using test data not involved in network training. Select the best binary classification function for the pair of diagnostic group.
- 7. Combine the obtained binary classification functions according to the binary classification decision tree to form a "super function" that produces a single valued diagnostic index with the Horus arbitrary unit and reference ranges for each of the different diagnostic groups.

### Example 6

ProstAsure™ Computer-Based System for Neural Network Analysis of Patient Data for Diagnosis of Prostate Cancer

This is a computer-based system which provides the capability to receive patient data, analyze the data with a trained neural network, produce an output value

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indicative of the presence or absence of prostate cancer, transmit the value to another computer, and transmit the value to another location. The system is schematically illustrated in Figure 15. The individual boxes in Fig. 15 are numbered and referred to in the following description. This system provides high capacity to receive and analyze a large volume of patient data, to rapidly produce output values to diagnose prostate cancer and to optionally transmit these results to remote locations. This system permits the rapid analysis of numerous sets of patient data and provides diagnostic values to the clinical laboratory and to the health care provider. It is to be understood that Figure 15 represents a preferred embodiment of the present invention and that other system configurations, such as different hardware configurations involving a single computer or multiple computers may be employed in the practice of this invention for the diagnosis of any disease including prostate cancer.

The data files contain data from patient tests that are required for the computation of the diagnostic index for prostate cancer. The data file is a standard ASCII file. Each patient record consists of one line in the file. Lines in the file are delimited with carriage return; line feed (CR/LF) pairs. The fields in a record are delimited with an ASCII character ",", and each record contains the following seven fields: 1) identification (ID)- alphanumeric; 2) Age - numeric; 3) prostate specific antigen (PSA)- numeric; 4) PAP - numeric; 5) CKBB - numeric; 6) CKMB - numeric; 7) CKMM - numeric. Each alphanumeric field contains a string of characters consisting of letters 'a' through 'z', 'A' through 'Z', digits '0' through '9', and the characters '\_', '-', '.', '\$'. A numeric field contains a string representation of a decimal number. It may contain a single decimal point '.'. The space character ' and comma character ',' are not allowed within a number.

Each patient record occupies a single line in the input data file. Data fields in a record are separated by commas. In the result file to be returned to LabCorp, the input values are repeated and then followed by two additional data fields also separated by commas: the computed ProstAsure<sup>TM</sup> (HORUS Therapeutics, Rochester, NY) value, and an integer valued error code.

Prior to the actual computation of the ProstAsure<sup>TM</sup> value, a patient record is checked for errors according to the following error detection criteria in the order as they are listed as shown in Fig. 16. Whenever an error other than code 130 happens, error check stops. No ProstAsure<sup>TM</sup> Value is computed for the patient. The ProstAsure<sup>TM</sup> field in the output file record is filled with "xxxx" and the first non-130 error code will attach as the last field. When all criteria have been checked and no error or only code 130 has been detected, the ProstAsure<sup>TM</sup> value is computed and

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reported in the result file record. The error code 0 or 130 is attached accordingly as the last field.

Error codes are defined as follows:

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Error code 110 - The record contains fewer than 7 comma separated fields. An empty field followed by a comma is still considered as a field and will not trigger this test.

Error code 100 - The first field (ID field) is empty.

Error code 120 - One of the remaining data fields is not in a valid numerical format (including an empty field) or one of the data fields has a negative value.

Error code 130 - One of the laboratory test values exceeds 5 times the upper bound of the normal patient reference range; or three (3) or more laboratory test results have zero values; or age =0 or age >150.

The ProstAsure<sup>TM</sup> system consists of two computer workstations and associated communication devices and links (Fig. 15). The following paragraphs provide an overview of the system.

ProstAsure<sup>TM</sup> Station I (14) is primarily a communication control station. It downloads test data from a remote computer system (LabCorp) (1) via a modem (2) and a telephone line and uploads the ProstAsure<sup>TM</sup> results back to the remote system. Station I (14) is linked to Station II (15) by a direct null modem cable (7) on their corresponding serial ports. Station I (14) sends successfully downloaded data files to Station II (15) and receives ProstAsure<sup>TM</sup> result files from Station II for uploading. Station I controls the timing of download intervals. It processes error conditions (6) by retrying and/or alarming operators (13) depending on the error conditions. Station I compares the data portions of outgoing result files and incoming data files (5) before uploading (4) and (3) to ensure integrity of the result files.

ProstAsure<sup>TM</sup> Station II (15) is the main computation station for ProstAsure<sup>TM</sup> algorithm computation (11) and houses the trained neural network (11). Station II (15) receives data files from Station I (14) and sends (8 and 9) results files to Station I (14). Station II (15) reads and verifies the data received from Station I. If invalid data are detected (12 and 10), the ProstAsure<sup>TM</sup> result field will be marked with "x" characters and a special error code will also reflect the condition. If the data values are detected to be unusual but valid, the ProstAsure<sup>TM</sup> result will be provided; however, an error code will indicate the condition. Station II invokes a dynamic link library (DLL) from the commercial software package NSHELL2 release 2.0 (Ward Systems Group, Inc., Frederick, MD) a leading neural network software, to perform the computations

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of neural network structures. Station II contains error handling procedure (10) to process various error conditions. It alarms (9 and 10) the operators (13) under critical error conditions. Station II is also responsible for archiving the original data files and result files.

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The ProstAsure<sup>TM</sup> system uses Kermit software (Columbia University) for communications between two Stations I and II and between Station I and remote computer systems. Kermit is reliable, well tested communication protocol. The ProstAsure<sup>TM</sup> system software runs under Microsoft Windows environment, which provides a consistent, friendly user interface. ProstAsure<sup>TM</sup> software is designed to execute in full screen mode to simplify the operations.

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## System Description

System Requirements:

A schematic overview of the system is provided in Figure 15.

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Station I 14: Station I requirements include the following: a Pentium computer 75 Mhz or higher, a minimum of 8 Mb RAM, a minimum of 1.0 Gb Hard Drive, an internal modem at speed 9600 bps or higher, a SVGA monitor, and Microsoft Windows for Work group (WFW) 3.11.

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Station II 15: Station II requirements include the following: a Pentium 75 Mhz or higher, a minimum of 8 Mb RAM, a minimum of 1.0 Gb Hard Drive, an internal 850 MB tape drive, a super VGA monitor, and Microsoft Windows for Workgroup (WFW) 3.11.

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The system requires a laser printer that has Microsoft Windows supported printer driver. Also required is null modem 7 and RS-232 cable for connection between Station I and II via serial ports.

Actually Installed System

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An example of an actually installed system is as follows:

Station I is composed of: NEC Ready Pentium Systems™

(Pentium 100 MHz CPU, 16 Mb RAM, 1.0 Gb Hard Drive)

NEC MultiSync XV17™ Monitor;

preloaded with MS Windows for Workgroup 3.11.

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Station II is composed of: NEC Ready Pentium Systems™

(Pentium 100 MHz CPU, 16 Mb RAM, 1.0 Gb Hard Drive)

Internal 850 Mb Tape unit:

NEC MultiSync XV17™ Monitor, preloaded with MS Windows for Workgroup 3.11.

Printer:

HP LaserJet III

References:

Operations Procedure:

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Ready Pentium Systems User's Guide;

NEC Ready Pentium Systems Hardware Ref./Operations Guide;

NEC MultiSync XV17TM User's Guide.

## Functions of the Systems

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In the following description of procedures, the term "emergent warning procedure" defines an automated procedure to report an abnormal situation in the computer software or hardware system, or in the data file transferring mechanism that requires the immediate attention or intervention of a human operator and/or the Director of Operation 13. In the "emergent warning procedure", 1) the affected computer produces a loud siren that can be heard throughout the facility; 2) the affected computer screen blinks and displays the error message and the corresponding error code; and 3) the computer system automatically dials the pager number of the officer on duty.

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Station I 14 downloads patient test data from and uploads computed results back to the host computer (1) (a HP3000 UNIX based workstation) located at the Laboratory Corporation of America (LabCorp) facility in Research Triangle Park, North Carolina. Station I serves as a buffer and a firewall between the external data source (LabCorp host computer) and the ProstAsure<sup>TM</sup> processing workstation (Station II) 15. The following are detailed descriptions of functions provided by Station I. These are also the functions tested during system validation.

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I-1: Initiating remote connection via modem to the host computer. Invoking the automated login procedure using the MS DOS Kermit software and the downloading procedure to obtain a new patient data file for processing. It uses the Kermit ASCII file transfer protocol.

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I-2: Connection and file down loading automatically occurs every 60 minutes. In case of a failed connection, a re-connection automatically repeated in 10 sec. interval. After a continuous sequence of 10 failed such attempts, System I issues error code #200 and starts the "emergent warning procedure".

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I-3: Upon completion of data file down loading, System I initiates connection to Station II and sends the newly received data file to Station II. If Station I fails to send data after 10 repeated attempts, it issues error code #230 and starts "emergent warning procedure".

Station II processes the received data, computes ProstAsure<sup>TM</sup> index for each patient, and sends the results together with the original input values to Station I.

- I-4: Upon successful reception of completed result data file, Station I then compares input values of each patient in the result data file with the input values in the originally received data file to ensure a complete match. If any error occurs, the "emergent warning procedure" is invoked and error code #300 or #310 (number of records do not match) or #320 (at least one record has unmatched input values) are displayed. When 300 series errors happen, no results are sent to the LabCorp host computer and the Director of Operations is notified immediately.
- I-5: Connecting to LabCorp and sending data back to the LabCorp host computer. (Similar to I-1, except for performing file unloading instead of file downloading).
- I-6: Similar to I-2, if the connection attempt fails, Station I repeats connection attempts in 10 seconds intervals. After a continuous sequence of 10 failed such attempts, Station I displays error code #290 and starts "emergent warning procedure".

Station II receives data from and sends data to Station I. Station II processes data using the ProstAsure<sup>TM</sup> algorithm. The following functions are provided by Station II. These functions are tested during system validation.

- II-1: Upon establishing connection initiated by Station I, Station II receives the transmitted patient file.
- II-2: Station II sequentially processes patient records in the data file using the ProstAsure<sup>TM</sup> algorithm. (See Figure 25)
- II-3: Upon completion of Step II-2, Station II initiates connection to Station I and sends the result data file to Station I using the MS DOS Kermit ASCII file transfer protocol. If file sending fails after 10 repeated attempts, Station II issues error code #260 and starts the "emergent warning procedure". A record (line) in the result data file consists of the input data values as used in the computation plus two additional fields, the computed ProstAsure<sup>TM</sup> value of the patient and a three digit code indicating whether the computation is normal or abnormal. In the abnormal case, the code is an error code which contains information about the type of abnormality that has occurred.

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II-4: After completion of sending the result data file to Station I, the data file and the result file which consists of the data file plus two additional field columns: 1) computed values, and 2) error codes, are archived in two designated directories in Station II, "c:\pacompu\padata\" and "c:\pacompu\paresult\" with the file names reflecting encoded date and time tag in the form: mmddhhnn.yy, where mm:month, dd:date, hh:hours, nn:minutes, and yy:year.

### Example 7

The present invention includes use of a computer-assisted neural network to diagnose ovarian cancer. This new version uses biomarkers listed above under the heading of Ovarian Cancer II and includes CA125, M-CSF, OVX1, LASA, CAA7-24 and CA19-9. When tested with an independent data set of 186 subjects, the test achieves a sensitivity of 89% and a specificity of 89%.

It should be understood, of course, that the foregoing relates only to preferred embodiments of the present invention and that numerous modifications or alterations may be made therein without departing from the spirit and the scope of the invention as set forth in the appended claims.

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### **Claims**

We claim:

1. A process for diagnosing or prognosing a disease in a patient comprising:

converting concentrations of patient biomarkers associated with the disease to digitized values;

preprocessing the digitized values to make preprocessed values;

inputting the preprocessed values to a computer which contains a trained neural network;

introducing the preprocessed values into the trained neural network, wherein the trained neural network is specifically trained to diagnose or prognose the disease, and produce an output value, the output value corresponding to the presence or the absence or the severity of the disease; and

transmitting the output value from the trained neural network to an output value receiver connected to a display means.

2. The process of Claim 1, further comprising: converting patient demographic data to digitized values; preprocessing the digitized values to make preprocessed values; inputting the preprocessed values to the computer; and introducing the preprocessed values into the trained neural network.

## 3. The process of Claim 1, further comprising:

introducing the output value from the trained neural network and a second set of preprocessed values from patient biomarkers or optionally from a second set of preprocessed values from patient demographic data into a second trained neural network in a computer, wherein the second trained neural network is trained to diagnose or prognose the disease and produces a second output value, the second output value corresponding to the presence or the absence or the severity of the disease; and

transmitting the second output value from the second trained neural network to an output value receiver connected to a display means.

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4. The process of Claim 1, comprising:

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inserting patient biomarker data and optionally patient demographic data into a patient record;

introducing the data in the patient record into a computer, wherein the data are analyzed for data format errors;

converting the patient data with no format errors to digitized values;

preprocessing the digitized values to make preprocessed values;

introducing the preprocessed values into a trained neural network, wherein the trained neural network is specifically trained to diagnose or prognose the disease and produce an output value which indicates the presence or the absence or the severity of the disease; and

inserting the output value and the patient data into the patient record.

5. The process of Claim 1, wherein the disease is selected from the group consisting of osteoporosis, osteopenia, breast cancer, ovarian cancer, colon cancer, prostate cancer, and testicular cancer.

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6. A process for training a computer-based neural network to be used in diagnosing or prognosing disease in a patient comprising:

randomizing connection weights in the computer-based neural network;

obtaining concentrations of patient biomarkers associated with a disease from a group of patients with the disease;

converting the concentrations of the biomarkers to digitized values;

preprocessing the digitized values to make preprocessed values;

training the network by serially introducing the preprocessed values from each patient as input variables through inputs to the neural network;

obtaining an output value from the neural network, wherein the output value indicates a neural network diagnosis and corresponds to the presence or the absence or the severity of the disease;

comparing the output value of the neural network to an actual diagnosis;

adjusting the connection weights if the neural network diagnosis does not correspond to the actual diagnosis;

introducing the preprocessed values from a patient within the group of patients as input variables through inputs to the neural network;

obtaining an second output value from the neural network,

comparing the second output value of the neural network to the actual diagnosis and adjusting the connection weights if the neural network diagnosis does not correspond to the actual diagnosis;

repeating the previous steps for introducing preprocessed values from other patients within the group to the neural network, obtaining a new output values, comparing the new output values to the actual diagnosis, and optionally adjusting the connection weights; and

optionally establishing decision limits regarding a classification error.

# 7. An apparatus comprising:

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a computer containing a trained neural network, wherein the trained neural network is trained to diagnose or prognose a disease.

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8. The apparatus of Claim 7, further comprising:

means for converting concentrations of patient biomarkers associated with the disease to digitized values;

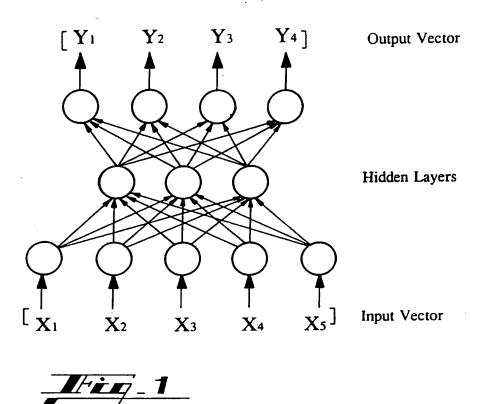
means for preprocessing the digitized values to make preprocessed values;
means for inputting the preprocessed values into the trained neural network
wherein the trained neural network produces an output value, the output value
corresponding to the presence or the absence or the severity of the disease; and,

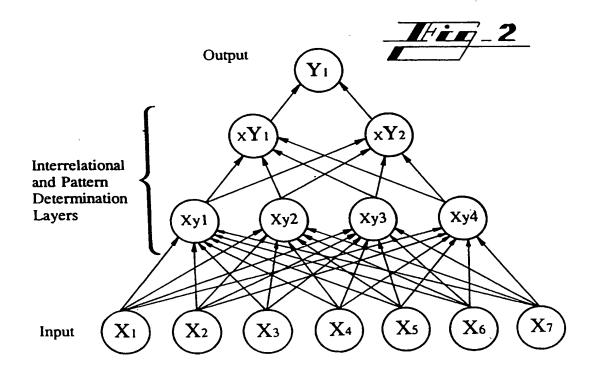
means for communicating the output value.

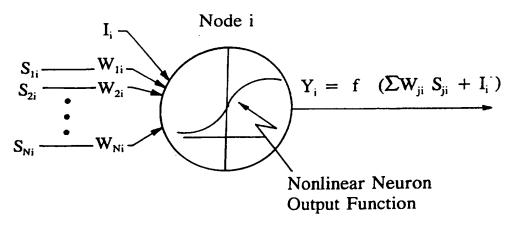
9. The apparatus of Claim 7, further comprising: means for converting patient demographic data to digitized values; means for preprocessing the digitized values to make preprocessed values; means for inputting the preprocessed values into the trained neural network wherein the trained neural network produces an output value, the output value corresponding to the presence or the absence or the severity of the disease; and, means for communicating the output value.

- 10. The apparatus of Claim 8, further comprising more than one trained neural network, wherein the trained neural networks are specifically trained to diagnose or prognose a disease and each produces an output value, the output value corresponding to the presence or the absence or the severity of the disease.
- 11. The apparatus of Claim 7, wherein the disease is selected from the group consisting of osteoporosis, osteopenia, breast cancer, ovarian cancer, colon cancer, prostate cancer, and testicular cancer.

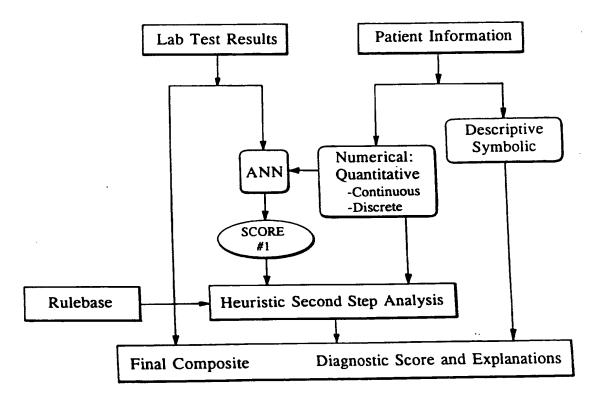
1/64













Prostate Cancer Prognosis Training Data

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0.69         7.8         1.3         5.6         0.1         0.9         0.10           0.44         0.6         1         0.3         0.9         0.1         0.90           0.44         0.6         1         0.3         0.9         0.1         0.90           0.02         1.3         1.2         1.6         0.9         0.1         0.80           0.02         1.2         1.7         1.2         0.9         0.1         0.80           0.02         1.2         1.7         1.2         0.9         0.1         0.90           0.02         1.2         1.7         1.2         0.9         0.1         0.90           0.04         0.7         0.9         0.1         0.90         0.1         0.90           0.04         0.7         0.9         0.1         0.9         0.10         0.90           0.05         0.4         0.1         0.9         0.1         0.90         0.10           0.24         2.9         0.4         0.1         0.9         0.1         0.90           0.25         0.2         0.3         0.1         0.9         0.1         0.90           0.05 <th>TPS</th> <th><b>PSA</b></th> <th>PAP</th> <th>CKA</th> <th>Testosterone</th> <th>Stable</th> <th>Progress</th> <th>ANNoutput</th> <th>ANNoutput2</th> <th>Actual</th> <th>Index</th>	TPS	<b>PSA</b>	PAP	CKA	Testosterone	Stable	Progress	ANNoutput	ANNoutput2	Actual	Index
0.59         0.7         0.4         1.9         0.9         0.1         0.90           0.44         0.6         1         0.3         0.9         0.1         0.90           0.02         1.3         1.2         1.6         0.9         0.1         0.90           0.02         1.2         1.7         1.2         0.9         0.1         0.90           0.02         1.5         0.8         0.9         0.1         0.90           0.04         0.7         0.6         0.8         0.9         0.1         0.90           0.01         0.7         0.9         0.1         0.90         0.1         0.90           0.02         1.6         0.9         0.1         0.9         0.1         0.90           0.02         1.6         0.9         0.1         0.9         0.1         0.90           0.04         0.1         0.9         0.1         0.9         0.1         0.90           0.44         2.9         0.4         0.1         0.9         0.1         0.90           0.45         5.0         0.2         0.3         0.1         0.9         0.10           0.02         0.2 <td>.53</td> <td>0.69</td> <td>7.8</td> <td>1.3</td> <td>5.6</td> <td>0.1</td> <td>6.0</td> <td>0.10</td> <td>06.0</td> <td>0.0</td> <td>0.90</td>	.53	0.69	7.8	1.3	5.6	0.1	6.0	0.10	06.0	0.0	0.90
0.44         0.6         1         0.3         0.9         0.1         0.90           0.02         1.3         1.2         1.6         0.9         0.1         0.80           0         1.2         1.7         1.2         0.9         0.1         0.80           0.02         1.5         0.8         0.5         0.9         0.1         0.90           0.04         0.7         0.6         0.8         0.9         0.1         0.90           0.04         0.7         0.6         0.8         0.9         0.1         0.90           0.05         0.1         0.9         0.1         0.90         0.1         0.90           0.04         0.7         0.6         0.3         0.9         0.1         0.90           0.05         0.1         0.9         0.1         0.90         0.10         0.90           0.44         2.9         0.4         0.1         0.9         0.1         0.90           0.05         0.4         0.1         0.1         0.9         0.1         0.90           0.05         0.2         0.3         0.1         0.9         0.1         0.90           0.05	25	0.59	0.7	0.4	1.9	0 0	-	06.0	0.10	0.1	0.10
0.02         1.3         1.2         1.6         0.9         0.1         0.80           0         1.2         1.7         1.2         0.9         0.1         0.90           0.02         1.5         0.8         0.5         0.9         0.1         0.90           0.04         0.7         0.6         0.8         0.9         0.1         0.90           0.01         0.2         0.1         0.9         0.1         0.90           0.05         1.1         0.9         0.1         0.90           0.05         1.1         0.9         0.1         0.90           0.44         2.9         0.4         0.1         0.9         0.1           0.44         2.9         0.4         0.1         0.9         0.1         0.90           0.44         2.9         0.4         0.1         0.9         0.1         0.90           0.02         1.4         0.1         0.9         0.1         0.90         0.10           0.02         1.2         0.3         0.1         0.9         0.1         0.90           0.02         1.2         0.3         0.1         0.9         0.1         0.90	8	0.44	9.0	1	0.3	6.0	0	0.90	0,10	0.1	0.10
0         1.2         1.7         1.2         0.9         0.1         0.90           0.02         1.5         0.8         0.5         0.9         0.1         0.90           0.04         0.7         0.6         0.8         0.9         0.1         0.90           0.0         0.4         0.9         1.1         0.9         0.1         0.90           0.26         1.6         0.6         0.3         0.9         0.1         0.90           0.42         1.1         1.2         0.9         0.1         0.90         0.1           0.26         1.6         0.6         0.3         0.9         0.1         0.90           0.44         2.9         0.1         0.9         0.1         0.90         0.10           0.02         1.4         1.7         0.7         0.9         0.1         0.90           0.02         1.4         0.7         0.9         0.1         0.90         0.10           0.02         1.4         0.7         0.9         0.1         0.90         0.10           0.02         0.5         0.1         0.9         0.1         0.90         0.10           0.02 <td>9.6</td> <td>0.02</td> <td>1.3</td> <td>1.2</td> <td>1.6</td> <td>0.0</td> <td>0.1</td> <td>0.89</td> <td>0.11</td> <td>0.1</td> <td>0.11</td>	9.6	0.02	1.3	1.2	1.6	0.0	0.1	0.89	0.11	0.1	0.11
0.02         1.5         0.8         0.5         0.9         0.1         0.90           0.04         0.7         0.6         0.8         0.9         0.1         0.90           0         0.4         0.9         1.1         0.9         0.1         0.90           0.01         0.5         0.9         0.1         0.90         0.90           0.26         1.6         0.6         0.3         0.9         0.1         0.80           0.42         1.1         1.2         0.9         0.1         0.90         0.10           0.42         1.1         1.2         0.9         0.1         0.9         0.10           0.44         2.9         0.4         0.1         0.9         0.1         0.90           0.02         0.5         0.7         2         0.9         0.1         0.90           0.02         0.5         0.1         0.9         0.1         0.90         0.10           0.02         0.5         0.7         2         0.9         0.1         0.90           0.01         0.5         0.7         2         0.9         0.1         0.90           0.02         0.5	22	0	1.2	1.7	1.2	6.0	0.1	0.00	0.10	0.1	0.10
0.04         0.7         0.6         0.8         0.9         0.1         0.90           0         0.4         0.9         1.1         0.9         0.1         0.90           0         0.4         0.9         1.1         0.9         0.1         0.90           0.26         1.6         0.6         0.3         0.9         0.1         0.90           0.42         1.1         1.2         0.9         0.1         0.90         0.10           0.44         2.9         0.4         0.1         0.9         0.1         0.90           0.44         2.9         0.4         0.1         0.9         0.10         0.90           0.02         1.4         1         0.7         0.9         0.1         0.90         0.10           0.02         0.5         0.1         0.9         0.1         0.9         0.10         0.90           0.01         0.5         0.7         2         0.9         0.1         0.90         0.11           0.02         0.5         0.7         2         0.9         0.1         0.90         0.11           0.02         0.5         0.7         2         0.9	2	0.02	1.5	8.0	0.5	0.9	0.1	06.0	0.10	0.1	0.10
0         0.4         0.9         1.1         0.9         0.1         0.90           0.01         0.5         0.9         1         0.90         0.90           0.26         1.6         0.6         0.3         0.9         0.1         0.90           0.42         1.1         1.2         0.9         0.1         0.90         0.10           0.44         2.9         0.4         0.1         0.9         0.1         0.90           0.65         5.5         0.2         0.3         0.1         0.9         0.10           0.02         3         0.9         2.9         0.1         0.9         0.10           0.02         0.4         0.1         0.7         0.9         0.10         0.90           0.01         0.5         0.7         2         0.9         0.1         0.90           0.01         0.5         0.7         2         0.9         0.1         0.90           0.02         0.5         0.7         2         0.9         0.1         0.90           0.02         0.5         0.7         2         4.1         0.9         0.1         0.90           0.01         <	29	0.04	0.7	9'0	8.0	6.0	1	06.0	0.10	0.1	0.10
0.01         0.5         0.9         1         0.90           0.26         1.6         0.6         0.3         0.9         0.1         0.89           0.42         1.1         1.2         0.9         0.1         0.90         0.10           0.44         2.9         0.4         0.1         0.9         0.10         0.90           0.66         5.5         0.2         0.3         0.1         0.9         0.10           0.02         3         0.9         2.9         0.1         0.9         0.10           0.02         1.4         1         0.7         0.9         0.1         0.90           0.01         0.5         0.1         0.9         0.1         0.90           0.01         0.5         0.1         0.9         0.1         0.90           0.02         0.5         0.1         0.9         0.1         0.90           0.02         0.5         0.1         0.9         0.1         0.90           0.02         0.2         0.2         0.9         0.1         0.90         0.1           0.02         0.2         0.4         0.1         0.9         0.1         0.90	5	٥	0.4	6'0	1.1	0.9	0.1	0.00	0,10	0.1	0.10
0.26         1.6         0.6         0.3         0.9         0.1         0.89           0.42         1.1         1.2         0.9         0.1         0.90         0.10           0.44         2.9         0.4         0.1         0.9         0.10         0.90           0.65         5.5         0.2         0.3         0.1         0.9         0.10           0.02         3         0.9         2.9         0.1         0.9         0.10           0.01         0.5         0.7         2         0.9         0.1         0.90           0.01         0.5         0.1         0.9         0.1         0.90           0.02         0.5         0.1         0.9         0.1         0.90           0.02         0.5         0.1         0.9         0.1         0.90           0.02         0.5         0.1         0.9         0.1         0.90           0.01         0.2         4.1         0.9         0.1         0.90         0.1           0.02         2.6         4.8         0.4         0.9         0.1         0.9         0.1           0.01         2.6         4.8         0.4	8	0.0	0.5	6'0	ı	6.0	0.1	06.0	0.10	0,1	0.10
0.42         1.1         1.2         0.9         0.9         0.1         0.90           0.44         2.9         0.4         0.1         0.9         0.10         0.90           0.66         5.5         0.2         0.3         0.1         0.9         0.10           0.02         3         0.9         2.9         0.1         0.9         0.10           0.02         1.4         1         0.7         0.9         0.1         0.90           0.01         0.5         0.7         2         0.9         0.1         0.90           0.02         0.5         1.0         4.3         0.9         0.1         0.90           0.04         2.6         1.2         4.1         0.1         0.9         0.11           0.01         1.2         4.1         0.1         0.9         0.11           0.01         1.2         4.1         0.1         0.9         0.11           0.02         2.6         4.8         0.4         0.1         0.9         0.11           0.01         1.2         4.1         0.9         0.1         0.9         0.11           0.4         2.6         1.2	8	0.26	1.6	9.0	0.3	0.9	0.1	0.89	0.11	0,1	0.11
0.44         2.9         0.4         0.1         0.1         0.9         0.10           0.66         5.5         0.2         0.3         0.1         0.9         0.10           0.02         3         0.9         2.9         0.1         0.9         0.10           0.02         1.4         1         0.7         0.9         0.1         0.90           0.01         0.02         0.7         2         0.9         0.1         0.90           0.02         0.5         1.0         4.3         0.9         0.1         0.90           0.02         2.6         4.8         0.4         0.1         0.9         0.11           0.01         1.9         5.4         0.5         0.1         0.9         0.11           0.01         1.2         4.1         0.9         0.1         0.9         0.11           0.01         1.2         4.1         0.9         0.1         0.8         0.11           0.02         2.6         4.8         0.4         0.9         0.1         0.9         0.10           0.93         2.9         2.2         4.1         0.9         0.1         0.9         0.10	-82	0.42	1.1	1.2	6.0	6.0	0	06.0	0.10	0,1	0.10
0.66         5.5         0.2         0.3         0.1         0.9         0.10           0.22         3         0.9         2.9         0.1         0.9         0.10           0.02         1.4         1         0.7         0.9         0.1         0.90           0.01         0.5         0.7         2         0.9         0.1         0.90           0.02         0.5         10         4.3         0.9         0.1         0.90           0.02         2.6         4.8         0.4         0.1         0.9         0.11           0.01         1.9         5.4         0.5         0.1         0.9         0.11           0.01         1.9         5.4         0.5         0.1         0.9         0.11           0.44         2.6         1.2         4.1         0.9         0.1         0.8           0.93         29.2         0.2         5.1         0.1         0.9         0.10           1.76         77         1.2         7         0.1         0.9         0.10           0.86         7.3         2.3         0.4         0.9         0.1         0.90           0.02	181	0.44	2.9	0,4	0.1	0.1	0.0	0.10	06.0	6'0	0.00
0.22         3         0.9         2.9         0.1         0.9         0.10           0.02         1.4         1         0.7         0.9         0.1         0.90           0.01         0.5         0.7         2         0.9         0.1         0.90           0.02         0.5         10         4.3         0.9         0.1         0.90           0.02         2.6         1.2         4.1         0.1         0.9         0.11           0.01         1.9         5.4         0.5         0.1         0.9         0.11           0.01         1.9         5.4         0.5         0.1         0.9         0.11           0.44         2.6         1.2         4.1         0.9         0.1         0.8           0.93         29.2         0.2         5.1         0.1         0.9         0.10           1.76         77         1.2         7         0.1         0.9         0.10           1.76         7.3         2.3         0.4         0.9         0.1         0.90           0.02         1.7         0.6         0.2         0.9         0.10         0.90           0.02	89	99'0	5.5	0.2	0.3	0.1	0.9	0.10	0.90	6'0	06.0
0.02         1.4         1         0.7         0.9         0.1         0.90           0.01         0.5         0.7         2         0.9         0.1         0.90           0.02         0.5         10         4.3         0.9         0.1         0.90           0.04         2.6         1.2         4.1         0.1         0.9         0.17           0.01         1.9         5.4         0.5         0.1         0.9         0.11           0.01         1.9         5.4         0.5         0.1         0.9         0.11           0.44         2.6         1.2         4.1         0.9         0.1         0.88           0.93         29.2         0.2         5.1         0.9         0.1         0.88           1.76         77         1.2         7         0.1         0.9         0.10           1         8.1         0.4         0.9         0.9         0.1         0.90           0.86         7.3         2.3         0.4         0.9         0.1         0.90           0.02         0.9         0.1         0.9         0.1         0.90           0.02         0.9	8	0.22	3	6'0	2.9	0.1	6.0	0.10	06.0	6.0	0.00
0.01         0.5         0.7         2         0.9         0.1         0.90           0.02         0.5         10         4.3         0.9         0.1         0.90           0.44         2.6         1.2         4.1         0.1         0.9         0.17           0.02         2.6         4.8         0.4         0.1         0.9         0.11           0.01         1.9         5.4         0.5         0.1         0.9         0.11           0.44         2.6         1.2         4.1         0.9         0.1         0.88           0.93         29.2         0.2         5.1         0.1         0.9         0.10           1.76         77         1.2         7         0.1         0.9         0.10           1.76         7.7         1.2         7         0.1         0.9         0.10           0.86         7.3         2.3         0.4         0.9         0.1         0.90           0.02         0.3         0.4         0.9         0.1         0.90         0.10           0.02         0.9         0.1         0.9         0.1         0.90           0.02         0.9	2	0.02	1.4	-	0.7	6'0	0.1	06.0	0.10	0.1	0,10
0.02         0.5         10         4.3         0.9         0.1         0.90           0.44         2.6         1.2         4.1         0.1         0.9         0.17           0.02         2.6         4.8         0.4         0.1         0.9         0.11           0.01         1.9         5.4         0.5         0.1         0.9         0.11           0.01         1.9         5.4         0.5         0.1         0.9         0.11           0.93         29.2         0.2         5.1         0.1         0.9         0.10           1.76         77         1.2         7         0.1         0.9         0.10           1         8.1         0.4         0.9         0.9         0.1         0.90           0.86         7.3         2.3         0.4         0.9         0.1         0.90           0.02         1.7         0.6         0.7         0.9         0.1         0.90           0.02         0.9         0.1         0.9         0.1         0.90         0.1           0.02         0.9         0.1         0.9         0.1         0.90         0.1           0.02	5	0.0	0.5	0.7	2	6'0	0.1	0.90	0.10	0.1	0.10
0.44         2.6         1.2         4.1         0.1         0.9         0.17           0.02         2.6         4.8         0.4         0.1         0.9         0.11           0.01         1.9         5.4         0.5         0.1         0.9         0.11           0.01         1.2         4.1         0.9         0.1         0.88           0.93         29.2         0.2         5.1         0.1         0.9         0.10           1.76         77         1.2         7         0.1         0.9         0.10           1         8.1         0.4         0.9         0.9         0.1         0.90           0.86         7.3         2.3         0.4         0.9         0.1         0.90           0.02         0.7         0.9         0.1         0.90         0.1         0.90           0.02         0.9         0.1         0.9         0.1         0.90           0.02         0.9         0.1         0.90         0.1         0.90	뒤	0.02	0.5	0	4.3	6.0	0.1	06'0	0.10	0.1	0.10
0.02         2.6         4.8         0.4         0.1         0.9         0.11           0.01         1.9         5.4         0.5         0.1         0.9         0.11           0.44         2.6         1.2         4.1         0.9         0.1         0.88           0.93         29.2         0.2         5.1         0.1         0.9         0.10           1.76         77         1.2         7         0.1         0.9         0.10           1.76         7.7         1.2         7         0.1         0.9         0.10           0.86         7.3         2.3         0.4         0.9         0.1         0.90           0.37         3.3         1         5.1         0.1         0.9         0.10           0.02         0.9         0.4         0.9         0.1         0.90           0.02         0.9         0.1         0.90         0.1         0.90	99	0,44	2.6	1.2	4.1	0.1	6'0	0.17	0.83	6.0	0.83
0.01         1.9         5.4         0.5         0.1         0.9         0.11           0.44         2.6         1.2         4.1         0.9         0.1         0.88           0.93         29.2         0.2         5.1         0.1         0.9         0.10           1.76         77         1.2         7         0.1         0.9         0.10           1.76         7.3         1.2         7         0.1         0.9         0.10           0.86         7.3         2.3         0.4         0.9         0.1         0.90           0.37         3.3         1         5.1         0.1         0.9         0.10           0.02         0.9         0.4         0.9         0.1         0.90           0.02         0.9         0.1         0.90           0.02         0.9         0.1         0.90	9	0,02	7.6	4.8	0,4	0.1	6'0	0.11	0.89	6.0	0.89
0.44         2.6         1.2         4.1         0.9         0.1         0.88           0.93         29.2         0.2         5.1         0.1         0.9         0.10           1.76         77         1.2         7         0.1         0.9         0.10           1         8.1         0.4         0.9         0.1         0.90           0.86         7.3         2.3         0.4         0.9         0.1         0.90           0.37         3.3         1         5.1         0.1         0.9         0.10           0.02         0.9         0.4         0.9         0.1         0.90           0.02         0.9         0.1         0.90           0.02         0.9         0.1         0.90	66:	0.01	61	5.4	0,5	0.1	6.0	0.11	0.89	6'0	0.89
0.93         29.2         0.2         5.1         0.1         0.9         0.10           1.76         77         1.2         7         0.1         0.9         0.10           1         8.1         0.4         0.9         0.1         0.90           0.86         7.3         2.3         0.4         0.9         0.1         0.90           0.37         3.3         1         5.1         0.1         0.9         0.10           0.02         1.7         0.6         0.2         0.9         0.1         0.90           0.02         0.9         0.4         0.7         0.9         0.1         0.90	997	0.44	2.6	1.2	4.1	6.0	0.1	0.88	0,12	0.1	.0.12
1.76         77         1.2         7         0.1         0.9         0.10           1         8.1         0.4         0.9         0.9         0.1         0.90           0.86         7.3         2.3         0.4         0.9         0.1         0.90           0.37         3.3         1         5.1         0.1         0.9         0.10           0.02         1.7         0.6         0.2         0.9         0.1         0.90           0.02         0.9         0.1         0.9         0.1         0.90	3.75	0.93	29.2	0.2	5.1	0.1	6'0	0.10	06'0	6.0	0.90
1         8.1         0.4         0.9         0.9         0.1         0.90           0.86         7.3         2.3         0.4         0.9         0.1         0.90           0.37         3.3         1         5.1         0.1         0.9         0.10           0.02         1.7         0.6         0.2         0.9         0.1         0.90           0.02         0.9         0.1         0.90         0.1         0.90	8	1.76	77	1.2	7	1.0	0.0	0.10	0.90	6.0	0.00
0.86         7.3         2.3         0.4         0.9         0.1         0.90           0.37         3.3         1         5.1         0.1         0.9         0.10           0.02         1.7         0.6         0.2         0.9         0.1         0.90           0.02         0.9         0.1         0.90         0.1         0.90	.56	-	8.1	9.4	6.0	6'0	0.0	06'0	0.10	0.1	0.10
0.37         3.3         1         \$.1         0.1         0.9         0.10           0.02         1.7         0.6         0.2         0.9         0.1         0.90           0.02         0.9         0.1         0.90         0.1         0.90	8.	0.86	7.3	2.3	0,4	6.0	0.1	06.0	0.10	0.1	0.10
0.02 0.9 0.4 0.2 0.9 0.1 0.90	4	0.37	3.3	-	5.1	0.1	6'0	0.10	0.90	6.0	0.00
0.02 0.9 0.4 0.2 0.0 0.1 0.90	6	0.02	7	9.0	0.2	6.0	1.0	06.0	0.10	0.1	0.10
0.50	.59	0.02	0.0	0.4	0,2	6.0	1.0	06.0	0.10	0.1	0,10

Page 2 of 3

Fig. 5

Prostate Cancer Prognosis Testing Data

NNoutput2 Actual Index	0 1 1 0 11	0.10 0.10	0.10 0.10	060 60 060	0.12 0.1 0.12	0.23 0.9 0.23	060 60 060	0.12 0.1 0.12	0.13 0.1 0.13	0 1 0 110	0.10 0.10	010 10 010
NNoutput	0.80	06 0	06.0	0.10	0.88	0.77	010	0.88	0.87	68 0	06.0	18.0
Progress	0	0	0	6.0	0.1	6.0	6.0	0.1	0.1	0	0	-
Stable	6.0	6.0	6.0	0	6.0	0	0	6.0	6.0	6.0	6.0	0
Testosterope	1.4	9.0	8.0	5	0.1	9'0	3.9	0.7	0.7	0.5	1.5	99
CKA	Ī	1.3	2.2		1.8	1.1	0.5	2.3	2.2		0.1	6.0
PAP	2.3	7	1.9	3.4	0.3	0	51.7	-	=	1.3	9.0	2.2
PSA	0.15	0.05	0.29	0.37	0.0	0.42	9.0	٥	0.05	101	0.03	0.25
nTPS	0.39	0.9	0.43	0.63	0.52	1.33	0.76	964	63	-	0.7	0.42

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0.1	5	0	00	0	5	-	,	9	270	-	2
0.10	110	-	000	01.0	010	0.0		0.10	0.50	0.10	0.10
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6.0	00	000	6	00	00	200		7-0	000	0.0	000
0.3	0.3	90	800	0.4	- C	× 0	-	4 6	0.4	0.5	0.1
0.3	0.1	=	S	1.8	0.5	90	90	-	0,7	2	0.5
-		9,0	12.1	5.1	0.4	0.7	-	3.8	0.3	8:	0.2
0.02	0.01	0.01	1.28	0.15	0.0	0.04	0.01	0.43	0.04	0.03	10.0
0.44	0.45	0,89	1.73	1.83	0.82	0.62	0.35	1.06	0.25	0.11	0.74

Fig. 6

GROUP	က	က	က	က	-	5	က	က	-	3	-	-	က	-	-	1	-	-	-	1	-	-	-	-	-	က	က	-	-	-	-	-	-	-	-: <b>-</b> : <b>-</b>	- -	-
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DRE	3	3	က	3	2	2	က	က	2	3	2	2	3	-	1	2	2	-	-	2	2	7	1	2	7	-	3	2	7	2	2	-	2	2	Nic	7	7
TOTAL CK	61.4	244.1	132.3	349.1	118.1	287.6	105.7	80.2	89.1	46.2	84	109.8	232.1	59.4	49.8	98.8	66.2	65.3	79.1	94.1	7.702	84.5	414.1	68.7	250.4	82.4	58.6	154.2	94.2	130.5	101.6	94	82.7	143.6	6.14 6.14	4.00	34.7
CKMM	54.5	239.7	131.8	344.3	116.3	285.9	100.9	7.97	87.1	46.2	84	107.2	229.3	57.2	47.8	95.2	65.1	63	75.9	93.1	2007	82.2	408.4	65.2	246.2	8	55.8	151.5	89.6	126.9	97.5	91.7	78.4	140.3	90.6	- 20	53.6
CKMB	9	4.4	0	2.3	1.2	0	2.6	2	1.5	0	0	1.8	2.8	4.4	2	5.6		2.3	2.3	0	6.9	1.9	5.7	2.6	3.1	2.4	7	2.7	က	2.8	3.6	2.3	3.6	2.6	3.2	4.4	0
CKBE	6.0	0	0.5	2.5	9.0	1.7	2.2	1.5	0.5	0	0	0.8	0	0.8	0	~	0	0	6.0	-	9.0	0.4	0	6.0	1.1	0	0.8	0	1.6	0.8	0.5	0	0.7	0.7	0.5		-
PAP	1.59	0.57	0.88	1.26	0.7	0.29	8.31	0.98	0.55	0.75	3.14	0.24	1.8	0.63	1.08	0.88	1.25	1.01	0.94	1.23	-	1.3	0.99	1.49	4.14	1.32	1.03	1.21	1.15	3.72	1.42	1.08	1.04	0.59	1.04	1.56	1.6
PSA	12.24	6.17	7.8	54.84	4.0	0.52	117.25	7.22	2.17	54.04	5.1	1.5	21.42	0.93	2.31	1.04	0.86	3.81	1.93	96.0	1.46	3.23	0.56	6.78	28.62	8.7	4.85	1.31	1.59	5.84	3.45	1.88	2.85	9.0	3.32	4.0	1.08
AGE	72	61	73	29	62	70	72	80	99	88	77	37	76	74	29	99	67	78	57	43	70	9	20	9	89	54	73	99	72	89	84	63	70	7	69	8	69
Ω	2	က	7	8	=	27	36	17	45	20	55	63	7	73	77	80	8	82	91	86	115	132	135	137	138	139	140	160	168	179	187	198	200	205	208	213	214

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Fig. 6

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5	179.2	53	80	54.7	46.9	97.7	160.2	1454.6	229.1	192.3	467.1	290.2	466.3	480	371.9	146.5	232	104.8	281	424.8	241	206.7	157.7	144.2	140.9	134.0	141.7	9	129.0	123.9	190.0	93.6	S .	7.71	256.2	200.7
29.7	177.8	50.7	77.7	52.8	44.5	93.9	154.7	1452.1	228.3	190.7	460.8	288.3	463	479	368.1	145.6	230.1	104.8	558.8	420.5	235.4	201	153.1	141.9	137.6	130.2	137.2	91.8	126./	119.3	184.3	06	402.9	116.6	091	707
7.7	4.6	2.3	4.	1.4	1.5	3.8	4.6	1.5	8.0	1.6	6.3	1.9	3.3	-	2.8	0	1.9	0	2.2	3.2	5.6	4.8	3.5	2.3	2.2	3.1	3.4	3.1	1.6	3.8		2.8	2.1	9.0	8.0	4.0
). O	0	0	6.0	0.5	6.0	0	6.0	-	0	0	0	0	0	0	-	6.0	0	0	0	1.1	0	0.0	-	0	1.1	5.		-		0.8	0	0.8	0	0		6.0
1.//	4.5	3.79	1.57	2.98	1.04	0.92	2.7	0.94	0.97	0.95	1.31	-	=	1.05	0.97	1.36	0.84	0.84	1.57	1.28	0.48	0.87	5.09	1.46	1.54	1.09	1.67	1.12	1.27	1.26	က	1.24	0.83	0.73	0.74	1.81
1.92	50.91	24.41	20.44	4.73	2.14	4.59	5.63	0.74	0.54	0.67	0.4	0.56	1 08	113	0.86	8.03	0.71	4.0	1.4	1.19	1.82	1.92	2.48	3.29	6.0	0.4	4.12	2.77	1.86	1.62	3.04	9.0	4.0	1.18	1.1	1.06
72	55	83	8	89	90	78	92	48	23	37	38	3 2	4	48	47	52	47	47	58	73	83	20	26	88	62	72	99	99	89	88	8	92	31	39	30	49
20	245	747	283	84	200	27.0	78	208	25	217	7 2	225	257	770	- 050	331	134	337	340	347	350	351	355	358	361	363	368	370	373	380	286	387	380	301	392	396

Fig. 6

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4	4	4	4	4	4	4	4	4	4	4	4	4	4	4	4	4	4	4	က	က	3	-	2	က	2	0	8			- -		-	-	-	- -	- -	7
198.5	207.3	311.2	862.7	312.3	231.9	121.1	145.1	146.8	131.5	116.2	113.8	421.1	205.2	283.5	137.8	300.4	365.8	251.1	159.9	127.8	131.6	132.9	63.1	386.9	29.1	88	80.7	109.5	114	288.2	182.6	120.7	233.5	222.1	141.4	60.5	343.1
191	206.7	307.9	860.5	309.3	226.5	120.4	142.9	145.6	129.8	114	111.1	412.8	200.9	279.8	137	297.1	365.2	251.1	157.1	125.2	126.2	130.2	62.4	380.3	58.6	97.7	77.3	106.8	110.8	283.6	177.2	116.9	227.7	217.9	137.3	57.2	334.2
4.5	9.0	2.8	8.	2.5	4.4	0.7	2.2	1.2	1.7	2.2	2.7	8.3	4.3	3.2	8.0	2.9	0	0	2.8	6.7	4	1.9	0	5.1	0	0	5.6	1.6	3.2	3.3	4.7	3.1	3.9	2.6	ပ	1.9	7.4
-	0	0.5	0.4	0.5	-	0	0	0	0	0	0	0	0	0.5	0	4.0	9.0	0	0	0.7	1.4	0.8	0.7	1.5	0.5	0.3	0.8	1.1	0	1.3	0.7	0.7	1.9	1.6	1.1	1.4	1.5
0.86	0.87	0.92	1.08	0.85	14.1	0.74	1.34	1.05	1.38	0.47	0.77	1.65	1.78	1.12	0.92	2.23	1.23	1.53	0.48	0.86	1.17	0.58	7.17	21.21	0.91	1.03	1.03	0.99	1.39	0.82	1.28	1.19	0.58	1.39	0.94	1.12	1.13
1.8	4.0	4.0	0.71	1.39	0.58	0.4	0.4	0.4	0.4	4.0	4.0	1.3	0.65	0.93	3.01	0.62	9.0	0.4	0.65	6.65	13 93	181	908	86.59	5.19	7.16	62.6	6.2	6.85	0.67	3.18	261	0.55	0.73	0.53	1.23	1.35
51	33	31	33	37	37	29	38	77	28	43	28	28	59	57	46	26	28	200	12	102	83	62	88	2	44	59	82	52	11	6	65	47	52	20	53	47	48
399	401	402	403	407	408	409	412	413	414	420	425	426	429	432	434	438	440	445	72.4	455	458	458	486	200	470	471	477	479	495	501	502	507	208	300	511	515	518

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234.7	380.7	132.7	306.5	287	185.2	218.1	214	146.4	4.00	146.3	900	007	145.0	119.0	189	118.4	162.3	208.9	168.1	104.7	231.2	156.4	211.5	473.4	171.4	96.9	361.6	111.2	63.9	6.16	182.5	163.3	87.6	57.9	54.3	155.9	64.6	72
243.0	374.5	130.6	301.4	277.9	181.6	2126	203	120.2	139.3	138.2	193.2	202.9	136.7	117	182.9	115.4	159	203	165.2	101.3	225.9	152	209.3	470.2	169.7	93.3	356.6	107.8	9.09	88.3	178.6	153.7	85.7	54.5	51.7	150.1	62.6	RO A
3.2	5.4	2.1	4	1.6	2.8	2	20,4	7.0	2.0	2.7	3.7	2.2	7.2	1.7	5.1	2.1	2.4	5.4	1.6	2.7	3.3	3.4	2.2	3.2	1.7	6	2	2.1	2.6	2.5	3.9	7.2	1.9	2.5	1.9	5.4	7	٦
4:	0.8	0	-	0		20	200	9	1.2	7-	=	6.0	1.7	0.0	-	0.0	6.0	0.5	1.3	0.7	2	1	0	0	0	9.0	0	1.3	0.7	1.1	0	2.4	0	6.0	0.7	0.4	0	0
0.98	6.0	0.88	-	160	9	200	1.02	01.1	1.47	1.5	0.61	0.56	1.26	0.85	99.0	0.92	0.88	0.97	1.31	1.18	1.28	0.77	0.55	5.98	1.05	2.26	1.04	0.72	1.26	1.14	1.33	16.43	1.74	0.82	3.13	117	6.	
0.71	0.86	160	4 18	3 5	200	0.02	10	1.06	12.45	10.42	1.5	0	3.84	0.89	0.55	0.58	4.01	1.12	0.95	1.59	5.65	1 98	12	273	5.45	8.59	7.55	0.4918	20.54	7.39	7.6	65.87	16.38	8.8	20 78	11 57	10.58	3
43	48	47	= =	10	3 5	3	8	2	73	64	8	62	76	8	67	28	5	62	8	5.4	187	25	2 2	76	66	61	73	72	88	200	8	3 8	75	7	17	11	2	3
518	240	200	250	070	200	533	240	542	543	548	549	557	559	580	270	572	575	578 578	Sas	205	200	200	600	95.F	667	670	676	283	682	A A A	200	200	200	400	3 3	5 5	3 5	) (0/

Fig. 6 Page 5 of

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	49.3	000	39.8		143.4		125.8		102	
	44.5		36.6		138.8		1236		1012	
	23		2.7		2 4		<u>۔</u>		0	0.0
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	68 79		2 14		78 S.4	10:01	α C	2	7 04	5.4
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	67	5	77		72	2	60	3	3	ຊ
	725	200	756	02/	-	- <b>20</b> /		99/		768

HTI ID:	AGE:	PSA	PAP	CKBB:	CKMB.	CKMM	DRE	GROUP!	STAGE	ProstAsure
541	42	1.91:	0.92	0:	1.5	295.3	enlarged	11		10.4
544	76	4.67:	2.18	1.4	2.7	109.41	enlarged	1		30.1
545	58	1.71	1.28	0.6	2.1	76.8	enlargedi	1		24.2
547	48	0.9	0.9	0!	3.9	156.4	enlarged	1		12.6
550	52	1.28	0.69	0	2.3	107.1	enlarged	1		21.8
551	71	1.23	0.72	1.6	2.8	114.5	enlarged	1		27.6
552	58	14.76	1.79	1	7.3	280	enlarged	1		41.3
555	75	5.74	11	0.7	1.7;	132	enlarged	1		41.8
556	84	4.46	1.06	1.1	3.3	108.3	enlarged	1		39.8
558	41	1.28	0.77	1.3	5.2	269.2	enlarged	1		9.9
561	62	4.23	0.63	1.4	4.5	216.5	enlarged	1		29.9
562	47	0.55	0.74	0.4	2.1	176.3	enlarged	1		10.9
563	70	0.74	1.08	0.7	4.3	164	enlarged	1		17.1
564	79	1.6	0.84	0.9	4.7	176.3	enlarged	1		25.2
567	59	1.52	1.33	1.1	4.1:	308.81	enlarged	1		10.3
568	61	1.64	0.87	0.7	3.3	84.1	enlarged	1		28.1
569	86	0	0.73	0.5	10.1.	557.6	enlarged	1		11.1
571	53	0.77	0.79	0	1.5:	178	enlarged	1		12.9
573	66	0.7	1	1.1	2.1	96.2	enlarged	11		22.2
574	67	2.22	1.37	0.7	1.8	39.61	enlarged	1		33.2
576	38	0.52	0.64	0	2.1	70.9	enlarged	1		15.3
577	62	0	0.57	0.3	9.1	529	enlarged	1		8.3
580	67	1.05	0.941	0	12.5	382.7	enlarged	1		10.7
581	70	2.88	0.92	0	3.4	118.2	enlarged	1		32.8
582	65	1.53	0.87	0.6	3.2	104.9	enlarged	1		27.0
583	65	3.03	1.33	1.1	3.4	117	enlarged	1		27.3
584	65	0.78	0.72	0	3.4	209.4	enlarged	1	· .	14.8
585	67	3!	1.26	0	2.8	120.9		1		28.9
587	61	1.18	1.05	1.6	<b>O</b> ;	104.1	enlarged	1		21.2
588	75	6.5;	1.87	0	1.2	61.7		1		44.5
589	70	1.57	1.05	1.1	3.4	194.8		1		18.5
590	77	11.33;	1.11	0	6	237.5		1		49.4
591	64	2.31	1.5	0	2.6	231.2		1		15.1
592	74	5.96	1.46	0.6	5.5	147.3		1		36.4
593	62	3.16	0.92	1.3	1.6	93.3		1		33.4
594	70	9.49	0.71	1	2.6	114.9		1		57.9
596	67	4.09	0.93	0.6	1.8	116.3	enlarged	1		36.7
597	45	1.76	0.72	1.2	12.2	98.5		1	<u>.</u>	21.4
598	61	. 0	0.44	0	1	139.5		1		18.7
600	57	1.56	0.78	0	2	99.8		1	<del></del>	
601	64	4.75	1.47	0.7	5.9	304		1		
602	64	1.18	1.29	1.2	4.5	121.7		1		18.7
603	59	1.79	1.01	0.4	3.6	176.7		1	<del></del>	
604	69	1.45	1.93	0.8	1.9	41.6	enlarged		1	26.0
605	67	2.13	1.19	1	1.3		enlarged	1		27.4 36.5
606	83	2.38	1.59	0.4	3.2		entarged			
607	68	2.41	1	1.1	4.3		enlarged			24.6
608	59	1.46	0.64	0.6	1.6		enlarged			29.5
610	59		0.94	0.7			enlarged			13.6
611	59		0.79	0.7	3.4		enlarged			13.3
612	68		0.79				: enlarged		<u> </u>	19.0
613	70	4.3	1.47	0.8	3.8	401	enlarged			19.6

Fig. 7
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614	58_	5.02	4.19	0.6	4.1	199.4	enlarged	1	• 19.4
615	66	1.29	1.17	0.8	1.6	89.3	enlarged	11	25.0
616	58	1.52	0.97	1.4	5.8	154.2	enlarged	1	18.1
617	65	6.52	2.01	0.9	4.6	268.2		1	23.9
618	62	5.47	0.92	0.9	4.1	208.7	enlarged	1	31.8
619	61	4.48	1.09	0.9	2.1	104.9:		1	35.4
620	62	0.83	0.92	1.5	7.1	403.9		1	9.8
621	70	1.53	0.86	0	4.1	218.3		1	18.0
622	63	3.31	1.21	0	3.2	3516.9	enlarged	1	16.3
623	60	3.29	1.04	0.6	3.5	169.9	enlarged :	1	24.7
624	69	2.53	1.82	0.4	9.1	353:		1	13.0
625	76	3.43	1.09	0.9	3.1	96.8	enlarged.	1	36.7
626	70	2.35	1.15	0.8	4.1	240.71	enlarged	1:	17.8
627	49	0.68	0.9	0.7	4.1	400.5	enlarged	1	7.9
628	62	2.02	0.94	0.8	1.7	108.5	enlarged	1	27.1
629	76	1.85	1.23	0.8	3.9	9.5	enlarged	1.	38.4
630	49	0.81	0.84	0.9	2.3	137:	enlarged.	1	14.5
631	51	1.01	1.14	0.3	2	83.6	enlarged	1	18.4
632	59	1.65	0.69:	1.8	2	129.6	enlarged	1	24.2
633	61	0.76	0.78	0.6	2.6	129.4	enlarged	1	19.8
634	83	1.54	1.01	8.0	3.1	165.2	enlarged	1	25.0
635	46	0.72	0.59	0.8	1.7	168.8		1.	13.0
636	78	13.2	2.86	1.4	9.2		enlarged	1.	34.8
637	78:	4.37	1.35	0	2.5	85.3	enlarged:	1:	39.9
639	70	4.74	1.37	1:	2.9	65.8	enlarged	1	39.7
640	54	1.06	1.2	0.8	2.1	126.9	enlarged!	1	15.5
641	63	4.54	1.57	1.6	6.5.	198.4	enlarged	1	23.0
642	55	4.4	2.21	0.6	3.3	171.1	enlarged	1	20.3
643:	84	1.76	0.82	0.8	2.1	181.7	enlarged	1	· 26.4
644	71:	1.68	1.22	1.1	2.6	72.5	enlarged	1:	29.5
645	62,	1.92	0.72	0	3.7		enlarged	1	13.8
646:	68	3.27	1.71	0.9.	2.5	120.8	enlarged	1	26.2
647	45	1.39	0.68	1.3	2.6	122.6	enlarged	1	18.7
648	61	2	0.97	1.3	2.5	140.5		1:	22.7
649	74	0.82	0.85	0.8	3.9	184	enlarged	1:	19.0
650	67:	3.04	1.51	0.9	8.9	426.3		1:	15.1
651	76	0.83	0.93	0	9.5.	248.71		<u> </u>	13.8
866	52	1.02	1	0.8:	1.7	157.4	enlargedi	1	14.0
867	73	2.93	1.02	1.9	2.7	120	enlarged	1	31.3
868	59	0.63	0.64	0.8	0.9	69.7	enlarged	1	26.2
869	68	4.42	1.27	0.9	2	84.4	enlarged	1	37.5
870	67	2.55	0.74	0.9	2.5	106.3	enlarged	11	33.7
871	67	0.76	0.75	1	2	81.5	enlarged	1	27.5
872	43	0.86	1.03	0.6	10.3	232	enlarged	1	8.6
873	64	1.72	1.5	1.5	2.2		enlarged	1	20.1
874	55	1.21	1.35	0.9	6.7·		enlarged	1	10.8
875	61	2.3	0.93	0.3	2.7		enlarged	1	13.9
876	78	12.61	0.84	0,	1.5		enlarged	1	67.2
877	61	1.2	0.83	0.8	2.1:		enlarged	1i	18.3
878:	70	1.94	1.03	0.7	2.4		enlarged	1	28.8
879	75	0.74	0.66	0	2.7		enlarged	1:	24.9
880	65	1.94	0.91:	0.5	1.8		enlarged	1.	28.9
881	66	3.51	0.87	1	1.6	64.4	enlarged <sup>,</sup>	1:	39.9

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882	69	5.46	1.57	0.7	2.5	105.4	enlarged	1		36.8
883	63	12.21	2.88	1.9	2.9	191.8	enlarged	1		36.3
884	62	4.27	1.53	0.8	3.8	142.8	enlarged	1		27.3
885	59	2.38	0.76	0.8	1.7	87.7	enlarged	1		31.9
886	61	3.56	1.08	1.8	1.5	87.9	enlarged	1		32.6
887	66	0.72	0.85	1.1	2.9	192.1:		1		15.2
888	65	0.86	0.91	1	3.2	129.1		1		20.4
889	78	0.69	1.13	1.5	4.3	132.7		1		20.8
99999	70	5.25	1.44	0.8	4.8	226	enlarged	1		26.9
638*	65	1.54	0.95	1.1	3.6	74.5	enlarged	<del> </del>		29.0
661	83	1.48	2.7	1.8	1.7	60.1	normal	3	Α	22.5
663	73:	41.76	5.08	0.8	2.5	148.8	normal	3	$\frac{1}{A}$	56.3
664	71	1.83	0.99	0	2.2	103.9	normal	3	A	29.9
673	72	4.88	0.8	0.4	2.1	168.5	normal	3	$\frac{\Lambda}{\Lambda}$	37.5
675	65	0	1.22	0	1.5	120.7	normal	3	$\frac{\Lambda}{A}$	
680	70	0	0.72	2.4	2.1	262.6	normal	3.		15.5 10.2
772	76	2.28	1.14	0.9	1.9	86	normal	3	A	
773	77	7.41	0.87	1.1	4	139.8	normal	3	A	33.4 47.3
774	58	1	0.91	0.7	2.8	119.5	normal	3	A	
775	85	1.03	1.59	0.6	2.5	120.2	normal	3	A:	19.6
897	71	1.14	0.75	0	1.8	185.6	normal	3	A ·	22.9
898	71	1.1	0.45	<del></del>	18.3	857.6	normal	3	A	20.6
899	74	12.3	2.89	1,	2.3	192.4	normal	3	A .	14.3
900:	59:	0	0.86	0.6	3.3	131.8	normal	3		40.3
901	73	22.96	1.75	0.9	2.9.	131	normal	3;	A .	14.6
902.	67	0.87	1.15	0.5	2.9:	113.7	normai	3; 3i	<u>A</u> :	61.9 21.1
903	71	3.06	1.02	0.6	2:	181.7	normal	3	A:	
904:	72	2.98	1.79	1.9:	1.8	74	normal	3	A:	26.6 28.6
905	76.	1.24	0.9	1.6	3.2	124.1	normal	3	A:	26.2
906	80	8.65	1.5	1.2	1.2	53	normal	3	A:	51.4
907	71:	20.29	2.34	0.4	2.3	114.6	normal	3	A	57.5
908	67	0.59	0.8	0	3.1	120.8	normali	3:	A	22.2
909	75.	2.47	1.38	1:	4	99.2	normal	3	A	29.9
910	74	45.34	3.43	1.2	2.4	90	normal	3:	A.	64.6
911	70:	0	0.75	1.1	2.7	168.8	normal	3	A	16.1
.912	72:	1.05	0.71	0.6	2	147.9	normal	3:	Ai	24.8
913	81	3.13	0.96	0.9	2.3	106.8	normal	3	A:	37.1
914	66	16.73	2.49	0.4	2.4	138.8	normal	3	A!	50.8
683	79 2	289.79	30.44	1	10	414.4	В	3	В:	49.0
684	82	75.19	6.07	1.2	4.4	49.5	В	3	В	66.1
685	84	5.52	1.81	1	4.5	100.1	В	3	В	37.4
688	79	35.32	11.91	1.4	2.7	189.5	В	3	В	43.3
689	79	11.79	0.94	0	3.1	227.6	В	3	B	54.2
691	79	10.7	1.11	0.8	2.6	102	В	3	Bi	56.8
692	81	6.57	1.24	1.1	21	61.5	В	3	B!	48.1
693	77	7.25	1.29!	11	4	154.7	В	3	Bi	41.2
695	79	4.85	1.24	1.9	6.8	159.8	В	3	B:	33.1
696	60	4.09	0.87	1:	2.9	260.4	В	3	B	22.8
697	68:	7.76	1.17:	1.9	1.7.	87.7	B	31	B	46.3
698	68.	14.22	1.1.	1	3.1	160.1	В	3	В	57.7
699	72:	20.32	3.35	0	2.4	203	B	3	В.	47.3
702i	73	24.75	2.36	1:	1.9	143.8	B:	3	В	56.8
704	70	23.2	2.91	0.8	2.1	137.6	B <sup>1</sup>	3:	В.	53.7
					<del>:</del>			<del></del>		

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TOS											
T08	705	72	143.58	7.26	1.1	3.1	138.1	В			
T09	706	66	2.76	1.2	1.3	2.8	149.4	В		B	24.6
T10	708	67	7.95	1.47	0.6	2.7	73.9	В	3		47.9
710         65         4.85         1.08         0.7         2.7         111.8         B         3         B         37.5           789         69         2.03         0.78         0.7         1.8         73.7         B         3         B         35.2           790         57         3.73         1.33         0.7         3.8         124         B         3         B         27.0           791         76         6.73         1.12         0.9         2         48.2         B         3         B         27.0           792         76         28.64         2.5         0.5         1.8         87.4         B         3         B         64.3           793         78         6.22         2         1.3         3.5         117.5         B         3         B         35.5           794         44         3.1         1.9         4.7         13.25         B         3         B         27.0           795         72         1.63         1.7         1.1         1.2         2.17.8         B         3         B         46.1           797         75         10.43         2.84 <td>709</td> <td>68</td> <td>4.92</td> <td>0.98</td> <td>0</td> <td>1.8</td> <td>121.5</td> <td>В</td> <td>3</td> <td>В</td> <td>39.3</td>	709	68	4.92	0.98	0	1.8	121.5	В	3	В	39.3
T89	710	65			0.7	2.7	111.8	В	3	В	37.5
T90	789				0:7	1.8	73.7	В	3	В	35.2
791         76         6.73         1.12         0.9         2         48.2         B         3         B         50.8           792         76         28.64         2.5         0.5         1.8         87.4         B         3         B         64.3           793         78         6.22         2         1.3         3.5         117.5         B         3         B         35.6           794         64         3.71         1.3         2.9         4.7         132.5         B         3         B         24.0           795         72         11.63         1.71         1.1         2.2         178.7         B         3         B         46.9           797         75         10.43         2.84         0.7         4.8         113.6         B         3         B         64.9           799         63         6.8         0.82         0.6         6.7         247.3         B         3         B         51.0           799         63         6.8         0.82         0.6         6.7         247.3         B         3         B         35.1           799         63         6.8 <td></td> <td>27.0</td>											27.0
792         76         28,64         2.5         0.5         1.8         87.4         B         3         B         64.3           793         78         6.22         2         1.3         3.5         117.5         B         3         B         35.6           794         64         3.71         1.31         2.9         4.7         132.5         B         3         B         46.1           796         72         11.63         1.71         1.1         2.2         178.7         B         3         B         46.1           796         65         17.996         1.37         1.3         2.4         52.7         B         3         B         46.9           797         75         10.43         2.84         0.7         4.8         113.6         B         3         B         49.1           799         63         6.8         0.82         0.6         6.7         247.3         B         3         B         51.0           800         73         22.16         1.24         0.6         2.5         73.3         B         3         B         71.0           801         73											
793         78         6,22         2         1,3         3,5         117.5         B         3         B         35.6           794         64         3,71         1,31         2.9         4,7         132.5         B         3         B         27.0           795         72         11,63         1,71         1,1         2,2         178.7         B         3         B         46.1           796         65         17.96         1,37         1,3         2,4         52.7         B         3         B         64.9           797         75         10,43         2,84         0.7         4,8         113.6         B         3         B         64.9           798         74         4,123         38.48         0.5         3.8         94.9         B         3         B         51.0           799         63         6.8         0.82         0.6         6.7         247.3         B         3         B         51.0           800         73         2.216         1.24         0.6         2.5         73.3         B         3         B         51.0           801         67 <th< td=""><td><del></del></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></th<>	<del></del>										
794 64 3.71 1.31 2.9 4.7 132.5 B 3 B 27.0 795 72 11.63 1.71 1.1 2.2 178.7 B 3 B 46.1 796 65 17.96 1.37 1.3 2.4 52.7 B 3 B 64.9 797 75 10.43 2.84 0.7 4.8 113.6 B 3 B 43.3 798 74 41.23 38.48 0.5 3.8 94.9 B 3 B 51.0 799 63 6.8 0.82 0.6 6.7 247.3 B 3 B 55.0 800 73 22.16 1.24 0.6 2.5 73.3 B 3 B 35.6 800 73 32.178 0.7 1.8 71.7 B 3 B 30.8 802 73 7.32 1.23 0.8 3 104 B 3 B 46.1 803 64 11.02 1.17 0.5 1 49.6 B 3 B 61.4 804 53 6.53 0.88 0 0.9 66.3 B 3 B 61.4 805 74 32.48 2.06 0.5 0.8 88.4 B 3 B 61.4 806 72 1.6 1.4 0.6 2 55.4 B 3 B 30.8 807 73 1.8 1.4 0.8 2 55.4 B 3 B 30.8 808 72 1.6 1.4 0.8 2 55.4 B 3 B 30.8 808 72 1.0 1.4 0.8 2 55.4 B 3 B 30.8 809 81 33.18 0.99 0.4 2.4 57.7 B 3 B 3 B 72.9 810 67 5.96 1.47 1.7 1.1 0.8 2.9 B 3 B 72.9 811 67 5.96 1.47 1.7 1.1 0.8 2.9 B 3 B 72.9 811 67 5.96 1.47 1.7 1.1 0.8 2.9 B 3 B 3 B 72.9 811 67 5.96 1.47 1.7 1.1 0.8 2.9 B 3 B 3 B 72.9 811 67 5.96 1.47 1.7 1.1 0.8 2.9 B 3 B 3 B 72.9 811 67 5.96 1.47 1.7 1.1 1.8 2.9 B 3 B 62.4 4 8 8 15 1.9 1 8 1 8 1 8 1 8 1 8 1 8 1 8 1 8 1 8 1											
795         72         11.63         1.71         1.1         2.2         1787         B         3         B         46.1           796         65         17.96         1.37         1.3         2.4         52.7         B         3         B         64.9           797         75         10.43         2.84         0.7         4.8         113.6         B         3         B         43.3           798         74         4.123         38.48         0.5         3.8         94.9         B         3         B         51.0           799         63         6.8         0.82         0.6         6.7         247.3         B         3         B         51.0           800         73         2.216         1.24         0.6         2.5         73.3         B         3         B         71.9           801         67         3.2         1.23         0.8         0.7         1.8         71.7         B         3         B         46.1           801         63         3.0         1.4         0.6         2.5         73.3         B         3         B <t>46.1           803         64</t>											
796         65         17.96         1.37         1.3         2.4         52.7         B         3         B         64.9           797         75         10.43         2.84         0.7         4.8         113.6         B         3         B         43.3           798         74         41.23         38.48         0.5         3.8         94.9         B         3         B         51.0           799         63         6.8         0.82         0.6         6.7         247.3         B         3         B         35.6           800         73         22.16         1.24         0.6         2.5         73.3         B         3         B         71.9           801         67         3.32         1.78         0.7         1.8         71.7         B         3         B         30.8           802         73         7.32         1.23         0.8         0.7         1.8         71.7         B         3         B         30.8           804         53         6.53         0.88         0.0         0.9         66.3         B         3         B         61.1           804 <th< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></th<>											
797.         75         10.43         2.84         0.7         4.8         113.6         B         3         B         43.3           798         74         41.23         38.48         0.5         3.8         94.9         B         3         B         35.5           800         73         22.16         1.24         0.6         2.5         73.3         B         3         B         31.8         71.9           801         67         3.32         1.78         0.7         1.8         71.7         B         3         B         30.8           802         73         7.32         1.23         0.8         3         104         B         3         B         46.1           803         64         11.02         1.17         0.5         1         49.6         B         3         B         46.1           804         53         6.53         0.88         0         0.9         66.3         B         3         B         49.4           805         74         32.48         2.06         0.5         0.6         88.4         B         3         B         70.5           806         72<											
798         74         41,23         38,48         0.5         3,8         94,9         B         3         B         51,0           799         63         6,8         0,82         0,6         6,7         247,3         B         3         B         35,6           800         73         32,16         1,24         0,6         2,5         73,3         B         3         B         71,9           801         67         3,32         1,78         0,7         1,8         71,7         B         3         B         30,8           802         73         7,32         1,23         0.8         3         104         B         3         B         46,11           803         64         11,02         1,17         0.5         1         49,6         B         3         B         46,1           804         53         6,53         0.88         0         0,9         66,3         B         3         B         46,1           806         72         1,6         1,4         0,6         2         55,4         B         3         B         70,5           806         72         1,6											
799 63 6.8 0.82 0.6 6.7 247.3 B 3 B 35.6 800 73 22.16 1.24 0.6 2.5 73.3 B 3 B 71.9 801 67 3.32 1.78 0.7 1.8 71.7 B 3 B 3 B 30.8 802 73 7.32 1.23 0.8 3 104 B 3 B 30.8 802 73 7.32 1.23 0.8 3 104 B 3 B 46.1 804 53 6.53 0.88 0 0.9 66.3 B 3 B 44.1 804 53 6.53 0.88 0 0.9 66.3 B 3 B 49.4 805 74 32.48 2.06 0.5 0.6 88.4 B 3 B 70.5 806 72 1.6 1.4 0.6 2 55.4 B 3 B 30.8 808 59 12.09 1.37 0.6 2.2 96.1 B 3 B 73.8 808 59 12.09 1.37 0.6 2.2 96.1 B 3 B 73.8 808 59 12.09 1.37 0.6 2.2 96.1 B 3 B 72.9 810 57 6.82 3.52 1.1 0 82.9 B 3 B 3 B 72.9 811 67 5.96 1.47 1.7 1.4 27.9 B 3 B 3 B 73.9 811 67 5.96 1.47 1.7 1.4 27.9 B 3 B 3 B 61.4 1812 62 34.72 2.04 0.9 2.4 140.5 B 3 B 63.4 815 74 91.5 0.9 2.4 140.5 B 3 B 63.4 815 74 91.5 0.9 5 0.5 3.6 108.8 B 3 B 63.4 815 74 91.5 0.9 5 0.5 3.6 108.8 B 3 B 54.6 816 74 33.25 2.46 0.4 2.7 161.8 B 3 B 63.4 815 74 91.5 0.95 0.5 3.6 108.8 B 3 B 38.0 83.6 816 77 9.85 3.13 1.6 3.3 62.7 B 3 B 38.0 83.6 816 77 9.85 3.13 1.6 3.3 62.7 B 3 B 38.0 83.6 816 77 9.85 3.13 1.6 3.3 62.7 B 3 B 38.0 83.6 816 77 9.85 3.13 1.6 3.3 62.7 B 3 B 38.0 83.6 816 77 9.85 3.13 1.6 3.3 62.7 B 3 B 38.0 83.6 816 77 9.85 3.13 1.6 3.3 62.7 B 3 B 38.0 83.6 816 77 9.85 3.13 1.6 3.3 62.7 B 3 B 38.0 83.6 816 77 9.85 3.13 1.6 3.3 62.7 B 3 B 38.0 83.6 816 77 9.85 3.13 1.6 3.3 62.7 B 3 B 3 B 34.7 88.9 83.0 B 34.0 B 3 B 34.0 B 34.						<del></del>					
800 73 22.16 1.24 0.6 2.5 73.3 B 3 B 71.9 801 67 3.32 1.78 0.7 1.8 71.7 B 3 B 30.8 30.8 30.8 30.8 30.8 30.8 30.8 30.8											
801 67 3.32 1.78 0.7 1.8 71.7 B 3 B 30.8 802 73 7.32 1.23 0.8 3 104 B 3 B 46.1 803 64 11.02 1.17 0.5 1 49.6 B 3 B 3 B 46.1 804 53 6.53 0.88 0 0.9 66.3 B 3 B 49.4 805 74 32.48 2.06 0.5 0.6 88.4 B 3 B 30.6 807 74 32.48 2.06 0.5 0.6 88.4 B 3 B 30.6 807 74 25.37 0.72 0.3 0 46.4 B 3 B 3 B 70.5 806 72 1.6 1.4 0.6 2 55.4 B 3 B 3 B 70.5 808 59 12.09 1.37 0.6 2.2 96.1 B 3 B 3 B 73.8 808 59 12.09 1.37 0.6 2.2 96.1 B 3 B 3 B 72.9 810 57 6.82 3.52 1.1 0 82.9 B 3 B 3 B 31.9 811 67 5.96 1.47 1.7 1.4 27.9 B 3 B 3 B 31.9 811 67 5.96 1.47 1.7 1.4 27.9 B 3 B 3 B 31.9 813 69 17.22 1.27 1 1.9 62.2 B 3 B 3 B 67.4 813 69 17.22 1.27 1 1.9 62.2 B 3 B 56.7 813 69 17.22 1.27 1 1.9 62.2 B 3 B 56.0 815 74 9.15 0.95 0.3 1 120.8 B 3 B 3 B 65.0 816 74 9.15 0.95 0.3 1 120.8 B 3 B 3 B 63.4 815 74 9.15 0.95 0.3 1 120.8 B 3 B 3 B 63.6 816 74 9.15 0.95 0.3 1 120.8 B 3 B 3 B 63.6 816 74 9.15 0.95 0.3 1 120.8 B 3 B 3 B 63.6 816 74 9.15 0.95 0.3 1 120.8 B 3 B 3 B 63.6 82 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1											
802 73 7.32 1.23 0.8 3 104 B 3 B 46.1 803 64 11.02 1.17 0.5 1 49.6 B 3 B 61.4 804 53 6.53 0.88 0 0.9 66.3 B 3 B 3 B 49.4 805 74 32.48 2.06 0.5 0.6 88.4 B 3 B 70.5 806 72 1.6 1.4 0.6 2 55.4 B 3 B 3 B 70.5 806 72 1.6 1.4 0.6 2 55.4 B 3 B 3 B 70.5 808 59 12.09 1.37 0.6 2.2 96.1 B 3 B 56.7 809 81 33.18 0.99 0.4 2.4 57.7 B 3 B 56.7 809 81 33.18 0.99 0.4 2.4 57.7 B 3 B 3 B 72.9 810 57 6.82 3.52 1.1 0 82.9 B 3 B 3 B 31.9 811 67 5.96 1.47 1.7 1.4 27.9 B 3 B 3 B 67.4 813 69 17.22 1.27 1 1.9 62.2 B 3 B 3 B 67.4 813 69 17.22 1.27 1 1.9 62.2 B 3 B 56.7 814 65 12.68 1.12 0.7 1.8 65 B 3 B 66.0 814 65 12.68 1.12 0.7 1.8 65 B 3 B 63.4 815 7 9.85 3.13 1.6 3.3 62.7 B 3 B 3 B 63.4 816 7 9.85 3.13 1.6 3.3 62.7 B 3 B 3 B 33.0 8 63.4 816 7 9.85 3.13 1.6 3.3 62.7 B 3 B 3 B 33.0 8 63.6 817 69 4.2 0.95 0.5 3.6 108.8 B 3 B 3 B 33.0 8 63.6 817 69 4.2 0.95 0.5 3.6 108.8 B 3 B 3 B 32.0 818 77 9.85 3.13 1.6 3.3 62.7 B 3 B 3 B 32.0 818 77 9.85 3.13 1.6 3.3 62.7 B 3 B 3 B 32.7 6 820 54 9.46 0.38 0.5 0.3 85.6 B 3 B 3 B 32.0 82.7 6 820 54 9.46 0.38 0.5 0.3 85.6 B 3 B 3 B 65.9 821 77 5.9 0.97 0.9 2.6 125.3 B 3 B 3 B 42.2 60 8.85 13.03 0.7 2.1 819 B 3 B 3 B 32.6 823 72 7.49 1.9 0.6 3.6 149.9 B 3 B 3 B 32.6 823 72 7.49 1.9 0.6 3.6 149.9 B 3 B 3 B 32.6 822 60 8.55 13.03 0.7 2.1 81.9 B 3 B 3 B 36.5 823 72 7.49 1.9 0.6 3.6 149.9 B 3 B 3 B 36.5 823 72 7.49 1.9 0.6 3.6 149.9 B 3 B 3 B 36.5 823 72 7.49 1.9 0.6 3.6 149.9 B 3 B 3 B 36.5 823 72 7.49 1.9 0.6 3.6 149.9 B 3 B 3 B 36.5 823 72 7.49 1.9 0.6 3.6 149.9 B 3 B 3 B 36.5 823 72 7.49 1.9 0.6 3.6 149.9 B 3 B 3 B 42.2 6.0 8.55 13.03 0.7 2.1 81.9 B 3 B 3 B 42.2 6.0 8.55 13.03 0.7 2.1 81.9 B 3 B 3 B 42.2 6.0 8.55 13.03 0.7 2.1 81.9 B 3 B 3 B 42.2 6.0 8.55 13.03 0.7 2.1 81.9 B 3 B 3 B 42.2 6.0 8.55 13.03 0.7 2.1 81.9 B 3 B 3 B 42.2 6.0 8.55 13.03 0.7 2.1 81.9 B 3 B 3 B 42.2 6.0 8.55 13.03 0.7 2.1 81.9 B 3 B 3 B 42.2 6.0 8.55 13.03 0.7 2.1 81.9 B 3 B 3 B 42.2 6.0 8.55 13.03 0.5 5 1.0 8.8 B 3 B 3 B 42.2 6.0 8.55 13.03 0.5 5 1.1 82.8 B 3 B 3 B 42.2 6.0 8.55 13.03 0.5 5 1.1 82.8 B 3 B 3 B 42.2 6.0 8.55 13.03 0.											
803 64 11.02 1.17 0.5 1 49.6 B 3 B 61.4 804 53 6.53 0.88 0 0.9 66.3 B 3 B 49.4 805 74 32.48 2.06 0.5 0.6 88.4 B 3 B 70.5 806 72 1.6 1.4 0.6 2 55.4 B 3 B 30.6 807 74 25.37 0.72 0.3 0 46.4 B 3 B 73.8 808 59 12.09 1.37 0.6 2.2 96.1 B 3 B 56.7 809 81 33.18 0.99 0.4 2.4 57.7 B 3 B 3 B 31.9 810 57 6.82 3.52 1.1 0 82.9 B 3 B 31.9 811 67 5.96 1.47 1.7 1.4 27.9 B 3 B 3 B 31.9 811 67 5.96 1.47 1.7 1.4 27.9 B 3 B 3 B 67.4 813 69 17.22 1.27 1 1.9 62.2 B 3 B 66.0 814 65 12.68 1.12 0.7 1.8 65. B 3 B 63.4 815 74 9.15 0.95 0.3 1 120.8 B 3 B 63.4 816 74 33.25 2.46 0.4 2.7 161.8 B 3 B 63.6 817 69 4.2 0.95 0.5 3.6 108.8 B 3 B 63.6 818 77 9.85 3.13 1.6 3.3 62.7 B 3 B 63.6 819 61 2 0.86 1 2.6 105.5 B 3 B 3.8 810 63.4 815 77 9.85 3.13 1.6 3.3 62.7 B 3 B 63.6 820 54 9.46 0.38 0.5 0.3 85.6 B 3 B 63.6 821 71 5.9 0.97 0.9 2.6 125.3 B 3 B 65.9 821 71 5.9 0.97 0.9 2.6 125.3 B 3 B 65.9 821 71 5.9 0.97 0.9 2.6 125.3 B 3 B 3.0 822 60 8.85 13.03 0.7 2.1 81.9 B 3 B 3 B 37.2 823 72 7.49 1.9 0.6 3.6 149.9 B 3 B 3 B 37.2 824 61 3.12 16.12 1.2 2.3 99.7 B 3 B 3 B 36.5 825 75 8.92 1.13 0.7 2.4 88.4 B 3 B 3 B 37.2 826 61 5.13 1.94 0.8 2.5 151.4 B 3 B 3 B 37.2 827 70 11.01 1.75 0.4 3.5 140.4 B 3 B 3 B 24.5 828 61 5.33 1.94 0.8 2.7 113 B 3 B 30.2 829 55 4.94 1.6 0.5 1.1 182 B 3 B 3 B 70.5 829 55 4.94 1.6 0.5 1.1 182 B 3 B 3 B 70.5 829 55 4.94 1.6 0.5 1.1 182 B 3 B 3 B 70.5 829 55 4.94 1.6 0.5 1.1 182 B 3 B 3 B 70.5 829 55 4.94 1.6 0.5 1.1 182 B 3 B 3 B 70.5 829 55 4.94 1.6 0.5 1.1 182 B 3 B 3 B 70.5 829 55 4.94 1.6 0.5 1.1 182 B 3 B 3 B 70.5 829 55 4.94 1.6 0.5 1.1 182 B 3 B 3 B 70.5 829 55 4.94 1.6 0.5 1.1 182 B 3 B 3 B 70.5 829 55 4.94 1.6 0.5 1.1 182 B 3 B 3 B 70.5 829 55 4.94 1.6 0.5 1.1 182 B 3 B 3 B 70.5 829 55 4.94 1.6 0.5 1.1 182 B 3 B 3 B 70.5 829 55 4.94 1.6 0.5 1.1 182 B 3 B 3 B 70.5 829 55 4.94 1.6 0.5 1.1 182 B 3 B 3 B 70.5 829 55 4.94 1.6 0.5 1.1 182 B 3 B 3 B 70.5											
804   53   6.53   0.88   0   0.9   66.3   B   3   B   49.4											
805:         74         32.48         2.06         0.5         0.6         88.4         B         3         B         70.5           806:         72         1.6         1.4         0.6         2         55.4         B         3         B         30.6           807:         74         25.37         0.72         0.3         0         46.4         B         3         B         73.8           808:         59         12.09         1.37         0.6         2.2         96.1         B         3         B         56.7           809:         81         33.18         0.99         0.4         2.4         57.7         B         3         B         56.7           810:         57         6.82         3.52         1.1         0         82.9         B         3         B         31.9           810:         57         5.96         1.47         1.7         1.4         27.9         B         3         B         31.9         44.1           812:         62         34.72         2.04         0.99         2.4         140.5         B         3         B         66.7           813:											
806   72   1.6   1.4   0.6   2   55.4   B   3   B   30.6											
807    74   25.37   0.72   0.3   0   46.4   B   3   B   73.8											
808         59         12.09         1.37         0.6         2.2         96.1         B         3         B         56.7           809         81         33.18         0.99         0.4         2.4         57.7         B         3         B         72.9           810         57         6.82         3.52         1.1         0         82.9         B         3         B         31.9           811         67         5.96         1.47         1.7         1.4         27.9         B         3         B         31.9           812         62         34.72         2.04         0.9         2.4         140.5         B         3         B         67.4           813         69         17.22         1.27         1         1.9         62.2         B         3         B         66.0           814         65         1.26         1.26         B         3         B         66.0           815         74         9.15         0.95         0.3         1         120.8         B         3         B         63.4           816         74         33.25         2.46         0.4         2.7<					0.6	2	55.4				
809         81         33.18         0.99         0.4         2.4         57.7         B;         3         B         72.9           810         57         6.82         3.52         1.1         0         82.9         B;         3         B         31.9           811         67         5.96         1.47         1.7;         1.4         27.9         B         3         B         31.9           812         62         34.72         2.04         0.9         2.4         140.5         B         3         B         67.4           813         69         17.22         1.27         1         1.9         62.2         B         3         B         66.0           814         65         12.68         1.12         0.7         1.8         65         B         3         B         66.0           816         74         9.15         0.95         0.3         1         120.8         B         3         B         54.6           816         74         9.15         0.95         0.5         3.6         108.8         B         3         B         38.0           817         69         4.2<											
810         57         6.82         3.52         1.1         0         82.9         B         3         B         31.9           811         67         5.96         1.47         1.7         1.4         27.9         B         3         B         44.1           812         62         34.72         2.04         0.9         2.4         140.5         B         3         B         67.4           813         69         17.22         1.27         1         1.9         62.2         B         3         B         66.0           814         65         12.68         1.12         0.7         1.8         65         B         3         B         63.4           815         74         9.15         0.95         0.3         1         120.8         B         3         B         54.6           816         74         33.25         2.46         0.4         2.7         161.8         B         3         B         63.6           817         69         4.2         0.95         3.6         108.8         B         3         B         38.0           818         77         9.85         3.13 </td <td>808:</td> <td>59</td> <td></td> <td></td> <td>0.6</td> <td>2.2</td> <td></td> <td></td> <td></td> <td></td> <td></td>	808:	59			0.6	2.2					
811         67         5.96         1.47         1.7         1.4         27.9         B         3         B: 44.1           812         62         34.72         2.04         0.9         2.4         140.5         B         3         B         67.4           813         69         17.22         1.27         1         1.9         62.2         B         3         B         66.0           814         65         12.68         1.12         0.7         1.8         65.5         B         3         B         63.4           815         74         9.15         0.95         0.3         1         120.8         B         3         B         54.6           816         74         33.25         2.46         0.4         2.7         161.8         B         3         B         54.6           817         69         4.2         0.95         0.5         3.6         108.8         B         3         B         38.0           818         77         9.85         3.13         1.6         3.3         62.7         B         3         B         27.6           820         54         9.46         <	809	81	33.18		0.4	2.4			3!		
812         62         34.72         2.04         0.9         2.4         140.5         B         3         B         67.4           813         69         17.22         1.27         1         1.9         62.2         B         3         B         66.0           814         65         12.68         1.12         0.7         1.8         65         B         3         B         63.4           815         74         9.15         0.95         0.3         1         120.8         B         3         B         54.6           816         74         33.25         2.46         0.4         2.7         161.8         B         3         B         63.6           817         69         4.2         0.95         0.5         3.6         108.8         B         3         B         63.6           817         69         4.2         0.95         0.5         3.6         108.8         B         3         B         63.6           818         77         9.85         3.13         1.6         3.3         62.7         B         3         B         38.0           818         71         5.9 </td <td>810</td> <td>57</td> <td>6.82</td> <td></td> <td>1.1</td> <td>0;.</td> <td>82.9</td> <td></td> <td></td> <td></td> <td></td>	810	57	6.82		1.1	0;.	82.9				
813         69         17.22         1.27         1         1.9         62.2         B         3         B         66.0           814         65         12.68         1.12         0.7         1.8         65         B         3         B         63.4           815         74         9.15         0.95         0.3         1         120.8         B         3         B         54.6           816         74         33.25         2.46         0.4         2.7         161.8         B         3         B         63.6           817         69         4.2         0.95         0.5         3.6         108.8         B         3         B         38.0           818         77         9.85         3.13         1.6         3.3         62.7         B         3         B         38.0           818         77         9.85         3.13         1.6         3.3         62.7         B         3         B         43.7           819         61         2         0.86         1         2.6         105.5         B         3         B         27.6           820         54         9.46	811	67	5.96	1.47	1.7	1.4	27.9	В			
814         65         12.68         1.12         0.7         1.8         65         B         3         B         63.4           815         74         9.15         0.95         0.3         1         120.8         B         3         B         54.6           816         74         33.25         2.46         0.4         2.7         161.8         B         3         B         63.6           817         69         4.2         0.95         0.5         3.6         108.8         B         3         B         38.0           818         77         9.85         3.13         1.6         3.3         62.7         B         3         B         43.7           819         61         2         0.86         1         2.6         105.5         B         3         B         27.6           820         54         9.46         0.38         0.5         0.3         85.6         B         3         B         65.9           821         71         5.9         0.97         0.9         2.6         125.3         B         3         B         42.2           822         60         8.85		62	34.72		0.9	2.4	140.5				
815         74         9.15         0.95         0.3         1         120.8         B         3         B         54.6           816         74         33.25         2.46         0.4         2.7         161.8         B         31         B         63.6           817         69         4.2         0.95         0.5         3.6         108.8         B         31         B         38.0           818         77         9.85         3.13         1.6         3.3         62.7         B         3         B         38.0           819         61         2         0.86         1         2.6         105.5         B         3         B         27.6           820         54         9.46         0.38         0.5         0.3         85.6         B         3         B         65.9           821         71         5.9         0.97         0.9         2.6         125.3         B         3         B         42.2           822         60         8.85         13.03         0.7         2.1         81.9         B         3         B         36.5           823         72         7.49 </td <td>813</td> <td>69</td> <td>17.22</td> <td>1.27</td> <td>1:</td> <td>1.9</td> <td>62.2</td> <td>B!</td> <td>3</td> <td></td> <td>66.0</td>	813	69	17.22	1.27	1:	1.9	62.2	B!	3		66.0
815         74         9.15         0.95         0.3         1         120.8         B         3         B         54.6           816         74         33.25         2.46         0.4         2.7         161.8         B         31         B         63.6           817         69         4.2         0.95         0.5         3.6         108.8         B         31         B         38.0           818         77         9.85         3.13         1.6         3.3         62.7         B         31         B         43.7           819         61         2         0.86         1         2.6         105.5         B         31         B         27.6           820         54         9.46         0.38         0.5         0.3         85.6         B         3         B         65.9           821         71         5.9         0.97         0.9         2.6         125.3         B         3         B         42.2           822         60         8.85         13.03         0.7         2.1         81.9         B         3         B         36.5           823         72         7.49	814	65			0.7	1.8:	65:	В			63.4
816         74         33.25         2.46         0.4         2.7         161.8         B         31         B         63.6           817         69         4.2         0.95         0.5         3.6         108.8         B         3         B         38.0           818         77         9.85         3.13         1.6         3.3         62.7         B         3         B         43.7           819         61         2         0.86         1         2.6         105.5         B         3         B         27.6           820         54         9.46         0.38         0.5         0.3         85.6         B;         3         B         65.9           821         71         5.9         0.97         0.9;         2.6         125.3         B         3         B         42.2           822         60         8.85         13.03         0.7         2.1         81.9         B         3         B         36.5           823         72         7.49         1.9         0.6         3.6         149.9         B         3         B         37.2           824         61         34.1	815	74		0.95	0.3	1 :	120.8	В		B:	54.6
817         69         4.2         0.95         0.5         3.6         108.8         B         3         B         38.0           818         77         9.85         3.13         1.6         3.3         62.7         B         3         B         43.7           819         61         2         0.86         1         2.6         105.5         B         3         B         27.6           820         54         9.46         0.38         0.5         0.3         85.6         B         3         B         65.9           821         71         5.9         0.97         0.9         2.6         125.3         B         3         B         65.9           821         71         5.9         0.97         0.9         2.6         125.3         B         3         B         42.2           822         60         8.85         13.03         0.7         2.1         81.9         B         3         B         36.5           823         72         7.49         1.9         0.6         3.6         149.9         B         3         B         37.2           824         61         3.4.12 <td></td> <td>74</td> <td></td> <td></td> <td>0.4</td> <td>2.7</td> <td></td> <td>В'</td> <td>31</td> <td>В</td> <td>63.6</td>		74			0.4	2.7		В'	31	В	63.6
818         77         9.85         3.13         1.6         3.3         62.7         B         3         B         43.7           819         61         2         0.86         1         2.6         105.5         B         3         B         27.6           820         54         9.46         0.38         0.5         0.3         85.6         B         3         B         65.9           821         71         5.9         0.97         0.9         2.6         125.3         B         3         B         42.2           822         60         8.85         13.03         0.7         2.1         81.9         B         3         B         36.5           823         72         7.49         1.9         0.6         3.6         149.9         B         3         B         37.2           824         61         34.12         16.12         1.2         2.3         99.7         B         3         B         47.6           825         75         8.92         1.13         0.7         2.4         88.4         B         3         B         53.4           826         61         5.13 <td></td> <td></td> <td></td> <td></td> <td>0.5</td> <td></td> <td></td> <td>B<sup>1</sup></td> <td></td> <td>B.</td> <td>38.0</td>					0.5			B <sup>1</sup>		B.	38.0
819         61         2         0.86         1         2.6         105.5         B         3         B         27.6           820         54         9.46         0.38         0.5         0.3         85.6         B         3         B         65.9           821         71         5.9         0.97         0.9         2.6         125.3         B         3         B         42.2           822         60         8.85         13.03         0.7         2.1         81.9         B         3         B         36.5           823         72         7.49         1.9         0.6         3.6         149.9         B         3         B         37.2           824         61         34.12         16.12         1.2         2.3         99.7         B         3         B         47.6           825         75         8.92         1.13         0.7         2.4         88.4         B         3         B         53.4           826         61         5.13         1.94         0.8         2.5         151.4         B         3         B         26.6           827         70         11.01<								B:	3	B:	43.7
820         54         9.46         0.38         0.5         0.3         85.6         B         3         B         65.9           821         71         5.9         0.97         0.9         2.6         125.3         B         3         B         42.2           822         60         8.85         13.03         0.7         2.1         81.9         B         3         B         36.5           823         72         7.49         1.9         0.6         3.6         149.9         B         3         B         37.2           824         61         34.12         16.12         1.2         2.3         99.7         B         3         B         47.6           825         75         8.92         1.13         0.7         2.4         88.4         B         3         B         53.4           826         61         5.13         1.94         0.8         2.5         151.4         B         3         B         26.6           827         70         11.01         1.75         0.4         3.5         146.6         B         3         B         70.5           829         55							105.5				27.6
821         71         5.9         0.97         0.9         2.6         125.3         B         3         B         42.2           822         60         8.85         13.03         0.7         2.1         81.9         B         3         B         36.5           823         72         7.49         1.9         0.6         3.6         149.9         B         3         B         37.2           824         61         34.12         16.12         1.2         2.3         99.7         B         3         B         47.6           825         75         8.92         1.13         0.7         2.4         88.4         B         3         B         53.4           826         61         5.13         1.94         0.8         2.5         151.4         B         3         B         26.6           827         70         11.01         1.75         0.4         3.5         146.6         B         3         B         48.0           828         61         53.63         1.69         0.8         2.7         113         B         3         B         70.5           829         55											
822         60         8.85         13.03         0.7         2.1         81.9         B         3         B         36.5           823         72         7.49         1.9         0.6         3.6         149.9         B         3         B         37.2           824         61         34.12         16.12         1.2         2.3         99.7         B         3         B         47.6           825         75         8.92         1.13         0.7         2.4         88.4         B         3         B         53.4           826         61         5.13         1.94         0.8         2.5         151.4         B         3         B         26.6           827         70         11.01         1.75         0.4         3.5         146.6         B         3         B         26.6           828         61         53.63         1.69         0.8         2.7         113         B         3         B         70.5           829         55         4.94         1.6         0.5         1.1         182         B         3         B         71.4           831         80         3.											
823         72         7.49         1.9         0.6         3.6         149.9         B         3         B         37.2           824         61         34.12         16.12         1.2         2.3         99.7         B         3         B         47.6           825         75         8.92         1.13         0.7         2.4         88.4         B         3         B         53.4           826         61         5.13         1.94         0.8         2.5         151.4         B         3         B         26.6           827         70         11.01         1.75         0.4         3.5         146.6         B         3         B         26.6           828         61         53.63         1.69         0.8         2.7         113         B         3         B         70.5           829         55         4.94         1.6         0.5         1.1         182         B         3         B         24.5           830         65         64.16         0.59         0.2         2.4         142.8         B         3         B         71.4           831         80         3											
824         61         34.12         16.12         1.2         2.3         99.7         B         3         B         47.6           825         75         8.92         1.13         0.7         2.4         88.4         B         3         B         53.4           826         61         5.13         1.94         0.8         2.5         151.4         B         3         B         26.6           827         70         11.01         1.75         0.4         3.5         146.6         B         3         B         26.6           828         61         53.63         1.69         0.8         2.7         113         B         3         B         70.5           829         55         4.94         1.6         0.5         1.1         182         B         3         B         70.5           830         65         64.16         0.59         0.2         2.4         142.8         B         3         B         71.4           831         80         3.58         0.52         0         0.9         89.8         B         3         B         46.0           832         59         17.											
825         75         8.92         1.13         0.7         2.4         88.4         B         3         B         53.4           826         61         5.13         1.94         0.8         2.5         151.4         B         3         B         26.6           827         70         11.01         1.75         0.4         3.5         146.6         B         3         B         48.0           828         61         53.63         1.69         0.8         2.7         113         B         3         B         70.5           829         55         4.94         1.6         0.5         1.1         182         B         3         B         70.5           830         65         64.16         0.59         0.2         2.4         142.8         B         3         B         71.4           831         80         3.58         0.52         0         0.9         89.8         B         3         B         46.0           832         59         17.4         0.99         0.6         3         140.4         B         3         B         66.3           833         68         790.46											
826         61         5.13         1.94         0.8         2.5         151.4         B         3         B         26.6           827         70         11.01         1.75         0.4         3.5         146.6         B         3         B         48.0           828         61         53.63         1.69         0.8         2.7         113         B         3         B         70.5           829         55         4.94         1.6         0.5         1.1         182         B         3         B         24.5           830         65         64.16         0.59         0.2         2.4         142.8         B         3         B         71.4           831         80         3.58         0.52         0         0.9         89.8         B         3         B         46.0           832         59         17.4         0.99         0.6         3         140.4         B         3         B         66.3           833         68         790.46         41.76         1.2         2.1         60.4         B         3         B         71.4           834         63         25.											
827         70         11.01         1.75         0.4         3.5         146.6         B         3         B         48.0           828         61         53.63         1.69         0.8         2.7         113         B         3         B         70.5           829         55         4.94         1.6         0.5         1.1         182         B         3         B         24.5           830         65         64.16         0.59         0.2         2.4         142.8         B         3         B         71.4           831         80         3.58         0.52         0         0.9         89.8         B         3         B         46.0           832         59         17.4         0.99         0.6         3         140.4         B         3         B         66.3           833         68         790.46         41.76         1.2         2.1         60.4         B         3         B         71.4           834         63         25.86         1.42         0.7         1.9         162.9         B         3         B         67.0           835         66         50											
828         61         53.63         1.69         0.8         2.7         113         B         3         B         70.5           829         55         4.94         1.6         0.5         1.1         182         B         3         B         24.5           830         65         64.16         0.59         0.2         2.4         142.8         B         3         B         71.4           831         80         3.58         0.52         0         0.9         89.8         B         3         B         46.0           832         59         17.4         0.99         0.6         3         140.4         B         3         B         66.3           833         68         790.46         41.76         1.2         2.1         60.4         B         3         B         71.4           834         63         25.86         1.42         0.7         1.9         162.9         B         3         B         67.0           835         66         50.54         3.02         0.8         2         38.1         B         3         B         73.1											
829     55     4.94     1.6     0.5     1.1     182     B     3     B     24.5       830     65     64.16     0.59     0.2     2.4     142.8     B     3     B     71.4       831     80     3.58     0.52     0     0.9     89.8     B     3     B     46.0       832     59     17.4     0.99     0.6     3     140.4     B     3     B     66.3       833     68     790.46     41.76     1.2     2.1     60.4     B     3     B     71.4       834     63     25.86     1.42     0.7     1.9     162.9     B     3     B     67.0       835     66     50.54     3.02     0.8     2     38.1     B     3     B     73.1					<del></del>						
830     65     64.16     0.59     0.2     2.4     142.8     B     3     B     71.4       831     80     3.58     0.52     0     0.9     89.8     B     3     B     46.0       832     59     17.4     0.99     0.6     3     140.4     B     3     B     66.3       833     68     790.46     41.76     1.2     2.1     60.4     B     3     B     71.4       834     63     25.86     1.42     0.7     1.9     162.9     B     3     B     67.0       835     66     50.54     3.02     0.8     2     38.1     B     3     B     73.1										<u>.</u>	
831     80     3.58     0.52     0     0.9     89.8     B     3     B     46.0       832     59     17.4     0.99     0.6     3     140.4     B     3     B     66.3       833     68     790.46     41.76     1.2     2.1     60.4     B     3     B     71.4       834     63     25.86     1.42     0.7     1.9     162.9     B     3     B     67.0       835     66     50.54     3.02     0.8     2     38.1     B     3     B     73.1											
832     59     17.4     0.99     0.6     3     140.4     B     3     B     66.3       833     68     790.46     41.76     1.2     2.1     60.4     B     3     B     71.4       834     63     25.86     1.42     0.7     1.9     162.9     B     3     B     67.0       835     66     50.54     3.02     0.8     2     38.1     B     3     B     73.1											
833     68     790.46     41.76     1.2     2.1     60.4     B     3     B     71.4       834     63     25.86     1.42     0.7     1.9     162.9     B     3     B     67.0       835     66     50.54     3.02     0.8     2     38.1     B     3     B     73.1											
834 63 25.86 1.42 0.7 1.9 162.9 B 3 B 67.0 835 66 50.54 3.02 0.8 2 38.1 B 3 B 73.1											
835 66 50.54 3.02 0.8 2 38.1! B 3 B 73.1											
836 64 52.21 2.47 1.1 3.8 173 B 3 B 65.5											
	836	64	52.21	2.47	1.1	3.8	173	B.	3,	<u>B</u> ·	65.5

Fig. 7
Page 4 of 8

837 72 12.63				· · · · · · · · · · · · · · · · · · ·							
849 72 50.75 22.69 0 2.9 87.5 B 3 B 54.3 840 63 18.86 1.82 0.9 1.1 76.2 B 3 B 61.00 441 65 9.77 1.76 0.6 2.6 80.9 B 3 B 3 B 49.3 842 76 10.63 2.06 1.2 2 55.5 B 3 B 59.8 843 73 11.25 1.43 0.6 2.3 60.7 B 3 B 59.8 844 71 146.44 2.9 0.3 0.7 156.7 B 3 B 58.8 844 71 146.44 2.9 0.3 0.7 156.7 B 3 B 70.4 845 65 10.28 1.58 0.9 2.8 114.5 B 3 B 70.4 846 68. 46.72 3.12 1.1 2.8 105.8 B 3 B 48.4 846 68. 46.72 3.12 1.1 2.8 105.8 B 3 B 48.4 847 70 22.1 3.5 1 4 211.8 B 3 B 3 B 56.5 849 841 70 22.23 2.63 0.8 3.5 103.8 B 3 B 56.5 849 81 2.20 94 2.21 0.9 3.1 152.3 B 3 B 56.5 849 81 2.09 4 2.21 0.9 3.1 152.3 B 3 B 54.5 85.5 10.23 3.16 1 2.3 92.1 B 3 B 54.5 85.5 10.23 3.16 1 2.3 92.1 B 3 B 54.5 85.5 10.33 1.77 1.6 0.9 112 B 3 B 54.5 85.5 10.33 1.77 1.6 0.9 112 B 3 B 42.3 85.5 10.3 8 17.7 1.6 0.9 112 B 3 B 42.3 85.5 10.3 8 1 8 42.3 85.5 10.3 1.77 1.6 0.9 112 B 3 B 42.3 85.8 85.5 10.3 8 1.77 1.6 0.9 112 B 3 B 42.3 85.8 85.5 10.3 8 1.77 1.6 0.9 112 B 3 B 42.3 85.5 10.3 8 1 4.5 2 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	837	72	12.63	2.42							
840 63 18.86 1.82 0.9 1.1 76.2 B 3 B 61.0 841 65 9.77 1.76 0.6 2.6 80.9 B 3 B 3 B 49.3 842 76 10.63 2.06 1.2 2 55.5 B 3 B 50.8 843 73 11.25 1.43 0.6 2.3 60.7 B 3 B 50.8 844 71 146.4 2.9 0.3 0.7 156.7 B 3 B 70.4 845 65 10.28 1.58 0.9 2.8 114.5 B 3 B 70.4 846 68 46.7 3.12 1.1 2.8 105.8 B 3 B 66.1 847 70 22.1 3.5. 1 4 211.8 B 3 B 48.4 848 76 22.23 2.63 0.8 3.5 103.8 B 3 B 56.5 849 81. 20.94 2.21 0.9 3.1 152.3 B 3 B 54.5 850 67, 55.47 6.6 2.1 2.1 88.6 B 3 B 54.5 851 60 12.63 3.16 1 2.3 92.1 B 3 B 54.5 852 50 10.33 1.77 1.6 0.9 112 B 3 B 54.5 853 55 19.38 1.17 1.4 3.3 103 B 3 B 54.5 854 66 25.14 17.38 1.5 2.5 85.9 B 3 B 58.8 854 66 25.14 17.38 1.5 2.5 85.9 B 3 B 58.8 855 64 5.42 1.41 3.4 3.3 161 B 3 B 58.8 856 69 7.9 7 1.61 0.8 2.8 55.1 B 3 B 20.6 857 67 14.04 3.1 1.6 3.5 141.2 B 3 B 20.6 858 60 63 6.38 1.04 0.6 2 90.8 B 3 B 45.2 859 65 44.32 28.31 4.05 0.8 2.8 84.1 C 3 3 B 22.6 859 65 4.32 2.8 1.4 1.0 0.8 2.8 55.1 B 3 B 22.6 859 65 4.32 2.8 1.4 1.0 0.8 2.8 55.1 B 3 B 45.2 859 67 15.5 1.7 1.8 1.0 0.8 2.8 55.1 B 3 B 45.2 859 67 18.5 0.8 2.8 55.1 B 3 B 45.2 859 67 18.5 0.8 2.8 55.1 B 3 B 22.6 859 67 18.5 0.8 2.8 55.1 B 3 B 45.2 859 67 18.0 8 2.8 55.1 B 3 B 45.2 859 67 18.0 8 2.8 55.1 B 3 B 45.2 859 67 18.5 0.8 2.8 55.1 B 3 B 22.6 859 67 18.5 0.8 2.8 55.1 B 3 B 45.2 859 67 18.5 0.8 2.8 55.1 B 3 B 45.2 859 67 18.0 8 2.8 55.1 B 3 B 45.2 859 67 18.0 8 2.8 55.1 B 3 B 45.2 859 67 18.5 0.8 2.8 55.1 B 3 B 45.2 859 67 18.5 0.8 2.5 55.1 B 3 B 45.2 859 67 18.5 0.0 9.3 5.5 88.8 B 3 B 45.2 859 67 18.5 0.0 9.9 3.5 88.8 B 3 B 45.2 859 67 18.5 0.0 9.9 3.5 88.8 B 3 B 45.2 859 67 18.5 0.0 9.9 3.5 88.8 B 3 B 45.2 859 67 18.5 0.0 9.9 3.5 88.8 B 3 B 45.2 859 67 18.5 0.0 9.9 3.5 88.8 B 3 B 45.2 859 67 18.5 0.0 9.9 3.5 88.8 B 3 B 45.2 859 67 18.5 0.0 9.9 3.5 88.8 B 3 B 45.2 859 67 18.5 0.0 9.0 1.1 1.1 1.1 1.1 1.1 1.1 1.1 1.1 1.1 1	838	60	19.02	1.47	1.2	1.3	68.4	В	3	В	
841 65 9.77 1.76 0.6 2.6 80.9 B 3 B 49.3 849.3 842.7 76 10.63 2.06 1.2 2 55.5 B 3 8 50.8 843 73 11.25 1.43 0.6 2.3 60.7 B 3 B 58.3 844 71 146.44 2.9 0.3 0.7 156.7 B 3 B 70.4 845 65 10.28 1.56 0.9 2.8 114.5 B 3 B 70.4 846 68. 46.72 3.12 1.1 2.8 105.8 B 3 B 48.4 846 68. 46.72 3.12 1.1 2.8 105.8 B 3 B 45.2 846 70 22.2 3.63 0.8 3.5 103.8 B 3 B 45.2 848 77 0 22.1 3.5 1 4 211.8 B 3 B 3 B 56.5 849 81 20.94 2.21 0.9 3.1 152.3 B 3 B 56.5 850 67, 55.47 6.6 2.1 2.1 88.6 B 3 B 56.5 850 67, 55.47 6.6 2.1 2.1 88.6 B 3 B 54.5 850 67, 55.47 6.6 2.1 2.1 88.6 B 3 B 54.5 850 67, 55.47 1.6 0.9 112 B 3 B 24.3 849.3 849.3 1.77 1.6 0.9 112 B 3 B 24.3 849.3 849.3 1.77 1.6 0.9 112 B 3 B 24.5 855 50 10.33 1.77 1.6 0.9 112 B 3 B 24.5 855 65 64 5.42 1.41 3.4 3.3 193.9 B 3 B 54.5 855 64 5.42 1.41 3.4 3.3 161 B 3 B 24.5 855 64 5.42 1.41 3.4 3.3 161 B 3 B 24.5 855 64 5.42 1.41 3.4 3.3 161 B 3 B 24.5 855 64 5.42 1.41 3.4 3.3 161 B 3 B 24.2 855 64 5.42 1.41 3.4 3.3 161 B 3 B 24.2 855 64 5.42 1.41 3.4 3.3 161 B 3 B 24.2 855 64 5.42 1.41 3.4 3.3 161 B 3 B 24.2 855 64 5.42 1.41 3.4 3.5 1.5 2.5 85.9 B 3 B 24.2 855 64 5.42 1.41 3.4 0.5 2.8 561 B 3 B 24.2 855 64 5.42 1.41 3.4 0.5 2.8 561 B 3 B 24.2 855 64 5.42 1.41 3.4 0.5 2.8 561 B 3 B 24.2 855 64 5.42 1.41 3.4 0.5 2.8 561 B 3 B 24.2 855 64 5.42 1.41 3.4 0.5 2.8 561 B 3 B 24.2 855 64 5.42 1.41 3.4 0.5 2.8 561 B 3 B 2.2 56 860 63 6.38 1.04 0.6 2 90.8 B 3 B 24.2 855 65 64 5.42 1.41 3.4 0.5 2.8 561 B 3 B 2.2 56 860 63 6.38 1.04 0.6 2 90.8 B 3 B 2.2 56 860 63 6.38 1.04 0.6 2 90.8 B 3 B 2.2 56 860 63 6.38 1.04 0.6 2 90.8 B 3 B 2.2 56 860 63 6.38 1.04 0.6 2 90.8 B 3 B 2.2 56 860 63 6.38 1.04 0.5 8 2.8 561 B 3 B 2.2 56 860 63 6.38 1.04 0.6 2 90.8 B 3 B 2.2 56 860 63 6.38 1.04 0.5 8 2.8 561 B 3 3 B 2.2 56 860 63 6.38 1.04 0.6 8 2 90.8 B 3 B 3 B 2.2 56 860 63 6.38 1.04 0.6 8 2 90.8 B 3 B 3 B 2.2 56 860 63 6.38 1.04 0.6 8 2 90.8 B 3 B 3 B 2.2 56 860 63 6.38 1.04 0.6 8 2 90.8 B 3 B 3 B 2.2 56 860 63 6.38 1.04 0.6 8 2 90.8 B 3 B 3 B 2.2 56 860 63 6.38 1.04 0.6 8 2 90.8 B 3 3 B 2.2 56 860 63 6.38 1.04 0.6 8 2 9	839	72	50.75	22.69	0	2.9	87.5	В	3	В	54.3
842         76         10.63         2.06         1.2         2         55.5         B         3         B         50.8           843         73         11.25         1.43         0.6         2.3         60.7         B         3         B         58.3           844         71         146.44         2.9         0.3         0.7         156.7         B         3         B         70.4           845         65         10.28         1.58         0.9         2.8         114.5         B         3         B         48.4           846         68         46.72         3.12         1.1         2.8         105.8         B         3         B         48.1           847         70         22.1         3.5         1         4         211.8         B         3         B         45.2           849         81         20.94         2.21         0.9         3.1         152.3         B         3         B         54.5           850         67         55.47         6.6         2.1         2.1         86.6         B         3         B         54.5           855         67         10	840	63	18.86	1.82	0.9	1.1	76.2	В			
842         76         10.63         2.06         1.2         2         55.5         B         3         B         50.8           844         71         146.44         2.9         0.3         0.7         156.7         B         3         B         58.3           844         71         146.44         2.9         0.3         0.7         156.7         B         3         B         70.4           845         65         10.28         1.58         0.9         2.8         114.5         B         3         B         49.4           846         68         46.72         3.12         1.1         2.8         105.8         B         3         B         46.1           847         70         22.1         3.5         1         4         211.8         B         3         B         45.5           848         76         22.23         2.63         0.8         3.5         103.8         B         3         B         45.5           850         67         55.47         6.6         2.1         2.1         8.6         B         3         B         54.5           855         50         10	841	65	9.77	1.76	0.6	2.6	80.9	В	3	В	49.3
844 71 146 44 2.9 0.3 0.7 156.7 B. 3 B 70.4 845 65 10.28 1.58 0.9 2.8 114.5 B. 3 B 48.4 846 68 46.72 3.12 1.1 2.8 105.8 B 3 B 66.1 847 70 22.1 3.5 1 4 211.8 B 3 B 65.2 848 76 22.23 2.63 0.8 3.5 103.8 B1 3 B 55.2 848 81 20.94 2.21 0.9 3.1 152.3 B 3 B 55.5 849 81 20.94 2.21 0.9 3.1 152.3 B 3 B 54.5 850 67 55.47 6.6 2.1 2.1 88.6 B 3 B 54.5 850 67 55.47 6.6 2.1 2.1 88.6 B 3 B 54.5 851 60 12.63 3.16 1 2.3 92.1 B 3 B 54.5 852 50 10.33 1.77 1.5 0.9 112 B 3 B 42.3 853 55 19.38 1.17 1.4 3.3 19.9 B 3 B 45.5 854 66 25.14 17.38 1.5 2.5 85.9 B 3 B 54.5 855 64 5.42 1.41 3.4 3.3 19.9 B 3 B 58.8 854 66 25.14 17.38 1.5 2.5 85.9 B 3 B 45.8 855 67 14.04 3.1 1.6 3.5 1412 B 3 B 22.6 856 69 7.97 1.61 0.8 2.8 58.1 B 3 B 42.0 857 67 14.04 3.1 1.6 3.5 1412 B 3 B 42.0 858 62 2.87 1.34 0.5 2.8 84.7 B 3 B 42.0 858 62 2.87 1.34 0.5 2.8 84.7 B 3 B 42.0 859 63 6.38 1.04 0.6 2 90.8 B 3 B 45.0 860 63 6.38 1.04 0.6 2 90.8 B 3 B 45.0 860 63 6.38 1.04 0.6 2 90.8 B 3 B 45.0 859 65 44.32 28.31 46.2 2.7 108.7 B 3 B 52.8 859 67 4.40 3.1 1.9 0.6 4.1 180 B 3 B 52.8 859 67 4.2 2.8 3 46.2 2.7 108.7 B 3 B 45.8 859 67 4.4 2.8 3 3 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	842	76	10.63	2.06	1.2	2	55.5	В	3	В	50.8
844 71 146 44 2.9 0.3 0.7 156.7 B. 3 B 70.4 845 65 10.28 1.58 0.9 2.8 114.5 B. 3 B 48.4 846 68 46.72 3.12 1.1 2.8 105.8 B 3 B 66.1 847 70 22.1 3.5 1 4 211.8 B 3 B 66.1 847 70 22.1 3.5 1 4 211.8 B 3 B 56.5 848 76 22.23 2.63 0.8 3.5 103.8 B 3 B 55.5 849 81 20.94 2.21 0.9 3.1 152.3 B 3 B 55.5 849 81 20.94 2.21 0.9 3.1 152.3 B 3 B 54.5 850 67 55.47 6.6 2.1 2.1 88.6 B 3 B 5.4 5 850 67 55.47 6.6 2.1 2.1 88.6 B 3 B 54.5 851 60 12.63 3.16 1 2.3 92.1 B 3 B 54.5 852 50 10.33 1.77 1.5 0.9 112 B 3 B 42.3 853 55 19.38 1.17 1.4 3.3 193.9 B 3 B 54.5 854 66 25.14 17.38 1.5 2.5 85.9 B 3 B 52.8 855 64 5.42 1.41 3.4 3.3 161 B 3 B 22.6 856 69 7.97 1.61 0.8 2.8 58.1 B 3 B 22.6 857 67 14.04 3.1 1.6 3.5 1412 B 3 B 44.0 858 69 2.87 1.34 0.5 2.8 84.7 B 3 B 42.0 858 62 2.87 1.34 0.5 2.8 84.7 B 3 B 42.0 858 62 2.87 1.34 0.5 2.8 84.7 B 3 B 42.0 859 63 6.38 1.04 0.5 2 90.8 B 3 B 45.0 860 63 6.38 1.04 0.5 2 90.8 B 3 B 45.0 860 63 6.38 1.04 0.5 2 8 84.7 B 3 B 45.0 861 72 53.16 4.07 0.9 3.5 86.8 B 3 B 52.8 859 65 44 32 28.31 46.2 2.7 108.7 B 3 B 45.2 859 64 67 2.7 1.9 0.6 4.1 180 B 3 B 52.8 859 65 44 3.2 28.31 46.2 2.7 108.7 B 3 B 52.8 859 67 4.4 2.8 3 3 0.3 6.1 318.2 C 3 C 57.8 859 85 64 5.4 2.6 3 3.1 1.9 0.6 4.1 180 B 3 B 52.8 859 67 4.3 2 8.3 3 3 5 5.5 1 3 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	843					2.3	60.7	В	3	В	58.3
845 65 10.28 1.58 0.9 2.8 114.5 B 3 B 48.4 846 68 46.72 3.12 1.1 2.8 105.8 B 3 B 66.1 847 70 22.1 3.5 1 4 211.8 B 3 B 56.5 848 76 22.23 2.63 0.8 3.5 103.8 B: 3 B 56.5 849 81 20.94 2.21 0.9: 3.1 152.3 B 3 B 56.5 850 67 55.47 6.6 2.1 2.1 88.6 B 3 B 54.5 851 60 12.63 3.16 1 2.3 92.1 B 3 B 54.5 852 50 10.33 1.77 1.6 0.9 112 B: 3 B 3 B 54.5 853 55 19.38 1.17: 1.4 3.3 193.9 B 3 B 58.8 854 66 25.14 17.38 1.5 2.5 85.9 B 3 B 58.8 855 64 5.42 1.41 3.4 3.3 161 B 3 B 29.6 856 69 7.97 1.61 0.8 2.8 58.1 B 3 B 29.6 857 67 14.04 3.1 1.6 3.5 141.2 B: 3 B 29.6 858 62 2.87 1.34 0.5 2.8 84.7 B 3 B 29.5 860 63 63.8 1.04 0.6 2 90.8 B 3 B 29.5 861 72 53.16 4.07 0.9 3.5 86.8 B: 3 B 29.5 861 72 53.16 4.07 0.9 3.5 86.8 B: 3 B 66.0 714 68 30.72 3.83 0.3 6.1 180.9 B: 3 B 66.0 714 68 30.72 3.83 0.3 6.1 180.9 B 3 B 66.0 714 68 30.72 3.83 0.3 6.1 180.9 B 3 B 66.0 714 68 30.72 3.83 0.3 6.1 180.9 B 3 B 66.0 7177 71 1.6 0.9 3.5 86.8 B: 3 B 66.0 718 77 18.58 1.75 1.2 3 112.4 C 3 C 57.8 720 80 40.38 3.27 1.3 3.5 3.4 1 C 3 C 57.8 721 721 731 742.5 50.4 9 0.5 3.1 12.4 C 3 C 57.8 722 737 742.7 50.4 9 0.5 3.1 12.4 C 3 C 57.8 723 742 75.6 77 1.5 1.2 3 112.4 C 3 C 57.8 724 67 42.76 3.11 0.7 3.8 84. C 3 C 57.8 727 77 1.6 1.3 3.5 1.2 3 112.4 C 3 C 57.8 729 79 7.65 0.49 0.5 3.1 195. C 3 C 65.5 741 71 71 71 71 71 71 71 71 71 71 71 71 71						0.7	156.7	B:	3	В	70.4
846 68 46.72 3.12 1.1 2.8 105.8 B 3 B 66.1 847 70 22.1 3.5 1 4 211.8 B 3 B 45.2 848 76 22.23 2.63 0.8 3.5 103.8 B 3 B 55.5 849 81 20.94 2.21 0.9 3.1 152.3 B 3 B 54.5 850 67 55.47 6.6 2.1 2.1 88.6 B 3 B 54.5 851 60 12.63 3.16 1 2.3 92.1 B 3 B 54.5 852 50 10.33 1.77 1.6 0.9 112 B 3 B 42.3 853 55 19.38 1.17 1.4 3.3 193.9 B 3 B 54.5 854 66 25.14 17.38 1.5 2.5 85.9 B 3 B 42.3 855 64 5.42 1.41 3.4 3.3 161 B 3 B 29.6 856 69 7.97 1.61 0.8 2.8 58.1 B 3 B 29.6 856 69 7.97 1.61 0.8 2.8 58.1 B 3 B 42.2 858 62 2.87 1.34 0.5 2.8 84.7 B 3 B 42.2 858 62 2.87 1.34 0.5 2.8 84.7 B 3 B 22.5 860 63 6.38 1.04 0.6 2 90.8 B 3 B 42.2 861 72 53.16 4.07 0.9 3.5 86.8 B 3 B 45.2 862 64 12.15 1.19 0.6 4.1 180. B 3 B 42.2 868 65 64 4.32 2.831 46.2 2.7 108.7 B 3 B 52.8 859 65 44.32 2.831 46.2 2.7 108.7 B 3 B 40.6 859 65 44.32 2.831 46.2 2.7 108.7 B 3 B 40.6 8714 68 30.72 3.83 0.3 6.1 318.2 C 3 C 45.1 8718 77 18.58 1.75 1.2 3 112.4 C 3 C 3 C 57.8 8724 67 42.76 3.11 0.7 3.8 84 C 3 C 57.7 8727 77 49.33 5.67 1.1 4.3 99.9 C 3 C 58.4 8729 79 7.65 0.49 0.5 3.1 195 C 3 C 65.7 8724 67 42.76 3.11 0.7 3.8 84 C 3 C 67.7 8727 77 14.93 3.567 1.1 4.3 99.9 C 3 C 58.4 8738 777 80.3 4.21 0.9 6.2 201.9 C 3 C 58.4 884 77 6.98 0.86 1.3 2.5 119 C 3 C 65.7 884 771 6.98 0.86 1.3 2.5 119 C 3 C 65.7 885 65 1.3 1.3 1.2 1.2 3 112.4 C 3 C 57.7 8738 779 1.22.4 566.9 C 6.4 3.6 111.8 C 3 C 65.7 8724 67 42.76 3.11 0.7 3.8 84 C 3 C 67.7 8727 77 4.93 3.567 1.1 4.3 99.9 C 3 C 58.4 884 77 6.98 0.86 1.3 2.5 119 C 3 C 58.4 884 77 6.98 0.86 1.3 2.5 119 C 3 C 59.7 884 779 77.50 0.49 0.5 3.1 195 C 3 C 59.7 884 779 77.50 0.49 0.5 3.1 195 C 3 C 59.7 885 65 1.1 1.4 1.8 1.8 1.8 1.8 1.8 1.8 1.8 1.8 1.8 1.8	845	65				2.8	114.5	B:	3.	В	48.4
847 70 22.1 3.5 1 4 211.8 B 3 B 45.2 848 76 22.23 2.63 0.8 3.5 103.8 B 3 B 56.5 849 81 20.94 2.21 0.9 3.1 152.3 B 3 B 56.5 859 67 55.47 6.6 2.1 2.1 88.6 B 3 B 54.5 850 67 55.47 6.6 2.1 2.1 88.6 B 3 B 54.5 851 60 12.63 3.16 1 2.3 92.1 B 3 B 45.5 852 50 10.33 1.77 1.6 0.9 112 B 3 B 45.5 853 55 19.38 1.17 1.4 3.3 193.9 B 3 B 58.8 854 66 25.14 17.38 1.5 2.5 85.9 B 3 B 45.4 855 66 7 14.04 3.1 1.6 3.5 141.2 B 3 B 45.4 856 69 7.97 1.61 0.8 2.8 58.1 B 3 B 48.0 857 67 14.04 3.1 1.6 3.5 141.2 B 3 B 48.0 858 62 2.87 1.34 0.5 2.8 84.7 B 3 B 29.5 860 63 6.38 1.04 0.6 2 90.8 B 3 B 29.5 861 72 53.16 4.07 0.9 3.5 86.8 B 3 B 29.5 859 65 4.32 2.31 46.2 2.7 108.7 B 3 B 52.8 859 65 4.32 2.31 46.2 2.7 108.7 B 3 B 52.8 859 65 4.32 2.33 46.2 2.7 108.7 B 3 B 52.8 714 68 30.72 3.83 0.3 6.1 318.2 C 3 C 66.0 723 59 332.64 21.75 0.7 2.9 176 C 3 C 65.3 724 67 42.76 3.11 0.7 3.8 84 C 3 C 65.7 727 71 61 0.8 2.8 84 C 3 C 3 C 65.7 727 71 63.9 0.8 3.2 7 1.3 3 3.5 34.1 C 3 C 65.0 728 79 79 79 79 79 79 79 79 79 79 79 79 79		68							3	В	66.1
848         76         22.23         2.63         0.8         3.5         103.8         B:         3         B         56.5           849         81         20.94         2.1         0.9         3.1         152.3         B         3         B         54.5           850         67         55.47         6.6         2.1         2.1         88.6         B         3         B         54.5           851         60         12.63         3.16         1         2.3         92.1         B         3         B         45.5           852         55         19.38         1.17         1.4         3.3         193.9         B         3         B         45.8           854         66         25.14         17.38         1.5         2.5         85.9         B         3         B         45.8           855         64         5.42         1.41         3.4         3.3         161         B         3         B         45.8           855         64         5.42         1.41         3.4         3.3         161         B         3         B         45.2           856         69         7											
849											
B50  67  55.47  6.6  2.1  2.1  88.6  B  3  B  54.1  851  60  12.63  3.16  1  2.3  92.1  B  3  B  45.5  852  50  10.33  1.77  1.6  0.9  112  B  3  B  42.3  853  55  19.38  1.17  1.4  3.3  193.9  B  3  B  58.8  854  66  25.14  17.38  1.5  2.5  85.9  B  3  B  58.8  854  66  25.14  17.38  1.5  2.5  85.9  B  3  B  29.6  856  69  7.97  1.61  0.8  2.8  58.1  B  3  B  42.2  858  69  7.97  1.61  0.8  2.8  58.1  B  3  B  42.2  858  69  7.97  1.61  0.8  2.8  58.1  B  3  B  42.2  858  69  7.97  1.61  0.8  2.8  58.1  B  3  B  42.2  858  62  2.87  1.34  0.5  2.8  84.7  B  3  B  42.2  858  62  2.87  1.34  0.5  2.8  84.7  B  3  B  42.2  858  62  2.87  1.34  0.5  2.8  84.7  B  3  B  45.2  860  63  6.38  1.04  0.6  2  90.8  B  3  B  3  B  45.2  860  63  6.38  1.04  0.6  2  90.8  B  3  B  56.0  862  64  12.15  1.19  0.6  4.1  180  B  3  B  52.8  859  65  44.32  28.31  46.2  2.7  108.7  B  3  B  52.8  859  65  44.32  28.31  46.2  2.7  108.7  B  3  B  52.8  859  65  44.32  28.31  46.2  2.7  108.7  B  3  B  52.8  859  65  44.32  28.31  46.2  2.7  108.7  B  3  B  52.8  712  60  40.38  3.27  1.3  3.5  34.1  C  3  C  57.8  712  60  40.38  3.27  1.3  3.5  34.1  C  3  C  57.8  712  60  40.38  3.27  1.3  3.5  34.1  C  3  C  57.8  712  67  42.76  3.11  0.7  3.8  84  C  3  C  57.8  712  72  73  74  73  2722  45  56.92  6.4  3.6  111.8  C  3  C  52.9  734  79  2722  45  56.92  6.4  3.6  111.8  C  3  C  52.9  734  79  2722  45  56.92  6.4  3.6  111.8  C  3  C  52.9  734  77  60  7.32  1.77  1.5  6.1  172.5  C  3  C  3  C  59.7  738  77  700  7.32  1.77  1.5  6.1  172.5  C  3  C  3  C  59.7  865  65  1.5  1.4  0.8  4.9  191.4  C  3  C  59.7  685  65  1.5  1.4  0.8  4.9  191.4  C  3  C  59.7  685  65  1.5  1.4  0.8  4.9  191.4  C  3  C  59.7  685  65  1.5  1.4  0.8  4.9  191.4  C  3  C  3  C  59.7  6919  69  22.76  4.6  1  2.5  89.5  C  3  C  3  C  59.7  6919  69  92.76  4.6  1  2.5  89.5  C  3  C  3  C  59.7  6919  69  92.76  4.6  1  2.5  89.5  C  3  C  3  C  59.7  6919  69  92.76  4.6  1  2.5  89.5  C  3  C  3  C  59.5  692  63  63  63  63											
B51											
852         50         10.33         1.77         1.6         0.9         112         B:         3         B         42.3           853         55         19.38         1.17         1.4         3.3         193.9         B         3         B         58.8           854         66         25.14         17.38         1.5         2.5         85.9         B         3         B         45.4           855         64         5.42         1.41         3.4         3.3         161         B         3         B         29.8           856         69         7.97         1.61         0.8         2.8         58.1         B         3         B         42.2           859         62         2.87         1.34         0.5         2.8         84.7         B         3         B         42.2           859         62         2.87         1.34         0.5         2.8         84.7         B         3         B         45.2           860         63         6.38         1.04         0.6         2         90.8         B         3         B         45.2           861         72         53.1											
853         55         19.38         1.17;         1.4         3.3         193.9         B         3         B         58.8           854         66         25.14         17.38         1.5         2.5         85.9         B         3         B         45.4           855         64         5.42         1.41         3.4         3.3         161         B         3         B         29.6           856         69         7.97         1.61         0.8         2.8         58.1         B         3         B         42.2           857         67         14.04         3.1         1.6         3.5         141.2         B         3         B         42.2           858         62         2.87         1.34         0.5         2.8         84.7         B         3         B         42.5           860         63         6.38         1.04         0.6         4.1         180.8         B         3         B         45.2           861         72         53.16         4.07         0.9         3.5         86.8         B         3         B         45.2           861         73 <td< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></td<>											
854.         66.         25.14         17.38         1.5         2.5         85.9         B         3         B         45.4           855.         64         5.42         1.41         3.4         3.3         161         B         3         B         29.6           856.         69         7.97         1.61         0.8         2.8         58.1         B         3         B         48.0           857.         67         14.04         3.1         1.6         3.5         141.2         B         3         B         42.2           858.         62         2.87         1.34         0.5         2.8         84.7         B         3         B         29.5           860.         63         6.38         1.04         0.6         2         90.8         B         3         B         45.2           861         72         53.16         4.07         0.9         3.5         86.8         B         3         B         45.2           861         72         53.16         4.07         0.9         3.5         86.8         B         3         B         45.2           859         65         <											
855         64         5.42         1.41         3.4         3.3         161         B         3         B         29.6           856         69         7.97         1.61         0.8         2.8         58.1         B         3         B         48.0           857         67         14.04         3.1         1.6         3.5         141.2         B         3         B         42.2           858         62         2.87         1.34         0.5         2.8         84.7         B         3         B         29.5           860         63         6.38         1.04         0.6         2.90.8         B         3         B         45.2           861         72         53.16         4.07         0.9         3.5         86.8         B         3         B         45.2           862         64         12.15         1.19         0.6         4.11         180         B         3         B         45.2           859         65         44.32         28.3         46.2         2.7         108.7         B         3         B         40.6           714         68.30         3.2											
856         69         7.97         1.61         0.8         2.8         58.1         B         3         B         48.0           857         67         14.04         3.1         1.6         3.5         141.2         B         3         B         42.2           858         62         2.87         1.34         0.5         2.8         84.7         B         3         B         42.2           860         63         6.38         1.04         0.6         2.90.8         B         3         B         45.2           861         72         53.16         4.07         0.9         3.5         86.8         B         3         B         66.0           862         64         12.15         1.19         0.6         4.1         1800         B         3         B         46.0           714         68         30.72         3.83         0.3         6.1         318.2         C         3         C         46.1           714         68         30.72         3.83         0.3         6.1         318.2         C         3         C         46.1           718         77         18.3											
857         67         14.04         3.1         1.6         3.5         141.2         B         3         B         42.2           858         62         2.87         1.34         0.5         2.8         84.7         B         3         B         29.5           860         63         6.38         1.04         0.6         2         90.8         B         3         B         45.2           861         72         53.16         4.07         0.9         3.5         86.8         B         3         B         52.8           859°         65         44.32         28.31         46.2         2.7         108.71         B         3         B         52.8           714         68         30.72         3.83         0.3         6.1         318.2         C         3         C         46.1           718         77         18.58         1.75         1.2         3         112.4         C         3         C         57.8           720         80         40.38         3.27         1.3         3.5         34.1         C         3         C         66.9           724         67         <											
858:         62         2.87         1.34         0.5         2.8         84.7         B         3         B         29.5           860:         63         6.38         1.04         0.6:         2         90.8         B         3         B         45.2           861:         72         53.16         4.07         0.9         3.5         86.8         B         3         B         45.2           862:         64         12.15         1.19         0.6         4.11         180:         B         3         B         52.8           859*         65         44.32         28.31         46.2         2.7         108.7         B         3         B         40.6           714:         68         30.72         3.83         0.3         6.1         318.2         C         3         C         46.1           718:         77         18.58         1.75         1.2         3         112.4         C         3         C         46.1           720:         80         40.40.38         3.27         1.3         3.5         34.1         C         3         C         66.0           723:         59 <td></td>											
860    63   6.38   1.04   0.6    2   90.8    B   3    B   45.2											
861         72         53.16         4.07         0.9         3.5         86.8         B         3         B         66.0           862         64         12.15         1.19         0.6         4.1         180         B         3         B         52.8           859*         65         44.32         28.31         46.2         2.7         108.71         B         3         B         40.6           714         68         30.72         3.83         0.3         6.1         318.2         C         3         C         46.1           718         77         18.58         1.75         1.2         3         112.4         C         3         C         46.1           720         80         40.38         3.27*         1.3         3.5         34.1         C         3         C         66.0           723         59         332.64         21.75         0.7         2.9         176         C         3         C         67.7           727         71         49.33         5.67         1.1         4.3         99.9         C         3         C         52.9           734         79; 272.4 <td></td>											
862         64         12.15         1.19         0.6         4.1         180         B         3         B         52.8           859°         65         44.32         28.31         46.2         2.7         108.71         B         3         B         40.6           714         68         30.72         3.83         0.3         6.1         318.2         C         3         C         46.1           718         77         18.58         1.75         1.2         3         112.4         C         3         C         57.8           720         80         40.38         3.27         1.3         3.5         34.1         C         3         C         66.0           723         59         332.64         21.75         0.7         2.9         176         C         3         C         63.5           724         67         42.76         3.11         0.7         3.8         84         C         3         C         67.7           727         71         49.93         5.67         1.1         4.3         99.9         C         3         C         58.4           729         79											
859°         65         44.32         28.31         46.2         2.7         108.71         B         3         B         40.6           714         68         30.72         3.83         0.3         6.1         318.2         C         3         C         46.1           718         77         18.58         1.75         1.2         3         112.4         C         3         C         56.0           720         80         40.38         3.27         1.3         3.5         34.1         C         3         C         66.0           723         59         332.64         21.75         0.7         2.9         176         C         3         C         66.0           724         67         42.76         3.11         0.7         3.8         84         C         3         C         63.5           724         67         42.76         3.11         0.7         3.8         84         C         3         C         58.4           729         79         7.65         0.49         0.5         3.1         1.95         C         3         C         52.9           734         79         <											
714         68         30.72         3.83         0.3         6.1         318.2         C         3         C         46.1           718         77         18.58         1.75         1.2         3         112.4         C         3         C         57.8           720         80         40.38         3.27         1.3         3.5         34.1         C         3         C         66.0           723         59         32.64         21.75         0.7         2.9         176         C         3         C         63.5           724         67         42.76         3.11         0.7         3.8         84         C         3         C         63.5           729         79         7.65         0.49         0.5         3.1         195         C         3         C         58.4           729         79         7.65         0.49         0.5         3.1         195         C         3         C         52.9           734         79         2722.4         566.92         6.4         3.6         111.8         C         3         C         49.2           738         77											
718         77         18.58         1.75         1.2         3         112.4         C         3         C         57.8           720         80         40.38         3.27         1.3         3.5         34.1         C         3         C         66.0           723         59         332.64         21.75         0.7         2.9         176         C         3         C         63.5           724         67         42.76         3.11         0.7         3.8         84         C         3         C         67.7           727         71         49.33         5.67         1.1         4.3         99.9         C         3         C         58.4           729         79         7.65         0.49         0.5         3.1         195         C         3         C         58.4           729         79         7.65         0.49         0.5         3.1         195         C         3         C         52.9           734         79         272.2.4         566.92         6.4         3.6         111.8         C         3         C         49.2           738         77 <td< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></td<>											
720         80         40.38         3.27         1.3         3.5         34.1         C         3         C         66.0           723         59         332.64         21.75         0.7         2.9         176         C         3         C         63.5           724         67         42.76         3.11         0.7         3.81         84         C         3         C         67.7           727         71         49.33         5.67         1.1         4.3         99.9         C         3         C         58.4           729         79         7.65         0.49         0.5         3.1         195         C         3         C         52.9           734         79         2722.4         566.92         6.4         3.6         111.8         C         3         C         49.2           738         77         78.03         4.21         0.9         6.2         201.9         C         3         C         49.2           741         71         6.98         0.86         1.3         2.5         119         C         3         C         46.9           776         67         <									3		
723         59         332.64         21.75         0.7         2.9         176         C         3         C         63.5           724         67         42.76         3.11         0.7         3.8         84         C         3         C         67.7           727         71         49.33         5.67         1.1         4.3         99.9         C         3         C         58.4           729         79         7.65         0.49         0.5         3.1         195         C         3         C         58.4           734         79         2722.4         566.92         6.4         3.6         111.8         C         3         C         49.2           738         77         78.03         4.21         0.9         6.2         201.9         C         3         C         49.2           741         71         6.98         0.86         1.3         2.5         119         C         3         C         46.9           776         67         275.16         132.2         0.7         2.3         198.5         C         3         C         43.3           777         60											
724         67         42.76         3.11         0.7         3.81         84         C         3         C         67.7           727:         71         49.33         5.67         1.1         4.3         99.9         C         3         C         58.4           729         79         7.65         0.49         0.5         3.1         195         C         3         C         52.9           734         79         2722.4         566.92         6.4         3.6         111.8         C         3         C         49.2           738         77         78.03         4.21         0.9         6.2         201.9         C         3         C         46.9           776         67         275.16         132.2         0.7         2.3         198.5         C         3         C         46.9           776         67         275.16         132.2         0.7         2.3         198.5         C         3         C         43.3           777         60         7.32         1.77         1.5         6.1         172.5         C         3         C         68.7           863         51											
727:         71         49.33         5.67         1.1         4.3         99.9         C         3         C         58.4           729         79         7.65         0.49         0.5         3.1         195         C         3         C         52.9           734         79;         2722.4         566.92         6.4         3.6         111.8         C         3         C         49.2           738         77         78.03         4.21         0.9         6.2         201.9         C         3         C         49.2           741         71         6.98         0.86         1.3         2.5         119         C         3         C         46.9           776         67:         275.16         132.2         0.7         2.3         198.5         C         3         C         43.3           777         60         7.32         1.77         1.5         6.1         172.5         C         3         C         43.3           778         74         15.29         0.6         0.7         1.4         102.5         C         3         C         29.9           863         51											
729         79         7.65         0.49         0.5         3.1         195         C         3         C         52.9           734         79         2722.4         566.92         6.4         3.6         111.8         C         3         C         49.2           738         77         78.03         4.21         0.9         6.2         201.9         C         3         C         49.2           741         71         6.98         0.86         1.3         2.5         119         C         3         C         46.9           776         67         275.16         132.2         0.7         2.3         198.5         C         3         C         43.3           777         60         7.32         1.77         1.5         6.1         172.5         C         3         C         43.3           778         74         15.29         0.6         0.7         1.4         102.5         C         3         C         68.7           863         51         2.25         0.67         0.7         0.8         82.5         C         3         C         59.7           865         65											
734         79         2722.4         566.92         6.4         3.6         111.8         C         3         C         49.2           738         77         78.03         4.21         0.9         6.2         201.9         C         3         C         65.2           741         71         6.98         0.86         1.3         2.5         119         C         3         C         46.9           776         67         275.16         132.2         0.7         2.3         198.5         C         3         C         43.3           777         60         7.32         1.77         1.5         6.1         172.5         C         3         C         43.3           778         74         15.29         0.6         0.7         1.4         102.5         C         3         C         68.7           7863         51         2.25         0.67         0.7         0.8         82.5         C         3         C         29.9           884         71         34.66         7.36         0.6         1.5         34.7         C         3         C         59.7           865         65									3:		
738         77         78.03         4.21         0.9         6.2         201.9         C         3         C         65.2           741         71         6.98         0.86         1.3         2.5         119         C         3         C         46.9           776         67         275.16         132.2         0.7         2.3         198.5         C         3         C         43.3           777         60         7.32         1.77         1.5         6.1         172.5         C         3         C         31.4           778         74         15.29         0.6         0.7         1.4         102.5         C         3         C         68.7           863         51         2.25         0.67         0.7         0.8         82.5         C         3         C         29.9           864         71         34.66         7.36         0.6         1.5         34.7         C         3         C         59.7           865         65         1.5         1.4         0.8         4.9         191.4         C         3         C         14.9           915         81 <td< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></td<>											
741         71         6.98         0.86         1.3         2.5         119         C         3         C         46.9           776         67         275.16         132.2         0.7         2.3         198.5         C         3         C         43.3           777         60         7.32         1.77         1.5         6.1         172.5         C         3         C         31.4           778         74         15.29         0.6         0.7         1.4         102.5         C         3         C         68.7           863         51         2.25         0.67         0.7         0.8         82.5         C         3         C         29.9           864         71         34.66         7.36         0.6         1.5         34.7         C         3         C         59.7           865         65         1.5         1.4         0.8         4.9         191.4         C         3         C         14.9           915         81         71.36         1.48         0.7         12         275         C         3         C         57.6           916         89         23											
776         67         275.16         132.2         0.7         2.3         198.5         C         3         C         43.3           777         60         7.32         1.77         1.5         6.1         172.5         C         3         C         31.4           778         74         15.29         0.6         0.7         1.4         102.5         C         3         C         68.7           863         51         2.25         0.67         0.7         0.8         82.5         C         3         C         29.9           864         71         34.66         7.36         0.6         1.5         34.7         C         3         C         59.7           865         65         1.5         1.4         0.8         4.9         191.4         C         3         C         14.9           915         81         71.36         1.48         0.7         12         275         C         3         C         61.5           916         89         23.43         2.21         0.9         2.8         121.6         C         3         C         57.6           917         77 <td< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td></td></td<>											
777         60         7.32         1.77         1.5         6.1         172.5         C         3         C         31.4           778         74         15.29         0.6         0.7         1.4         102.5         C         3         C         68.7           863         51         2.25         0.67         0.7         0.8         82.5         C         3         C         29.9           864         71         34.66         7.36         0.6         1.5         34.7         C         3         C         59.7           865         65         1.5         1.4         0.8         4.9         191.4         C         3         C         14.9           915         81         71.36         1.48         0.7         12         275         C         3         C         61.5           916         89         23.43         2.21         0.9         2.8         121.6         C         3         C         57.6           917         77         69.19         12.95         1.6         2         82.4         C         3         C         53.6           918         63         176											
778         74         15.29         0.6         0.7         1.4         102.5         C         3         C         68.7           863         51         2.25         0.67         0.7         0.8         82.5         C         3         C         29.9           864         71         34.66         7.36         0.6         1.5         34.7         C         3         C         59.7           865         65         1.5         1.4         0.8         4.9         191.4         C         3         C         14.9           915         81         71.36         1.48         0.7         12         275         C         3         C         61.5           916         89         23.43         2.21         0.9         2.8         121.6         C         3         C         57.6           917         77         69.19         12.95         1.6         2         82.4         C         3         C         53.6           918         63         176.84         6.88         0.6         2.1         99.5         C         3         C         71.8           919         69         92											
863         51         2.25         0.67         0.7         0.8         82.5         C         3         C         29.9           884         71         34.66         7.36         0.6         1.5         34.7         C         3         C         59.7           865         65         1.5         1.4         0.8         4.9         191.4         C         3         C         14.9           915         81         71.36         1.48         0.7         12         275         C         3         C         61.5           916         89         23.43         2.21         0.9         2.8         121.6         C         3         C         57.6           917         77         69.19         12.95         1.6         2         82.4         C         3         C         57.6           918         63         176.84         6.88         0.6         2.1         99.5         C         3         C         71.8           919         69         92.76         4.6         1         2.5         89.5         C         3         C         70.9           920         73         60.67							102.5	c			
864         71         34.66         7.36         0.6         1.5         34.7         C         3         C         59.7           865         65         1.5         1.4         0.8         4.9         191.4         C         3         C         14.9           915         81         71.36         1.48         0.7         12         275         C         3         C         61.5           916         89         23.43         2.21         0.9         2.8         121.6         C         3         C         57.6           917         77         69.19         12.95         1.6         2         82.4         C         3         C         57.6           918         63         176.84         6.88         0.6         2.1         99.5         C         3         C         71.8           919         69         92.76         4.6         1         2.5         89.5         C         3         C         70.9           920         73         60.67         5.85         0.7         2.7         79.2         C         3         C         64.1           921         77         89.9											
865         65         1.5         1.4         0.8         4.9         191.4         C         3         C         14.9           915         81         71.36         1.48         0.7         12         275         C         3         C         61.5           916         89         23.43         2.21         0.9         2.8         121.6         C         3         C         57.6           917         77         69.19         12.95         1.6         2         82.4         C         3         C         53.6           918         63         176.84         6.88         0.6         2.1         99.5         C         3         C         71.8           919         69         92.76         4.6         1         2.5         89.5         C         3         C         70.9           920         73         60.67         5.85         0.7         2.7         79.2         C         3         C         64.1           921         77         89.95         3.71         0         4.5         56.1         C         3         C         75.2           922         85         85.69<											
915         81         71.36         1.48         0.7         12         275         C         3         C         61.5           916         89         23.43         2.21         0.9         2.8         121.6         C         3         C         57.6           917         77         69.19         12.95         1.6         2         82.4         C         3         C         53.6           918         63         176.84         6.88         0.6         2.1         99.5         C         3         C         71.8           919         69         92.76         4.6         1         2.5         89.5         C         3         C         70.9           920         73         60.67         5.85         0.7         2.7         79.2         C         3         C         64.1           921         77         89.95         3.71         0         4.5         56.1         C         3         C         64.1           921         77         89.95         3.71         0         4.5         56.1         C         3         C         69.1           922         85         85.69<											
916         89         23.43         2.21         0.9         2.8         121.6         C         3         C         57.6           917         77         69.19         12.95         1.6         2         82.4         C         3         C         53.6           918         63         176.84         6.88         0.6         2.1         99.5         C         3         C         71.8           919         69         92.76         4.6         1         2.5         89.5         C         3         C         70.9           920         73         60.67         5.85         0.7         2.7         79.2         C         3         C         64.1           921         77         89.95         3.71         0         4.5         56.1         C         3         C         64.1           921         77         89.95         3.71         0         4.5         56.1         C         3         C         75.2           922         85         85.69         2.58         1.5         4.5         75.8         C         3         C         69.1           923         74         12.3											
917         77         69.19         12.95         1.6         2         82.4         C         3         C         53.6           918         63         176.84         6.88         0.6         2.1         99.5         C         3         C         71.8           919         69         92.76         4.6         1         2.5         89.5         C         3         C         70.9           920         73         60.67         5.85         0.7         2.7         79.2         C         3         C         64.1           921         77         89.95         3.71         0         4.5         56.1         C         3         C         75.2           922         85         85.69         2.58         1.5         4.5         75.8         C         3         C         69.1           923         74         12.37         2.59         0.8         4.5         200.1         C         3         C         41.0           924         85         0         0.57         1.2         2.9         104.9         C         3         C         28.5											
918         63         176.84         6.88         0.6         2.1         99.5         C         3         C         71.8           919         69         92.76         4.6         1         2.5         89.5         C         3         C         70.9           920         73         60.67         5.85         0.7         2.7         79.2         C         3         C         64.1           921         77         89.95         3.71         0         4.5         56.1         C         3         C         75.2           922         85         85.69         2.58         1.5         4.5         75.8         C         3         C         69.1           923         74         12.37         2.59         0.8         4.5         200.1         C         3         C         41.0           924         85         0         0.57         1.2         2.9         104.9         C         3         C         28.5								<del></del>			53.6
919         69         92.76         4.6         1         2.5         89.5         C         3         C         70.9           920         73         60.67         5.85         0.7         2.7         79.2         C         3         C         64.1           921         77         89.95         3.71         0         4.5         56.1         C         3         C         75.2           922         85         85.69         2.58         1.5         4.5         75.8         C         3         C         69.1           923         74         12.37         2.59         0.8         4.5         200.1         C         3         C         41.0           924         85         0         0.57         1.2         2.9         104.9         C         3         C         28.5											
920         73         60.67         5.85         0.7         2.7         79.2         C         3         C         64.1           921         77         89.95         3.71         0         4.5         56.1         C         3         C         75.2           922         85         85.69         2.58         1.5         4.5         75.8         C         3         C         69.1           923         74         12.37         2.59         0.8         4.5         200.1         C         3         C         41.0           924         85         0         0.57         1.2         2.9         104.9         C         3         C         28.5											
921     77     89.95     3.71     0     4.5     56.1     C     3     C     75.2       922     85     85.69     2.58     1.5     4.5     75.8     C     3     C     69.1       923     74     12.37     2.59     0.8     4.5     200.1     C     3     C     41.0       924     85     0     0.57     1.2     2.9     104.9     C     3     C     28.5											
922     85     85.69     2.58     1.5     4.5     75.8     C     3     C     69.1       923     74     12.37     2.59     0.8     4.5     200.1     C     3     C     41.0       924     85     0     0.57     1.2     2.9     104.9     C     3     C     28.5											
923 74 12.37 2.59 0.8 4.5 200.1 C 3 C 41.0 924 85 0 0.57 1.2 2.9 104.9 C 3 C 28.5											
924 85 0 0.57 1.2 2.9 104.9 C 3 C 28.5											
027 00 0.07 1.2 2.5 10.00											
925 /1 8.88 U.6 U.5 2.7 52.3 C 5 C 65.4											
	925	/1	8.88	0.6	U.5	2.1_	5∠.3	<u> </u>	<u>-</u>		03.4

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000										07.0
926		2.44	2.79	0.5	1.5	204.5	<u>c</u>	3	<u>C</u>	67.2
927		6.73	2.45	0.8	4.9	155.6	C	3	C	57.5
928		6.25	6.55	1	1.5	69.7	Ċ	3	С	29.5
929		5.29	3.26	0	2.5	74	С	3	С	65.0
930		5.46	21.05	0	2.1	94.3	С	3	С	54.1
931		1.66	6.53	-0	4.4	191.4	С	3	С	48.9
932	69 3	9.93	1.58	1	2.2	89	С	3	C	71.4
743	86. 45	0.13	427.6	9.5	1.2	65.6		3	D	48.4
747	74: 34	5.62	70.55	2.2	3.8	219.8		3	D	42.5
748	67 2	2000	26.31	1.3	2.4	167.6		3	D	65.0
749	78:	0	0.63	0.9	3.4	94.4		3	D	28.3
750		5.97	7.36	1.3	1.7	97.4	:	3	D.	69.2
751		5.38	2.88	0.6	1.5	85.2	<del></del>	3	D:	72.8
756		9.84	20.62	1	6.2	195.1		3:	D	40.8
757		4.55	11.14	1.4	1.4	105.1		3	D	50.6
760		5.95	2.05	0.9	1.1.	77.7	<del></del>	3	D.	57.1
764		19.7	5.81	1.7	4.5	114	<del></del>	3.	<u>D</u> .	65.7
765		13.6	159.5	1.2.	1.4	75.2		3	<u>b</u>	66.9
770		0.35	1.1	1.1	3.5	122.9		3		53.4
779		3.38	2.27	1.3	2.3	59		3	D D	67.0
780		22.2								
781.		3.26	2.42	1.2.	2.7	148.7	<del></del>	3	<u>D</u>	52.6
			2.83	0.9	1.6	54.3		3;	<u>D</u> _	72.6
782		23.7	1.75	0.8:	1.4	93.1	<del>:</del>	3.	D	65.5
783		0.96	1.3	0.9	2.2	52.5	:	3	D.	71.4
784		8.9	47.38	0.8	1.1	104.6	<u> </u>	3	D	51.9
785		.26	2.65	1.1	2.7	58.1	•	3	D	71.7
786		3.35	2.84:	3.6	2.3	43.1		3	D:	66.4
787		6.5	35.43	1.4	1.3,	44.3	<del></del>	3	D:	58.3
788		.71	1.21.	1;	0.9	84	i	3	D	71.2
933		.66	85.79:	1:	4.5	101	i	3	D.	49.9
934		3.67	1.28	0.8	2.8	130.4	<u> </u>	3:	D.	56.8
935	80 236		116.27	0.9	3.5	136.6	·	3	<u>D:</u>	48.5
936		7.49·	11.19	1.5	2.3	236.5	i	3	D.	59.6
937		.32	75.89	<u> 1:</u>	4.1	160.3	<u> </u>	3	D:	47.7
938	74 530		15.46	1.7	1.7	99.7		3	D!	66.7
939	57 742		83.76	0.7:	1: .	56.5	:	3	D:	62.5
940		2.79	6.79	0.3	4:	94.8	:	3	D:	73.5
941		75.3	72.76	18.3	0	41.2	!	3	DI	67.4
942		33.3	53.84	8.8	1.8	126.4		3	D	62.7
943		3.37	1.62	0.5	2.9	59.1		3	D	72.8
944	75 223		10.98	0.8	2.7	63.3		3	D	73.1
945	53 13	3.43	1.91	1.5	1.4	132.8		3	D	46.5
946	62 475	5.53	4.31	1.2	1.7	148.9		3	D	66.4
947	84 26	5.59	2.83	1.2	3.5	62.2		3	D	59.2
503	68;	1.08	1.14	2.9:	1.7	51.3	normal	5		26.6
504		0.73	0.69:	1.1	2.2	105.5	normal	5		14.3
505		0.94	1.29	0.7	3.1	97.8	normal	5		19.3
506		2.54	1.39	0.9	3.6	163.4	normal	5	i	18.6
510		2.07	1.38	1.1	5:	166.9	normal	5		14.6
512		0.65	0.73	0.7	1.6	82.9	normal	5		18.3
513	60	0.7	0.96:	1.4	4.1	205.4	normali	5		12.0
514		1.41	0.88	0	2	233.5	normal			11.0
517		1.47	1.13	0.7	2.5	92.5	normal			20.2
317	<u> </u>	1.4/	1.13	<b>U.1</b>	2.5	32.5	mornial.			20.2

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521	57	0.74	0.74	0	. 2.4	282	normal	5	9.4
522	65	0.58	1.21	0	1.7	113.8	normal	5	18.5
523	70	3.58	1.52	1.4	2.8	176.6	normal	5	23.9
524	41	0.65	0.97	0.7	1.4	169.7	normal	5	9.7
525	53	0.92	1.15	0.8	2.8	219.4	normal	5	10.2
527	37	0.78	1.04	0	1.1	110.6	normal	5:	11.4
528	62	0.55	0.92	1.4	5.8	126.3	normal:	5	17.0
529	42	0.56	0.95	0.7	0	110.4	normal	5	12.3
531	64	0.71	0.56	0.9	3	92.1	normal	5:	27.2
532	25	0	0.88	1	1.3	201.6	normal	5	7.0
534	41	0.63	0.83.	0.7	3.9	153	normal:	5.	10.7
535	40	0.69	0.95	1.4	3.6	207.5	normali	5	9.0
536	64	0.98	0.99	0.8	3.9	114.9	normal	5:	21.4
537	41	0.68	0.91	0.9.	2.7	166.2	normal	5	10.2
538	68	2.13	1.1	1	3.5	47.7	normal	5	34.2
539	69	1.73	0.96	1.1	2.9	40.8	normal	5:	34.8
553	48	1.39	1.18	1.1	2.5	329.4	normal:	5:	9.3
554	46	2.11	0.95	1.2	2.3	86.7		5	23.0
565	46	1.14	1.47	0	3.4	267.3.	normal	5	8.4
566	48	1.52	0.9	1	3.4	105	normal	<u> </u>	19.6
948	43	1.03	1.05	0.2		99.5	normal:	<u> </u>	14.8
949	44	0			1.2		normal	5;	
950	52	1.1	0.74	0.6	2.2	121.1	normal	5	11.3
951	54	0.69	0.69	0.5	3.5	136.8	normal	5	11.3
952:	42		1.13	0.3	2.6	176.2	normal	5	
953	51	0.8, 0.85	0.9	0.4	3.3 2	158.9 98.5	normal	5	10.9
954	43		0.52	0.8:			normal	5	14.2
955	42	0.87	0.9.	0.7	2.2 <sub>:</sub> 5.5	110.9	nomal	5	7.3
956	46	0.53 1.18	0.72	0.6 1.8	3.4	390.4 215.2	normal	5	12.9
957	42	0.81	0.89	0.7	1.9	134	normal	5	12.3
958:	47	1.39	0.58	1.7	3.2.	247.9	normal	5	12.9
959	48	0	0.34	0.4	2.5	257	normal	5	
960	54	0.65	0.34			96.2	normal	5	19.7
961	56	3.6	1.01	0.4	1.3	201.5	normal	5	22.7
962	63.	2.63	0.56	0.5	3.1	107.9	normal	5	35.0
963	50	1.4	1.03	0.8	1.6	157.5	normal	5	14.8
964	53	1.48	1.03	0.8	1.4	61.3	normal	5	25.2
965	56:	0.	0.67	0.7:	5.4	147.8	normal	51	13.6
966	43	0	0.72	0.6	2.3	167.1	normal	5	9.1
967	43	0.92	0.72	0.9	2.1	119.7	normal	5	18.3
968	50	1.18	0.43	0.8	2.1	124.8	normal	5	20.7
989	51	0.86	0.72	0.9	2.8	131.4	normal	5	16.8
970	62	1.5	0.72	1	4.2	116.3	normal	5	23.9
970	44	1.84		0.8	1.2	109	normal	5	19.3
971			0.92			332	normal	5	9.7
972	42	2	1.41	0.3	3.2	192.2		5	8.0
973	43	0	0.96	1.3	3.1	44.5	normal	5	33.1
	63!	1.64		1!	2.9	92.8	normal	5	19.7
975	48	1.05	0.77	1:	1.7		normal	5	17.0
976	48;	1.53	1.16	0.7	1.6	113.1;	normal	5	
977	40	0.72	0.98	0.4	0.5	52	normal	5	
978	35.	0.91	0.97:	0.6	0.8:	185.8	normal	5	
979	46	0.93'	0.89	0.6	2.4	180.1	normal!		11.4
980	42	1.25	1.06	0.6	2.6	175.4	normal:	5!	11.3

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	981	43	0.79	0.92	0.6	3.8	285.7	normal	5	· 7.9
	982	46	_ 1.13	1.05	1.2	1_	171.6	normal	5:	12.1
	983	61.	0.88	0.69	1	1.6	85	normal	5.	26.1
L	984	42	1.15	1.74	0.9	2.5	241.7	normal	5:	. 8.3
L	985	61	0	1.39	0.7	1.5	64.4	normal	5	17.5
	986	41	0.64	1.03	0.6	2.8	136.3	normal	5;	10.6
	987	56	0.88	0.7.	0.9	1.6	77.9	nomal	5	24.6
	988	45	1.52	1.35	0.6	2.9	152.4	normali		12.7
	989	52	0.77	0.53	0.7	0.9	127.7	normal	5	19.2
	990	53	2.45	1.14.	2.4	2.2	148	normal	5	19.5
	991	39	0.7	0.98	0.7	3.2;	191.1	normal	5	8.9
	992	51	1.1	1.06	1.2	3.5	240.9	normal	5	10.3
	993	60	1.96	0.81	0.3	1	53.3	normal	5	33.8
	994	50	0.62	1.08	0.4	2.8	146.3	normal	5	11.8
	995	51	1.11	0.56	0.4	3.6	269.1	normal	5	10.9
	996	68	0.65	1.05	0.5	3.9	196.8	normal	5!	13.8
	997	111	3.22	0.86	0.8	2.5	95.9	normal	5	17.7
	998	60	0.78	0.67	0.6	0.9	81.5	normal	5	26.0
	999	53:	0.7	0.68	0	1.6	74.9	normal	5	22.6
	000	56	1.19	0.83	0	1.6	157	normal	5	17.0
	001	47	0.73	0.92	1	2.7	120.5	normal	5	14.0
	002	48	1.03	0.92	0.5	1.8	212.6	normal	5	10.7
	003	39	0.86	0.91	0.4	0.9	181.5	normai	5	9.8
	004	61	0.8	0.36	0.5	1.9	104.6	normal	5	28.1
	005	50	0.52	0.49	0.7	1.1	106.2	normal	5	19.2
	006	39	0.97	1.27	0.6	0.6	279	normal	5	7.7
	007	49	0.51	0.74	1	1.7	106.3	normal	5	16.1
	800	62	0.72	0.69	1.1	2	113.2	normal	5	22.4
	009	41	0	0.93	0.6	0.9 <sub>i</sub>	75.6	normal	5	12.2
	010	49	0.61	1.17:	0.4	1.9	128.6	normal	5	12.2
	011	41	0.58	1.24	0.5	1.8	118.9	normal	5	10.4
	012	55	0.84	0.44	1	1.8	103.8	normal	5	24.6
	013	50	1.69	1.23	0.9	1.4!	132.2	normal	5	16.5
	014	51	2.35	0.87	0.9	1.3	111.2	normal	5	24.7
	015	49	0.53	1.19	0.8	2.3	104.6	normal	5	13.1
	)16 )17	72 53	1.03	0.94	1.2	2	87.8	normal	5	27.8
		63	1.06 3.25	1.22	0.8	1.7	87.5	normal	5	18.3 25.9
	118			0.97	0.8	2.6	173.8	normal	5	
	20	45 60	0 74	0.62	0.6	0.6	97.6	normal	5	14.1
	21		0.74	0.76	0.8	2.8	184.9	normal	5	
	22	51	1.41	0.86	0.4	0.8	111.1	normal	5	16.4 21.2
	023		0.83	0.74	0.5	0.6	82.6	normal		16.6
	224	41	1.47	0.78	0.6	1.8	120	nomai	5	25.1
	225	46	2.22	0.95	0.5	1	73.8	normal	5	16.5
<del>  "</del>	123	47	1.03	0.95	0.6	1.5	104.7	normal	5	16.9
	<u> </u>	48	1.6	0.81	0	1.2	150.6	normal	51	10.9

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									20075
PATIENT	AGE	CAL	PHOS	ETWO	PROG	TALP	TINTES	PLIVER	SCORE
	61	9.7	3.6	15	0.2	82	0	67.317	0.645
2	55	9.2	3.9	83	7.9	31	3.7	49.032	0.747
3_	33	9.4	3.6	12	0.1	39	2.8	62.821	0.819
4	43	8.5	4	4	0,3	39	2.6	50.513	0.841
5	58	9.5	3.5	40	0.1	75	0	78.267	0.660
6	48	9.6	3.8	145	7.5	49	0	59.388	0.679
7	56	8.6	3.8	43	0.1	48	0	60.833	0.698
8	36	9.4	4.1	106	6	77	0	54.156	0.819
9	32	8,5	3.6	18	0.7	52	0	51.538	0.810
10	33	9.4	3.6	65	2.4	63	4.6	70.794	0.815
11	74	9.2	4.2	13	0.2	70	0	62.571	0.619
12	41	8.8	4.1	43	0.7	70	13.1	48.000	0.890
13	28	9.1	3	84	0.3	76	7	52.763	0.802
14	44	9.1	3.3	176	0.6	82	10.3	62.805	1.011
15	62	9.1	3.4	90	0.2	32		40.625	0.693
16	36	9.6	3.8	59	0.1	39	0	66.154	0.822
17	60	8.9	3.4	129	0.1	64		78.125	0.668
18	42	9.3	3.8	35	0.8	43		39.070	0.814
19	35	9.4	3.7	58	0.2	39	0	55.128	0.828
20	47	9.1	5.2	42	1.4	50	7.6	60.200	0.762
21	46	9	4.5	95	7	52	10.4	60.192	0.886
22	37	9.3	3.4	231	0.2	60	0	84.667	0.779
23	30	9.1	4.2	5	0.2	61	11.3	52.459	0.837
24	45	9.2	3.6	63	2.3	44	5.4	64,318	0.766
25	42	9.2	3.5	139	0.4	44	0	72.045	0.773
26	61	9.8	4	22	0.3	70	- 0	49.571	0.669
27	64	8.8	4.1	17	0.2	73	5.7	65.068	0.646
28	79	10.2	3.9	13	0.1	67	0	53.731	0.602 0.791
29	33	8.5	2.9	20	0.4	39	5.2	47,949 55,893	0.770
30	41	9	2.5	120	0.8	56	0		0.721
31	50	9	3	79	0.7	49	- 0	48.367	0.729
32	46	9.5	4.1	22	0.3	58	4 0	46.034 50.172	0.716
33	51	9.2	3.2	162	0.3	58 42		65.714	0.713
34	45	- 9	3.1	44	- 12.0		0		0.755
35	45	9.3	3.8	123	12.8	66	18.3	54.848	0.965
36	32	9.3	3.8	40	0.6_	40	7.1	39,000 55,429	0.849
37	51	8.9	3.6	71	2.8	70		57,000	0.894
38	29	9.2	4	117	16.5	30	0		0.894
39	31	9.3	4	93	0.3	41	0	25.610	0.615
40	69	10	4.2	15	0.3	110	36.4	45.364 54.694	0.013
41	29_	9.2	3.9	12	0.1	147	18.1	48.000	0.770
42	67	9.3	4.7	57	0.2	65	3.9	48.000 31.091	0.827
43	42	8.8	3	57	2.5	55	3.8	63.774	0.82
44	52	9.6	3.8	118	0.6	62	8.6	39.516	0.74
45	51	10	4.4	52	0.3	<del></del>	8.0	26.444	0.78
46	46	8.8	3.6	73	3	45	<del></del>		0.78
47	46	8.9	4.4	14	0.4	64	0	62.031	1

Fig. 8

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PATIENT	AGE	CAL	PHOS	ETWO	PROG	TALP	TINTES	PLIVER	SCORE
48	45	9.1	4.5	206	0.2	84	19.6	45.357	0.843
49	81	9.3	4.2	4	0.3	66	7.4	64.848	0.594
50	32	9	2.5	25	1.4	56	0	68.929	0.763
51	52	9.5	3.8	11	0.1	49	0	66.735	0.714
52	47	8,9	4.7	15	0.2	64	7	66.563	0.744
53	60	9.2	3	18	0.2	- 101	23.8	39.604	0.622
54	47	9.5	4.5	8	0.1	72	8.2	66,389	0.702
55	46	9.5	3.5	34	10.6	67	9.8	54.925	0.767
56	57	10.1	3.9_	38	0.4	120	9.6	73.083	0.649
57	69	9,5	3.7	10	0.1	91	0	68.132	0.612
58	62	8.7	3.5	13	0.2	65	0	52.615	0.650
59	73	8.9	4	15	0.2	102	11.1	60.294	0.594
60	51	8.9	3.5	. 74	4.4	51	0	69,608	0.726
61	51	9	3,7	12	0.4	109	0	56,330	0.667
62	63	9.5	4.7	9	0.3	51	0	51.961	0.692
63	77	9.3	3.2	17	0.2	106	10.7	51.226	0.567
64	63	9.2	4.1	17	0.2	51	7.9	31.569	0.675
65	73	9.6	1.1	19	0.2	69	0_	75.217	0.576
66	83	9	3.6	2	0.1	57	0	81.404	0.581
67	59	8.8	3.7	24	0.1	85	6.9	59,294	0.648
68	60	8.9	4	110	0.3	40	0	66.500	0.706
69	76	9.4	3.5	21	0.1	54	5.8	62.593	0.604
70	59	9.2	4.6	15	0.1	_60	0	51.500	0.699_
71	63	9.2	3.4	121	0.1	48	0	140.833	0.667
72	63	9,4	3.2	65	0.1	64_	8.3	62.188	0.648
73	76	8.9	3.8	8	0	91	11.8	58.132	0.587
74	46	8.6	3.5	54	7.4	73	10.1	46.301	0.993
75	57	9.1	3.7	195	0.1	61	11.4	55.410	0.695
76	41	9.1	3.4	67	3	57	0	68,772	0.733
77	61	9.9	4.3	20	0.1	61	8.6	57.213	0.679
78	25	9.1	3.3.	122	0.6	62	0	66.935	0.821
79	51	9.2	3.1	124	7.7	79	11.1	26.835	0.704
80	57	8.9	3.9	15	0.3	84		72,500	0.662
81	76	8.8	3.1	12	0.2	88	0	86.023	0.574
82	64	9.3	3.4	131	0.1	57	4.5	55.965	0.662
83	61	9.4	3.5	22	0.5	86	9.4	60.581	0.637
84	42	9.3	3.4	150	14.9	78_	0	54.744	0.699_
85	28	8.9	3.5	177	9.6	46	0	34.348	0.867
86	26	9.4	4.1	139	0.2	52	6.9	52.500	0.878
87	73	9.3	3.5	0	0.2	72	11.5	52.361	0.604
88	37	9.3	3.1	55	2.2	77	6.4	56.623	0.756
89	72	9.2	4.3	4	0.2	111	6.3	50.811	0.603
90	69	9.2	2.8	14	0.1	125	0	75.360	0.580
91	88	9.1	3.3	19	0.2	74	0	52.027	0.554
92	76	9	3.1	13_	0.1	65	6.2	66.308	0.587
93	77	8.5	3.1	10	0.1	31	3.2	31.290	0.609
94	80	9.2	2.7	15	0.1	67	<u> </u>	72.836	0.568

Fig. 8
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PATIENT	AGE	CAL	PHOS	ETWO	PROG	TALP	TINTES	PLIVER	SCORE
95	70	8.8	4	19	0.1	102	7.1	67.353	0.603
96	52	9.7	3.3	21_	0.1	94	20.6	43.298	0.666
97	76	9.3	2.4	66	0.1	130	0	62.769	0.563
98	74	9.4	3.2	19	0.1	85	0	73.529	0.587
99	70	9.4	4	11	0.1	56	0	60.714	0.639
100	80	9.5	3.9	17	0.1	77	. 0	72.338	0.587
101	72	9.4	3.7	5	0.1	93	0	79.677	0.598
102	74	9.6	2	24	0.1	88	4.9	61.364	0.563
103	55	10.1	3.5	15	0,1	68	6	35.294	0.684
104	52	9.1	4.2	. 11	0.2	71	2.8	58.732	0.706
105	60	9.1	3.1	29	0.3	88	10.7	46.023	0.631
106	77	9.1	4	15	0.4	66	5.8	68.636	0.603
107	46	8.8	4	14	0.2	44	0	72.500	0.784
108	52	8.5	3.2	14	0.2	88	6.1	43.409	0.663
109	52	8.6	3.7	10	0.1	62	3.8	41.452	0.700
110	79	9.1	3.8	13	0.2	78	0	71.795	0.587
111	66	9.5	4.4	9	0.1	74	0	64.189	0.652
112	40	9.2	3.1	38	0.7	51	6.8	41.961	0.758
113	82	9.7	3.7	5	0.1	70	5.8	72.714	0.579
114	66	10	4.5	9	0.1	66	0	67.879	0.662
115	62	9.3	3	34	0.1	63	0	71.587	0.639
116	60	8.7	3.9	14	0.1	56	11.7	59.464	0.669
117	81	8.8	3.6	17	0.1	96	7.3	64.792	0.564
118	75	9.2	3.3	11	0.2	72	0	61.528	0.595
119	66	8.9	4.5	9	0.2	81	0	45.062	0.651
120	78	8.4	3.9	7	0.1	71	8.5	62,676	0.591
121	74	8,8	2.8	ó	0.1	62	0	62.742	0.592
122	81	8.8	3.2	10	0.1	61	6.8	28.033	0.581
123	74	10.4	3.4	11	0.2	69	0	48.551	0.609
124	82	8.8	3.4	17	0.2	79	ő	61.772	0.569
125	44	8.6	3.2	208	_ 0.3	120	0	70.417	0.728
126	69	8.5	4.5	18	0.1	78	5.9	57.179	0.634
127	75	8.7	3.8	9	0.2	69	0	66.957	0.605
129	74	9.7.4	3.8	8	0.1	80	4	72.375	0.599
130	89	8.7	2.9	32	0.2	130	0	68.615	0.525
131	77	9.5	4.2	41	0.1	74	6.8	69.054	0.606
132	72	8.9	3.5	24	0.3	58	0.8	43.621	0.620
133	69	9.2	3.1	9	0.2	94	8.4	49.468	0.597
134	71	9.2	6.3	5	0.1	70	4.6	61.571	0.646
135	68	9.2	3.6	11	0.1	84	7.0	72.857	0.616
136	85	9.2	3.9	7	0.1	71	12.6	64.366	0.571
136	43	9.2	3.8	149	0.1	46	0	68.261	0.777
		9.2	2.9	73	3.3	42	0	57.619	0.696
138	49		4.1	117	15.7	93	0	63.656	0.716
139	41	8.6				59	0	73.051	0.646
140	67	9	3.4	93	0.1		3.5	42.000	0.646
141	50	9.8	2.1	132	0.2	45			0.600
142	70	9.2	2.7	13	0.1	67	1 0	72.985	0.000

Fig. 8

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	ننيور خبر خريم	<del>,</del>			<del></del>				
PATIENT	AGE	CAL	PHOS	ETWO	PROG	TALP	TINTES	PLIVER	SCORE
143	66	9.4	3.3	14	0.1	71	0	71.690	0.625
144	52	9	3.5	53	0.3	64	3.8	35.156	0.706
145	82	8.5	3.1	15	0.1	64	0	49,063	0.572
146	64	9,6	3.6	149	0.5	47	8.7	58.936	0.675
147	65	9.1	4.6	9	0.3	78	0	41.154	0.661
148	54	9.4	4.5	16	0.2	96_	5.7	69.583	0.683
149	48	9.2	4.1	33	0.3	143	8.7	34.895	0.708
150	75	10	3.9	10	0.2	88	0	39,545	0.605
151	57	9.4	3.9	10	0.2	54_	3.4	51.111	0.692
152	47	9.4	4	42	0.3	65	8.6	51.846	0.739
153	70	8.8	3.5	6	0.1	65	_ 5	37.231	0.621
154	59	9.2	4	9	0.2	49	4.4	47.143	0.690
155	60	9.2	4.1	_12	0.1	56	2.8	60.357	0.680
156	49	9.1	3.6	59	0.2	35_	0	54.571	0.762
157	59	9.5	4.1	7	0.1	92	6.5	45,978	0.660
158	66	9.2	3.8	1	0.2	46	0	40.000	0.660
159	57	9.2	4.3	16	0.2	81	5.4	53.704	0.679
160	41	10	4.6	306	1.2	46	0	75.217	0.763
161	38	9.5	3.6	4	0.2	68	5.1	69.265	0.758
162	35	9.5	3.4	36	0.4	57	3.3	64.561	0.785

Fig. 8
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PATIENT	AGE	CAL	PHOS	етwо	PROG	TALP	TINTES	PLIVER	SCORE
123	52	9.4	4.2	-1	0.3	61	0	46	0,722
128	27	9.8	4.4	-1	0.4	58	0	43	0.862
131	39	9.1	3.9	156	11.5	44	0	59	0.820
173	26	9.5	3.8	41	0.2	98	0	60	0.790
201	30	9.1	3.5	123	3.3	90	0	53	0.814
206	39	9.2	2.6	50	1.5	74	89	42	0.729
213	46	9.7	3.4	37	0.2	90	0	36	0.708
220	46	8.8	3.4	118	4.3	90	9	63	0.996
223	49	9.7	3.3	72	0.4	78	8.6	38	0.717
234	38	9.5	3.2	186	12.6	50	0	46	0.803
243	33	9.3	4.4	65	0.3	58	0	40	0.857
244	53	9.6	3.7	96	0.3	58	0	49	0.725
245	30	9.5	3.2	-1	0.1	64	0	53	0.800
247	28	9.1	3.6	-i	0.3	58	0	50	0.821
249	22	9.3	3.5	42	0.2	98	11.1	38	0,782
253	24	9.2	3.4	-1	0.3	68	0	63	0.797
254	30	9.6	4	143	10.1	45	0	31	0.894
256	19	9.1	3.8	219	0.2	53	6.1	32	0.871
258	30	9.3	3.4	60	0.6	68	0	33	0.829
259	21	9.2	4.4	44	0.2	108	0	54	0.805
260	23	9.1	3.8	-1	0.3	62	0	61	0.818
261	23	9.4	3.4	-1	0.2	85	0	32	0.795
265	24	9.4	3.2	191	0.2	71	0 _	30	0.829
266	26	9	3.9	91	0.3	51	5.5	47	0.869
268	20	9.3	4.3	62	0.2	61	0	60	0.857
269	19	8.9	3.9	53	0.8	68	0	42	0.837
271	20	8.9	4.1	277	18.9	65	0	40	0.869
272	24	9	3.3	58	0.4	66	0	49	0.815
274	19	9.7	3.8	44	0.3	120	0 1	70	0.776
276	25	9.2	3.9	-1	0.9	65	5	27	0.837
279	21	10	4.6	115	0.5	106	0	70	0.834
280	21	9.5	4.1	202	0.9	68	0	57	0,856
281	20	9.1	3.6	-1	0.3	47	0	53	0.831
284	27	9	3.3	376	0.6	43		37	0.855
285	31	9.6	3.7	208	1.2	60	0	62	0.847
286	27	9	3.2	350	1.5	65	0	60	0.819
287	22	9	3.1	45	0.2	_66_	0	39	0.80
290	23	9.3	4.3	57	0.3	104	0	47	0.81
292	24	9.4	3.7	35	0,3	62	0	43	0.82
296	21	9.2	3.2	65	0.3	111	0	55	0.76
298	26	9.4	3.2	248	0.8	57	0	35	0.84
321	39	8.9	3.6	84	0.2	66	0	42	0.78
326	22	9.4	3.6	45	0.4	50	0	37	0.84
331	48	9.7	3.1	47	0.3	84	0	58	0.67
332	51	9.8	3.5	-1	0.3	64	0	40	0.70
333	53	9.2	3.3	166	1.2	63	- 0	56_	0.70
340	42	9.1	2.8	52	0.2	67		64	0.77

**Fig. 9**Page 1 of 8

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PATIENT	AGE	CAL	PHOS	ETWO	PROG	TALP	TINTES	PLIVER	SCORE
342	50	9.6	3.8	76	0.3	62	0	71	0.730
346 347	44	9.2	3.4	111	4.9	72	12.4	50	0.977
359	41	9.5	3.7	-1	0.2	77	0	69	0.735
360	54	9.3	3.6	95	0.2	77	0	69	0.693
364	34	9.4	3.6	62	0.4	76	0	63	0.791
365	40	10	4.2	104	0.3	62	9	57	0.811
375	46	9	3.5	97	6.7	54	0	64	0.698
382	53	9.3	3.9	75	0.2	62	0	66	0.718
386	48 24	8.7	4.8	36	0.2	63	0	66	0.796
389		9.3	3.8	-1	0.3	68	0	65	0.812
389	22	9.1	4.3		0.3	66	0	65	0.831
391	32	9.7	3.3		0.4	57	0	64	0.797
393	29	9.6	3.5	30	0.5	47	0	61	0.828
402	27	8.9	4.1	-1	0.4	45	0	56	0.848
402	38	8.7	3.5	33	0.6	43	0	46	0.786
404	49	9.2	3.4	-1	0.3	21	0	24	0.842
407	52	9.2	4.5	-1	0.1	100	0	53	0.736
407	24	9.4	3.3	152	0.4	71	0	52	0.704
408	46	9.2	3.7	132	0.6	87	0	49	0.819
412			4.1	69	7.1	52	0	58	0.698
416	52	$\frac{9.7}{0.7}$	3.6	-1	0.2	68	0	29	0.704
417	44	9.7	3.4	142	0.7	80	0	79	0.692
	49	9.5	3.4		0.2	75	0	47	0.708
418	49	10	4.2	403	1.3	88	0	75	0.678
419	26	9.3	- 3	-1	0.4	82	0	65	0.767
539	38 46	9.2	3.3	198 793	0.2	76	0	24	0.780
545	26	9.7	4.5	96	0.7	46	<u> </u>	33	0.813
549	26	9.5	3.9	50	0.3	65 46	7.2	42	0.825
560	33	8.9	3.4	118	0.4	79	7.4	61	0,862 0,791
562	23	9.4	3.2	-1 l	0.3	58	0	36	0.791
579	20	9	3.4	48	0.5	80	0	53	0.813
588	36	9.3	3.5	-1	0.1	48	0	51	0.793
591	28	9.7	3.7	36	0.1	52	0	54	0.793
593	35	9	3.7	108	0.3	69	9.6	41	0.811
597	32	9.3	3.5	-1 -1	0.3	53	9.6	71	0.801
602	49	9.3	3.6	180	4.3	69	0	46	0.693
2520	29	9.2	4.4	52	0.2	49	0	41	0.877
3000	28	9.4	3.7	49	0.4	66	0	53	0.828
3020	25	9.6	4	164	16.8	56	ő	41	0.880
100	52	8.7	3.1	371	0.3	59	ŏ	54	0.703
113	53	9.8	3.5	3	0.2	63	ŏ	67	0.690
126	42	9	4	99	16.4	83	14.4	36	0.984
130	50	9.3	3.5	336	0.6	40	0	25	0.754
139	74	8.9	3.7	209	0.4	35	5.9	36	0.648
160	60	9.5	3.9	81	0.3	47	5.2	53	0.704
176	56	9	2.9	115	0.2	64	0	58	0.677

Fig. 9
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PATIENT	AGE	CAL	PHOS	ETWO	PROG	TALP	TINTES	PLIVER	SCORE
177	39	9.4	3.1	71	0.2	82	0	45	0.751
208	42	9.1	2.4	177	15.6	54	0	70	0.757
211	50	9.5	3.1	69	0.2	77	0	60	0.696
214	25	9.2	3.7	-1	0.9	43	0	29	0.852
251	24	9.5	3.9	-1	0.1	61	0	25	0.844
273	30	9.4	3	99	0.2	156	8.3	26	0.776
299	27	9.2	3.2	41	0,2	77	0	· 58	0.788
309	35	9	3.9	55·	0.3	90	8.7	62	0.773
316	41	9.4	3.5	75	7.3	44		27	0.733
320	52	9.3	3.4	57	0.2	58	0	55	0.707
355	54	9.1	3.6	93	0.4	55	0	40	0.718
358	54	9.5	3.6	38	0.3	71	0	54	0.688
361	49	9	3.8	31	0.3	74	9.5	50	0.744
371	49	9.5	3.8	-1	0.2	72	10.3	42	0.698
377	52	9.6	3.6	120	0.2	68	0	53	0.717
385	55	9	3.3	-1	0.2	97	0	73	0.646
398	53	9.3	4.6	30	0.2	97	10.3	28	0.697
406	26	9.6	3.4	35	0.3	62	0	70	0.806
414	52	9.3	3.9	56	0.4	66_	0	72	0.710
421	31	9	3.5	72	0.3	69	0	52	0.818
536	48	9.4	3.4	54	3.2	56_	0	63	0.688
544	38	9.3	2.4	126	0.2	64	0	59	0.747
566	36	9.3	4	-1	0.5	41	0	44	0.822
603	27	8.9	4.4	42	0.3	48	0	38	0.872
109	54	9.4	3.3	64	0.3	121	9.6	65	0.652
110	58	9.4	3.9	20	0.1	85	0	58	0.663
129	45	8.8	3.7	197	10.8	56	0	53	0.733
141	46	9.7	3.6	141	2.1	68_	0	44	0.709_
158	45	8.9	3.3	243	0.8	63	0	43	0.763
164	51	9.3	3.5	139	0.5	59	0	43	0.727
170	51	9.4	3.3	120	4.2	50	0	30	0.737
178	36	9.7	3.3	139	0.4	40	0	46	0.824
180	38	8.7	3.4	48	0.4	52	0	39	0.783
181	34	8.7	3.4	78	11.1	67	6.8	33	0.817
183	44	9	3.6	131	0.2	35	0	54	0.807
191	45	9.3	3.5	1	0.4	45	0	58	0.760
194	29	9.2	3.7	89	0.1	82	0	52	0.824
200	45	9,2	3.7	226	1.6	46	0	27	0.786
204	25	9.5	3.5	170	0.3	43	0	46	0.863
209	42	9.6	2.9	539	0.4	50	0	64	0.738
216	46	9.2	3.6	156	0.5	43	0	39_	0.780
218	43	9.5	4.4	133	0,7	59_	0	41	0.791
225	37	9	2.7	159	1.4	64_	6.7	48	0.766
226	72	9.9	4.9	46	0.3	77	8.9	61	0.643
227	46	9.6	4.4	-1	0.2	94	0	38	0.757
230	43	9.3	3.4	94	0	71	0	77	0.721
231	35	8.9	3.2		0.3	51	<u> </u>	61	0,777

Fig. 9
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<del> </del>		<del></del>	T	T			771 PTC	PLIVER	SCORE
PATIENT	AGE	CAL	PHOS	ETWO	PROG	TALP	TINTES 0	23	0.709
233	50	9.1	3.5	43	0.3	73		46	1.094
238	46	8.3	3,4	234	0.2	55	5.9	63	0.758
239	40	9.5	3.6	43	1.6	71			0.738
246	34	9.8	3.3	-1	0.3	42	0	58	0.724
248	51	8.9	3.8	76	0.2	61	0	62	
255	19	9.6	4.3	49	0.3	86	0	34	0.841
257	23	8.9	2.9	118	2.7	75	0	21	
262	26	9.1	3.6	-1	0.2	47	0	24	0.844
267	23	9	3.8	170	0.4	84	0	50	0.825
270	21	9.1	3.9	47	0.9	40	0	70	0.850
277	27	9.4	4.6	58	0.2	138_	0	69	0.811
278	29	9.4	3,9	404	1.2	62	7.9	46	0.864
282	28	9.4	3.9	60	0.2	57	0	36	0.859
283	25	10	3.6	-1	0.3	48	0	32	0.847
288	24	9.7	4.1	65	0,3	107	7.2	35	0.816
289	27	9.4	3.4	68	0.6	87	0	37	0.812
291	26	9.6	3.3	-1	0.3	-58	0	28	0.823
293	26	9.6	4	32	0.2	68	0	35	0.838
295	26	9.1	3.3	57	0.5	51	0	63	0,324
310	47	9.5	3.6	306	1.5	53	0	46	0.730
314	48	9.1	2.7	-1	0.2	64	0.	53	0.704
328	37	9.4	3.2	54	0.4	74	0	55	0.762
335	47	9.2	4.2	49	0.4	74	0	56	0.745
333	37	9.3	3.3	-1	0.1	68	0	56	0.758
			3.1	151	0.1	67	8	30	0.710
349	50	8.8	4.1	374	0.2	53	0	30	0.759
353		9.7	4.3	74	0.3	48	6.8	45	0.726
354	58 50	9.1	3.3	76	0.6	93	13.8	31	0.694
363				-1	0.5	50	0	31	0.806
366	24	9.4	2.7	56	0.7	79	0	61	0.789
372	21			169	0.7	72	ő	56	0.754
378	42	9.2	3.5	56	0.1	63	o l	30	0.672
381	62	9.5	3.6		0.1	98	25.3	33	0.644
384	62	9.4	- 4	34	0.2	133	0	55	0.669
387	52	9.6	3.7		0.2	80	0	75	0.636
388	64	9.1	3.1	87	0.3	83	7.7	51	0.659
396	57	8.8	3.1	76		85	7.7	52	0.665
397	58	9.6	3.3	73	0.3	99	9.7	50	0.671
400	50	9.1	3.5	-1	0.2	44	9.7	48	0.769
410	37	9.5	2.8	-1	0.3	69	0	27	0.674
411	49	9.4	3.1	138	7.5	42	0	72	0.861
415	31	9.6	4.6	-1	0.4			35	0.662
424	54	9.4	3.1	59	0.4	101	0	65	0.002
507	45	9	3.4	46	0.3	55	+	52	0.74
513	25	9.4	3.5	52	0.2	72	1 o	61	0.65
533	61	9.6	3.9	<del>  -!</del>	0.1	80	0		0.03
535	24	9	3.3	1 -1	0.3	68		55	0.79
537	48	9.9	3.2	32	0.3	81	0	58	1 0.07

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				·					00000
PATIENT	AGE	CAL	PHOS	ETWO	PROG	TALP	TINTES	PLIVER	SCORE
540	45	9.5	2.9	391_	0.7	49	7	35	0.955
541	54	9.3	4.4	-1	0.2	68	0	37	0.714
542	32	9.2	3.4	80	0.6	51	0	60	0.829
546	62	9.3	4.5	100	0.1	45	0	59	0.711
548	52	9.2	4.1	-1	0.4	55	0	59	0.719
550	48	9.9	3.7	92	0.3	127	0	78	0.668
554	36	9.1	3.5	42	0.4	44	0	37	0.808
561	30	8.9	3	54	0.2	55	0	54	0.809
568	53	9.6	3.2	-1	0.3	49	0	40	0.699
569	26	9.2	4.5	274	0.5	80	9	30	0.870
571	45	9.1	3.3	402	- 1	72	- 0	54	0.731
572	58	9.5	3.9	52	0.2	57	7.3	23	0.700
576	65	9.5	3.3	43	0.2	78	0	56 43	0.632
580 582	50	9.3	3.2	60	0.2	76 80	7.1	24	0.696 0.967
	44	8.9	3	119	0.2	68	7.1	64	0.744
583 586		8.9	3.2	353	0.2	73	12.4	22	1.206
589	52	9.3	3.7	223	0.7	88	0	45	0.678
592			3.5	-1 95		50	0	57	0.717
595	55	9,2	3.7	128	0.3 4.5	90	8.2	35	1.000
596	46	9.5	3.6	-1 120 -1	0.2	53	0	47	0.757
604	56	9.3	4.3	-1	0.2	84	0	53	0.684
605	47	8.9	3.4	-1	1.4	64	0	40	0.740
608	46	9.7	3.8	-1	0.1	69	0	48	0.742
2500	30	9.2	3.6	70	0.2	62	10.1	42	0.842
3010	24	9.4	3.8	178	15.9	33	0	34	0.894
106	52	9.1	3.4	44	0.2	86	9	55	0.674
117	61	9.5	3.2	-i	0.1	85	0	60	0.634
121	46	9.5	2.9	48	0.3	80	0	54	0.690
133	47	9	4.2	203	15	57	7	52	0.939
151	36	9.1	3.8	-1	0.3	80	0	57	0.768
156	34	9.6	3.9	114	17.9	41	0	37	0.866
166	51	9.2	3.8	60	0.1	60	0	42	0.727
167	49	8.5	3.8	76	0.5	97	10	48	0.810
179	32	9.5	3.6	59	0.2	61	0	47	0.826
182	51	8.4	3.7	99	0.2	84	0	31	0.709
189	53	9.2	4.2	-1	0.1	68	8	47	0.705
212	37	9,4	3.7	162	18.6	55	0	57	0.818
217	67	9.4	3.2	-1	0.2	64	6.3	33	0.628
219	50	9.6	3.7	-1	0.3	81	0	18	0.707
222	56	9.1	3.9	30	0.2	102	0	61	0.657
228	51	9.4	3.5	141	0.4	61	0	28	0.730
235	41	9	4.3	96	0,3	45	0	39	0.868
252	52	9.5	3.3	34	0.2	79	0	48	0.681
264	28	9.1	3.4	-1_	0.2	50_	<u> </u>	60	0.816
275	25	9.1	2.5		0.4	38	0	34	0.806
297	23	9.4	4.4	177	12.2	72	1 0	55	0.873

Fig. 9
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DATER	4.00	1	T 22122		2200	7417		D. 1100	00000
PATIENT	AGE	CAL	PHOS	ETWO	PROG	TALP	TINTES	PLIVER	SCORE
317	47	9.6	2.4	-1	0.2	60	0	27	0.709
324	46	9.4	4	117	0.4	75	0	54	0.732
327	46	9	3.4	322	1	46	0	52	0.765
329	49	9.5	3.7	72	2.4	78	0	45	0.692
337	46	9.3	3.5	122	10,3	_48	0	42	0.700
352	56	8.8	3.6	73	0.2	53	0	35	0.707
357	35	9.4	2.9	89	2,3	71	7.6	23	0.791
367	42	9.1	3.2	58	0.5	90	9.8	64	0.846
369	62	9.6	3.6	31	0.2	86	0	39	0.645
379	42	8.6	3.4	156	6.3	84	0	61	0.742
380	49	9.6	4.2	-1	0.2	71	11	52	0.690
383	62	9	3.5	81	0.1	66	7	52	0.665
392	63	9.5	3.4		0.3	98	0	76	0.620
517	25	10	4	31	0.1	50	0	50	0.853
526	47	9.1	3.8	94	0.2	62	0	51	0.750
543	59	9.4	4.2	-1	0.2	104	0	20	0.662
553	48	8.8	4.1	35	0.5	57	0	66	0.759
556	69	9.6	4	77	0.1	44	6.8	53	0.668
567	29	9.4	4.2	-1	0.3	67	9.7	33	0.841
575	45	9.1	3.1	406	0.6	104	0	54	0.704
584	57	9.2	3.2	141	0.2	79	0	40	0.674
599	49	8.9	4	42	0.2	79	9	51	0.748
2510	26	9.5	3.9	157	16.2	56	. 0	25	0.881
105	75	9.4	4.1	42	0.4	88	8	52	0.605
116	67	8.9	4	-1	0.3	56	0	70	0.647
118	55	8.9	4.3	38	0.2	78	0	37	0.699
119	56_	9.3	4.3	75	0.3	41	0	43	0.740
127	73	9	4.1	30	0.4	54	6.5	35	0.632
134	50	9.4	3.7	486	0.4	54	0	63	0.737
136	36	9.1	3.6	167	5.7	154	0	74	0.758
140	56	9	3.9	-1	0.2	94	0	58	0.663
143	55	9.1	4	<u>-l</u>	0.2	65	0	38	0.698
145	49	9.3	3.3	67	8.9	63	0	54	0.656
147	53	9.1	3.6	75	0,2	103	4.9	78	0.670
157	52	9.2	3.5	65	0.2	70	0	62	0.701
159	57	9.4	3	-1	0.2	129	30.2	27	0.631
161	74	9.3	3,9	-1	0.1	62	0	34	0.623
162	62	9	4.1	81	0.1	54	7.2	21	0.698
163	46	9.2	2.9	128	5.7	62	0.	35	0.704
165	57	9.2	2.9	-1	0.2	108	0	39	0.629
169	59	9.5	3.9	61	0.1	64	0	34	0.693
174	40	9.5	3.2	261	4.6	85	0	22	0.764
175	39	9.1	2.3	126	3.5	90	0	36	0.726
185	78	8.7	2.9	-1	0.1	99	8.5	35	0.563
186	73	9.2	2.9	62	0,2	55	0	42	0.616
187	59	9	3.8	55	1.8	70	0	37	0.682
190	41	8.7	3	110_	11.6	60	1 0	26	0.772

Fig. 9
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PATIENT	AGE	CAL	PHOS	ETWO	PROG	TALP	TINTES	PLIVER	SCORE
192	42	9.5	4.1	46	0.4	58	0	66	0.767
195	58	9	3.4	236	0.1	61	0	40	0.688
202	67	9.4	3.2	66	0.3	59	0	61	0.641
210	60	9.6	3.2	82	0.1	49	4.7	56	0.681
215	45	9.2	3.8	135	1.8	70	0	56	0.729
221	52	9.5	4	83	0.8	60	. 0	57	0.735
224	53	8.7	3.6	110	0.2	52	0	27	0.726
229	51	9.5	4.1	33	0.3	97	0	51	0.693
237	59	9.4	4	-1	0.2	90	9.9	34	0.660
241	48	9.6	3,9	44	0.5	68	0	31	0.747
263	23	9.6	4.2	39	0.5	69	0	28	0.853
294	25	9.3	3.8	91	2.9	64	0	54	0.853
308	54	8.8	3.1	-1	0.2	40	0	48	0.692
313	53	9.8	4.3	-1	0.4	90	0	40	0.700
319	31	9	3.5	296	2.8	49	0	27	0.859
322	42	9.4	3.3	-1	0.3	63	6.6	41	0.757
323	56	8.8	3.6	38	0.1	54.	6.5	54	0.685
334	68	8.8	4.1	83	0.4	44	0	39	0.676
338	42	9.9	3.2	35	1	92	9.4	41	0.719
339	52	9.9	3.7	84	0.2	78	0	62	0.711
343	44	9.1	3.4	55	1.3	75	8	55	0.834
344	61	9.2	4.3	82	0.3	116	8.3	65	0.655
351	46	9.2	3.9	140	0.3	58	8	51	0.905
362	53	9.6	3.9	94	0.1	83	.0	72	0.703
373	62	9.9	3.4	172	0.2	83	0	66	0.654
376	70	9.9	4.7	-1	0.1	109	0	38	0.627
390	72	9	3.8	-1	0.2	108	14.5	28	0.597
395	54	9.2	4.1	-1	0.3	96	0	67	0,674
399	49	9.4	3	-1	0.4	64	0	50	0.701
401	83	8.7	3.8	31	0.2	111	0	55	0.558
413	46	9.4	3.6	90	0.1	98	25.1	54	0.746
423	44	9.2	3.6	62	0,2	47	0	45	0.785
527	38	9.3	3.3	40	0.4	62	4.1	56	0,763
552	54	9.4	3.7	-1	0.2	80	0	57	0.679
555	50	9.5	3	108	0,2	126	7.4_	50	0,670
557	59	9.4	3.5	192	0.2	42	0	66	0.697
563	44	9.5	3.8	37	0.5	46_	0	39	0.790
565	70	9	3.2	-1	0.2	54	0	45	0.623
570	24	9.2	3.5	50	0.5	53	7_	32	0.842
573	65	9.9	4,2	-1	0.3	59	0	56	0,665
574	65	9.2	3.2	122	0,3	64	0_	58	0.649
577	46	9.5	4.1	397	.04	56	0	70	0.738
585	62	9	3.5	56	0.2	77	0	21	0.658
590	65	9.2	3.7	-1	0.2	72	0	57	0.64
594	55	9.9	3.6	-1	0,2	43	0	52	0,70
601	45	8.9	3.1	81	3.4	75	6.6	54	0.85
607	81	9.7	3.5	-1	0.1	66	0_	31	0.59

Fig. 9
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PATIENT	AGE	CAL	PHOS	ETWO	PROG	TALP	TINTES	PLIVER	SCOR
111	69	9	3.3	34	0.4	68	9.3	55	0.615
124	51	9.2	3.7	35	0.2	69	0	48	0.704
149	52	9.2	3,9	-1	0.3	82	0	72	0.686
152	56	9	2.5	79.	0.2	77	0	43	0.659
168	56	9.1	4.1	-1	0.1	76	0	45	0.686
196	61	9.3	3.3	69	0.1	97	8.8	36	0.642
330	63	_ 8.9	3.8	-1	0.1	68	9.6	54	0.648
345	65	8.9	4.2	40	0.1	50	5.3	19	0.676
356	53	9.7	3.5	54	0.2	99	0	60	0.673
534	66	8.9	3.5	78	0.1	61	0	53	0.654
551	67	9.3	3.5	47	0.2	66	10	47	0.635
558	38	9.3	3.3	137	7.9	85	0	66	0.765
578	51	8.8	3.9	34	0.3	50	0	54	0.722
581	53	9.3	3.4	62	0.2	56	0	54	0.707
104	63	9.3	4.3	77	0.3	88	7.6	41	0.669
120	66	9.3	3.8	35	0.2	81	0	61	0.633
125	63	9.3	4	-1	0.4	92	ő	55	0.642
138	60	9.3	2.8	58	0.3	84	ő	77	0.634
144	68	9.5	4.6	-1	0.4	118	ő	30	0.632
146	67	9.8	3.3	-1	0.2	74	0	59	0.623
150	44	9.6	3.8	65	0.2	122	ŏ l	44	0.716
193	50	10	3.2	-1	0.3	67	ő	24	0.705
198	36	9.4	3.2	262	0.6	101	14.1	18.3	0.761
207	57	9.7	3.5	33	0.3	74	0	57	0.668
232	65	9.4	4	80	0.2	69	0	53	0.668
236	48	9	3.6	73	8.9	43	0	33	0.704
240	53	9.1	4.1	41	0.2	56	5	39	0.721
242	57	9.4	3.8	-1	0.1	71	9.8	34	0.677
315	64	9.7	3.5	46	0.1	83	11.4	37	0.639
318	49	9.8	3.2	168	3	46	0	34	0.039
325	57	9.2	4.3	-1	0.1	124	0	43	0.662
336	55	9.2	3.6	-1	0.1	76	10	28	0.676
348	58	8.7	3.5	-1	0.3	55	10	55	0.672
368	62	9.4	3.9	-1	0.2	68	0	45	0.663
370	77	9.4	4.1	-1	0.4	98	10.2	21	0.596
374	76	9.5	3.7		0.3	78	0	54	0.600
528		9.9			0.3	103			
529	80	9.1	3.9	-1	0.2	67	0	71 54	0.57
	66		3.5		0.1	96	9.4		0.634
538	79	9.4	3.9	-1				39	0.583
547	73	9.3	3.6	126	0.1	64	0	22	0.630
559	68	9.7	3.6	91	0.1	37   113	10.7	57	0.66
564	80	9.5	3.6	33	0.2			52	0.56
598	69	9.6	4.4	128	0.7	72	2.5	57	0.66
600	64	9.2	4.5		0.4	66	0	47	0.67
606	78	9.5	3.9	-1	0.1	77	0	58	0.59
									L

Fig. 9
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<u> </u>		Indication of Cilnically Significant Osteopenia (QuiOs <sup>TM</sup> > 0.730)							
Radiological Diagnosas based on DEXA scans at Hip and Spine	Having a Blochemical Indication of Clinically Significant Osteopenia (QuiOs™ ≤ 0.730)	Indication of Clinically Significant Ostsopenia							
Advanced	131	15	148						
Moderate	161	97	258						
Mild	68	160	248						
Normal	7	67	74						
Column Total	367	359	726						

Sensitivity of detecting radiologically diagnosed Advanced Ostsopenia as having a biochemical indication of clinically significant ostsopenia:

Sensitivity = 90%

Sensitivity of detecting radiologically diagnosed Advanced or Moderate Osteopenia as having a biochemical indication of clinically significant osteopenia:

Sensitivity = 72%

Specificity of identifying Normal patients as having no blochemical indication of clinically significant osteopenia:

Specificity = 91%

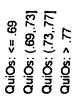
Specificity of identifying Normal or Mild Ostsopenia as having no blochemical indication of clinically significant ostsopenia:

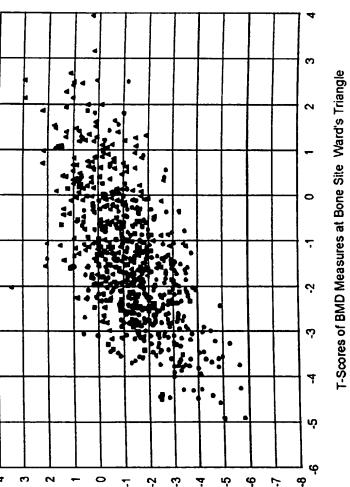
Specificity = 77%

Definition of DEXA based diagnoses of test subjects:

- \*Advanced both DEXA scans at Lateral Spine L2-4 and Ward's Triangle have T-scores ≤ -2.0;
- \*Moderate one of the DEXA scans at Lateral Spine L2-4 and Ward's Triangle has T-score ≤ 2.0, or both sites have T-scores > -2.0 and ≤ -1.0;
  - Mild one of the DEXA scans at Lateral Spine L2-4 and Ward's Triangle has T-score > -1.0 and the other has T-score ≥ -2.0, not including cases with both sites T-scores > 0.0;
  - Normal both DEXA scans at Lateral Spine L2-4 and Ward's Triangle have T-scores > 0.0.

Clinically significant osteopenia may be confirmed by finding of low bone mass (for example, at least 2 standard deviation (SDs) below the premenopsusal population mean peak).





T-Scores of BMD measures at Bone Site L2-L4

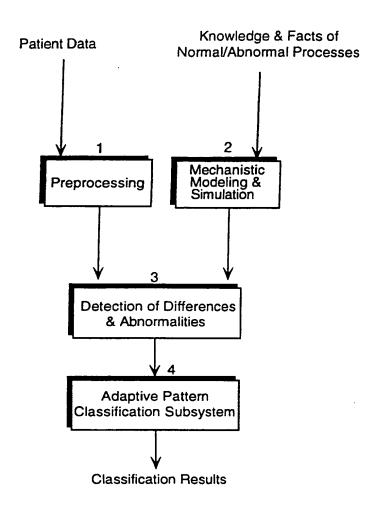


Fig. 12



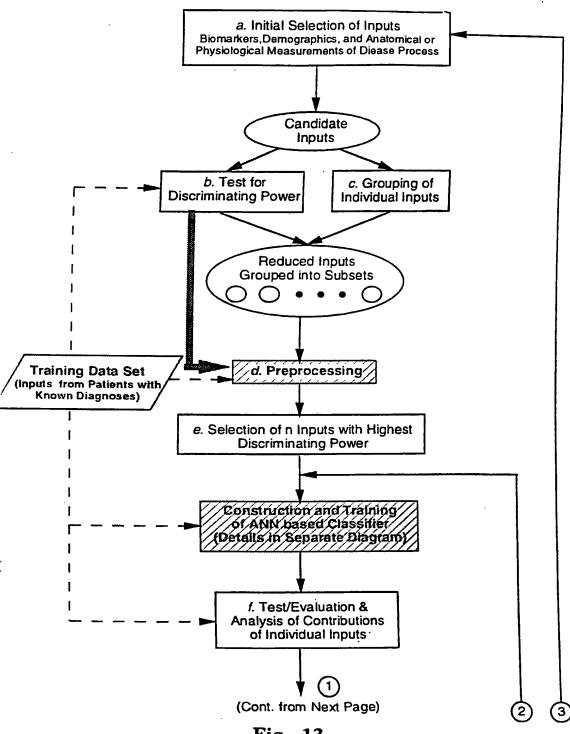


Fig. 13
Page 1 of 2

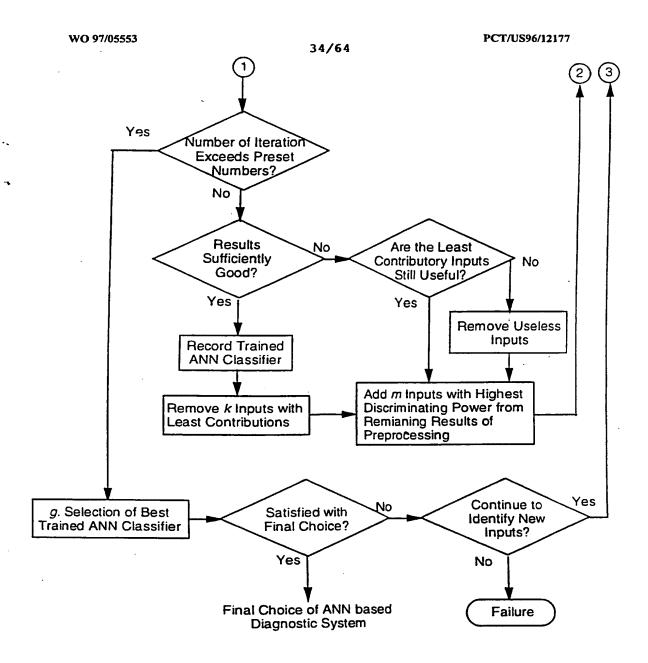


Fig. 13
Page 2 of 2

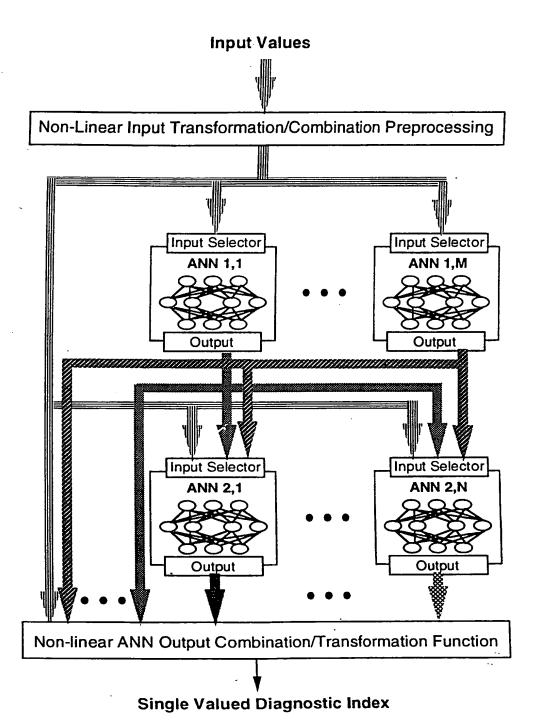
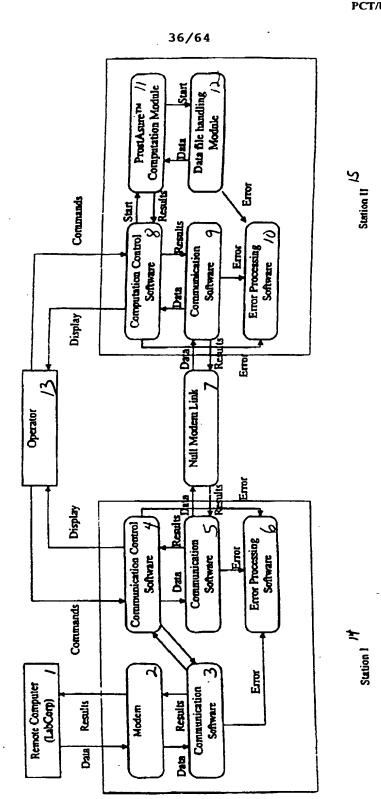
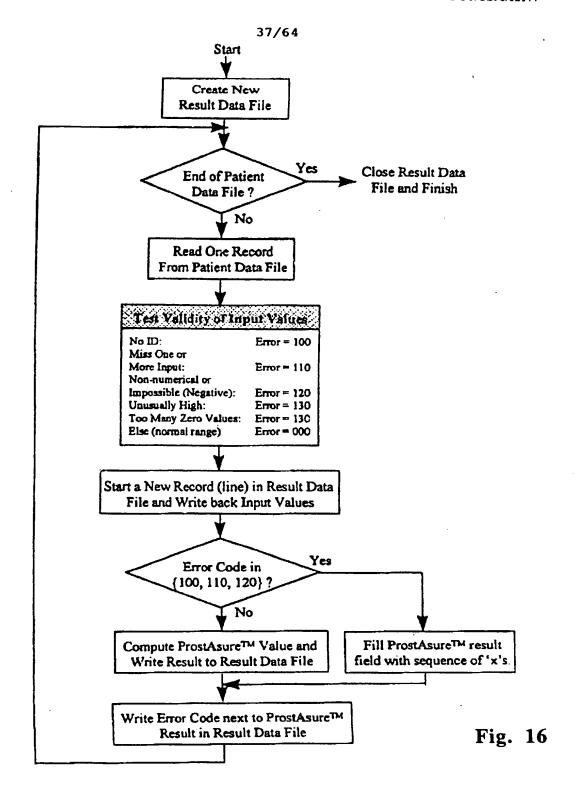


Fig. 14





-

	ProstAsure <sup>TM</sup>	ProstAsure <sup>TM</sup> Age-Specific Reference Ranges	ence Ranges
Age Groups	Normal	BPH*	Cancer
40 - 59	< 20.0	(20.0, 32.0]	> 32.0
69 - 09	≥ 10.0	(10.0, 35.0]	> 35.0
> 70	≥ 10.0	(10.0, 37.0]	> 37.0

 a BPH patient with ProstAsure<sup>TM</sup> above the mid-point of his age-specific BPH reference range is labeled as Suspicious BPH and is strongly recommended for a biopsy for a definitive diagnosis.

Presumed Normal: PSA < 4.0 and negative DRE;

Enlarged prostate by DRE (examined by Stanford Urology faculty members only);

BPH.

Cancer: Confirmed by biopsy and histologic report.

Fig. 18

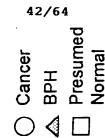
Diagnoses         Cancer         BPH         Normal         Row Totals           Cancer         155         36         2         193           BPH         16         76         23         115           Presumed Normal         0         35         73         108           Column Totals         171         147         98         416	Gold Standard		ProstAsure <sup>TM</sup>	Jretm	
155     36     2       16     76     23       0     35     73       171     147     98	Diagnoses	Cancer	ВРН	Normal	Row Totals
16     76     23       0     35     73       171     147     98	Cancer	155	36	2	193
0     35     73       171     147     98	ВРН	16	9/	23	115
171 147 98	Presumed Normal	0	35	73	108
	Column Totals	171	147	98	416

Pearson Chi-Square=314.5556 df=4 p=0.0000

Fig. 19

Confirmed		Prost	ProstAsure <sup>TM</sup>	
Cancer Stages	Cancer	ВРН	Normal	Row Totals
Stage T1b	10	16	2	28
Stage T2	80	14	0	26
Stage T3	29	5	0	82
Stage TNxM <sub>1</sub>	36	_	0	37
Column Totals	155	36	2	193

Fig. 20



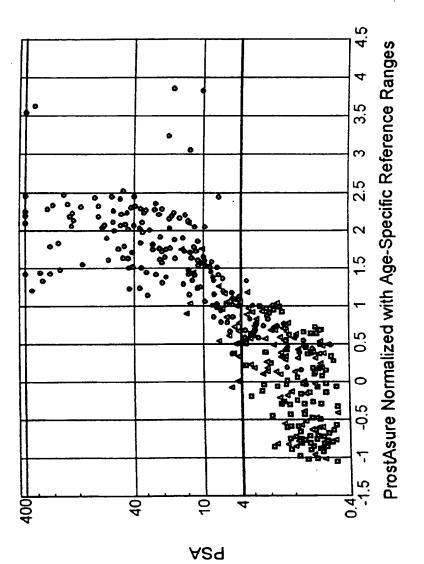


Fig. 21

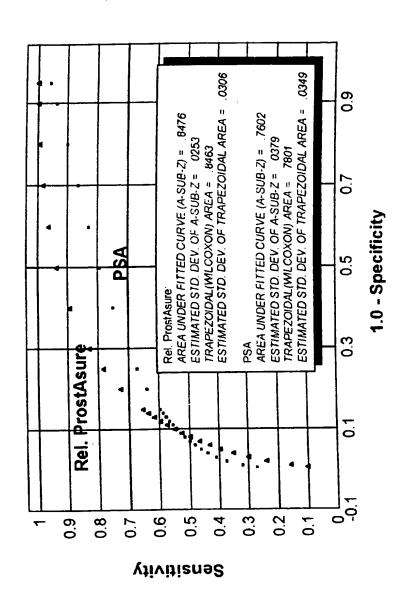
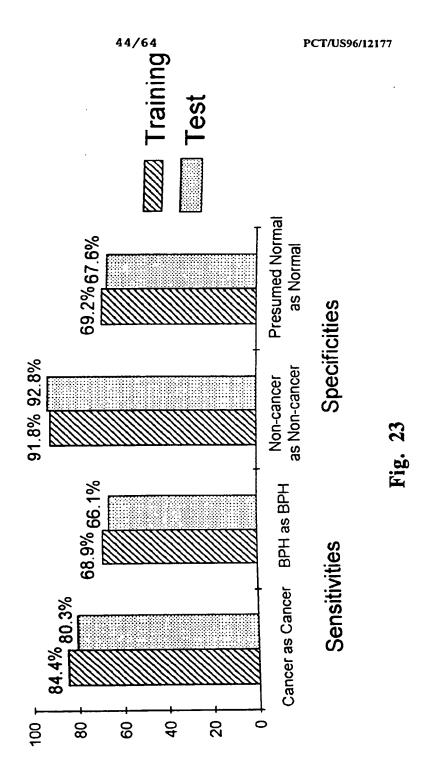


Fig. 22



WO 97/05553

Sensitivity for Detecting Prostate Cancer	80.3%
Sensitivity for Detecting Stage T2 Prostate Cancer	85.3%
Sensitivity for Detecting Stages T2, T3 and TNxM <sub>1</sub> Prostate Cancer	87.9%
Sensitivity for Detecting BPH as BPH	66.1%
Specificity for Identifying Non-Cancer as Non-Cancer	92.8%
Specificity for Identifying Presumed Normal as Normal	67.6%

Fig. 24

# MATHEMATICAL DESCRIPTION OF THE PROSTASURE™ ALGORITHM

Input variables: age, PSA, PAP, CK-BB, CK-MB, and CK-MM.

#### The Input Layer

Internal Input vector before truncation:

$$X = [age, PSA/PAP, \ln(PSA + 1), \ln(PAP + 1), CK \cdot BB, CK \cdot BB + CK \cdot MB + CK \cdot MM, x_7]^T,$$

where

$$x_7 = 1.856 - 0.023 \cdot age - 0.573 \cdot \ln(PSA + 1) + 0.0001 \cdot age^2 + 0.004 \cdot \ln(PSA + 1) \cdot age - 0.005 \cdot \ln(PSA + 1)^2$$

Truncation Threshold vectors:

$$T_{\text{lower}} = \begin{bmatrix} 20.0 & 0.0 & 0.336 & 0.0 & 0.2 & 0.0 & -0.4 \end{bmatrix}^T$$
  
 $T_{\text{upper}} = \begin{bmatrix} 80.0 & 18.0 & 2.565 & 1.253 & 2.0 & 300.0 & 1.2 \end{bmatrix}^T$ 

Then,

Fig. 25
Page 1 of 7

for i = 1, 2..., 7, let

$$y_i = \begin{cases} -1.0 & \text{if}(x_i \le T_{\text{lower,i}}) \\ 1.0 & \text{if}(x_i \ge T_{\text{upper,i}}) \\ \frac{2(x_i - T_{\text{lower,i}})}{(T_{\text{upper,i}} - T_{\text{lower,i}})} - 1.0 & \text{else} \end{cases}$$

and define

$$y_0 = 1.0$$
.

The augmented output of the first layer,

$$Y = [y_0, y_1, \dots, y_7]^T$$

will be used by both ANN No. 1 and ANN No. 2 as input to their hidden layers and jump connections.

### Calculation of Output of ANN No.1

There are two hidden layer slabs and one jump connection.

Fig. 25
Page 2 of 7

For  $i = 1, \ldots, 7$ , let

and

 $WGO = \begin{bmatrix} -0.03539 & -0.11231 & 0.19318 & -0.13088 & 0.00137 & -0.24651 & 0.50834 & -0.35074 \end{bmatrix}^{T}$ 

### Output of the Gaussian Slab of hidden layer

The two weight matrices (one leads to the slab, the other away from the slab):

			7 9 1	WC!		
-0.11272	0.03887	7.1660'0	0.19431	-0.10049	Seezu.	-0.30404
0.22494	0.15684	0.07160	-0.22778	0.12797	0.26265	0.27786
0.35798	-0.25465	-0.31651	-0.09058	-0.26480	-0.24423	-0.12895
0.06121	-0.19699	-0.10221	-0.27022	-0.22189	-0.23780	-0.07592
-0.37441	-0.33428	0.09032	0.13686	-0.09213	-0.05485	0.02998
0.13152	0.11620	-0.09873	0.01684	0.21939	0.11606	0.10233
0.05846	-0.45861	0.18685	-0.15848	0.13761	0.09825	0.25638
-0.1648	0.17490	0.36407	0.29588	0.17154	0.14387	-0.1633

and

 $s_i = \exp \left[ -\left( \sum_{j=0}^{7} WGI_{i-1,j}y_j \right) \right]$ 

The input from the Gaussian Slab to the output layer:

 $s_0 = 1.0$ .

$$t = \sum_{j=0}^{7} WGO_{j} a_{j}.$$

Fig. 25
Page 3 of 7

Output of the Jump Connection from the Input Layer

Connection weight matrix:

 $WJO = \begin{bmatrix} -0.18985 & -0.59914 & -0.21779 & -0.39691 & 0.50123 & 0.09711 & 0.75722 & 0.59222 \end{bmatrix}^T$ 

The input from this jump connection:

$$u = \sum_{j=0}^{7} W J O_j y_j.$$

# Output of the Gaussian Complement Slab of Hidden Layer

The two weight matrices (one leads to the slab, the other away from the slab):

			-			
-0.02604	-0.16674	0.00191	0.11067	0.13564	0.14143	-0.06994
-0.23948	-0.13803	0.23656	-0.01953	-0.17246	0.01008	0.28190
-0.25193	0.45174	0.12143	-0.20974	0.24953	0.18619	0.09219
-0.27160	0.23105	-0.15937	0.24071	0.14175	-0.11845	0.08302
-0.18836	-0.25352	0.20671	-0.00630	-0.23635	0.11619	0.15931
-0.24602	-0.14086	0.04799	0.18369	0.01791	0.28822	0.22994
-0.16843	0.25369	-0.11121	0.14089	0.07420	0.02910	-0.16291
0.03996	-0.19282	0.11162	-0.01729	-0.03022	0.27442	0.09244
			WCI =			

Pue

 $WCO = \begin{bmatrix} -0.12130 & -0.17390 & 0.36017 & -0.31029 & 0.02372 & 0.04508 & -0.02368 & -0.36532 \end{bmatrix}^T.$ 

F1g. 25
Page 4 of 7

For  $i = 1, \dots, 7$ , let

$$p_i = 1.0 - \exp \left[ -\left( \sum_{j=0}^{7} WCI_{i-1,j}y_j \right)^2 \right]$$

and

$$p_0 = 1.0$$
.

The input from the Gaussian Complement Slab to the output layer:

$$q = \sum_{j=0}^{7} WCO_j p_j.$$

### Output of the Output Layer of ANN No. 1

ANN 
$$\Delta t = \{1/(1.0 + \exp\{-(t + u + q)\}) - 0.1\}/0.8$$
.

$$ANN J_{output} = \begin{cases} 1.0, & ANN Jt > 1.0; \\ ANN Jt, & 0.0 \le ANN Jt \le 1.0; \\ 0.0, & ANN Jt < 0.0. \end{cases}$$

### Calculation of Output of ANN No.2

The calculations within ANN No. 2 are similar to that in ANN No. 1 except that the Weight Matrices have different entries:

Fig. 25
Page 5 of 7

			-				
-0.20041	0.19462	0.24657	0.34791	0.35697	0.08375	-0.09268	7 ] .
0.32115	0.29731	0.02840	-0.25071	-0.02234	-0.18645	0.24447	9 -0.25157
0.07470	0.23146	0.21491	0.01545	-0.14523	0.27423	0.16605	138 0.35469
0.07152	0.05455	-0.23839	0.11309	-0.02611	-0.10635	-0.30955	199 -0.24138
-0.04266	-0.26102	-0.35511	-0.34358	-0.10120	0.01659	0.07783	.23 -0.03399
-0.14134	-0.30465	-0.28497	-0.09318	-0.26887	-0.23501	0.36293	0.29840 0.24123
0.27551	0.21017	0.16655	-0.22915	0.25152	0.13650	0.01100	).06597 0.2
-0.34718	-0.02642	-0.22531	0.21253	0.08815	-0.02748	-0.12284	0.08647 0
			W.G.1 =				and W.C.O =

 $WJO = \begin{bmatrix} -0.24938 & 0.13448 & -0.32493 & -0.41677 & 0.02293 & 0.09125 & 0.26847 & 0.32690 \end{bmatrix}^T$ 

-0.01896-0.139580.10914 0.15072 0.13191 -0.056610.03812-0.18542-0.195920.18674 -0.01479-0.207300.00186 0.13730 -0.254680.273560.11302 -0.208370.22243 0.19068 -0.21388-0.217350.24318 0.27017 0.11843 -0.11641-0.04242-0.00455 -0.25874 -0.18879-0.091870.09749 0.12095 0.00660 -0.20532-0.158190.18175 -0.037410.00873 0.29272 0.15400-0.07862-0.23630-0.066630.07024 0.14126 0.069890.04568 -0.17253 0.13655-0.01853-0.01639-0.017470.27522 MCI =

 $WCO = \begin{bmatrix} 0.00056 & -0.05491 & 0.14461 & -0.26470 & -0.02535 & 0.02504 & -0.07503 & -0.24079 \end{bmatrix}^T$ 

and

Fig. 25 Page 6 of 7

Calculation of ProstAsure<sup>TM</sup> Index

 $ProstAsure^{TM} = 13.2 \cdot ln \left[ (1.0 + exp (-5.0 (ANN J_{output} - 0.5))) \cdot (1.0 + exp (-5.1 (ANN J J_{output} - 0.73))) \right]$ 

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#### MATHEMATICAL DESCRIPTION OF THE QUIOSTM ALGORITHM

The QuiOs<sup>TM</sup> software system uses four independent artificial neural network (ANN) classifiers to process information internally. The output of the four ANNs are combined to form a single value as the QuiOsTM quotient output.

Input variables: age, CAL, PHOS, ETWO, PROG, TALP, PLIVER, BONE, and weight and height,

where weight is in pounds and height in inches.

#### The Input Layer

Internal Input vector before truncation:

 $X = [age, CAL, PHOS, ETWO, PROG, TALP, PLIVER, BONE, weight/height]^T$ 

Truncation Threshold vectors:

$$T_{\text{lower}} = \begin{bmatrix} 15 & 8 & 2 & 30 & 0 & 30 & 20 & 10 & 1.5 \end{bmatrix}^T$$
  
 $T_{\text{upper}} = \begin{bmatrix} 80 & 11 & 5 & 120 & 9 & 110 & 70 & 56 & 3.2 \end{bmatrix}^T$ 

Then,

for i = 1, 2, ..., 9, let

$$y_i = \begin{cases} -1.0 & \text{if}(x_i \le T_{\text{lower},i}) \\ 1.0 & \text{if}(x_i \ge T_{\text{upper},i}) \\ \frac{2(x_i - T_{\text{lower},i})}{(T_{\text{upper},i} - T_{\text{lower},i})} - 1.0 & \text{else} \end{cases}$$

 $y_0 = 1.0$ .

and define

The augmented output of the first layer,

Fig. 26 Page 1 of 12

will be used by ANN No. 1, ANN No. 2, ANN No. 3 and ANN No. 4 as input to their hidden layers and jump connections.

 $Y = [y_0, y_1, \ldots, y_9]^T.$ 

## Calculation of Output of ANN No.1 (Def:A1)

There are two hidden layer slabs and one jump connection.

### Output of the Gaussian Slab of hidden layer

The two weight matrices (one leads to the slab, the other away from the slab):

-0.0297.17		1946	1.088	25-183	7513	3057	828.93
	•		•	•			•
-0.286049	0.241983	-0.138839	-0.135420	0.047367	0.101629	0.218254	0.139329
-0.143262	-0.118657	0.203580	-0.285991	-0.075372	-0.225876	0.107194	-0.264909
0.227745	-0.180561	0.159832	0.207400	0.288059	0.284816	0.080888	-0.063356
0.224696	0.113563	0.282687	0.251277	0.035729	-0.232591	-0.051817	-0.155416
-0.038508	-0.089029	-0.258678	0.064453	0.159887	0.158628	-0.004815	-0.116692
-0.294612	-0.068623	0.014653	0.044623	0.051242	0.046788	-0.198856	0.097780
-0.242210	-0.087058	-0.210839	-0.201171	0.292250	-0.043779	-0.237170	-0.296771
0.238712	0.145/96	-0.207428	0.214520	0.129192	-0.021639	-0.112765	-0.312350
0.303299	0.056030	-0.190152	0.188927	0.039047	0.008743	-0.061566	0.238742
			WGI =	:			

and

For  $i = 1, \ldots, 8$ , let

 $s_i = \exp \left[ -\left(\sum_{j=0}^9 W(GI_{i-1,j}y_j)^2\right] \right]$ 

 $WGO = \begin{bmatrix} 0.044272 & -0.151565 & 0.101315 & 0.101873 & 0.025073 & -0.063053 & -0.206456 & -0.190877 & -0.104936 \end{bmatrix}^T$ 

 $s_0 = 1.0$ .

and

Fig. 26 Page 2 of 12

The input from the Gaussian Slab to the output layer:

$$t = \sum_{j=0}^{8} WGO_j s_j.$$

Output of the Jump Connection from the Input Layer

Connection weight matrix:

The input from this jump connection:

$$u = \sum_{j=0}^{9} W J O_j y_j.$$

.

Output of the Gaussian Complement Slab of Hidden Layer

The two weight matrices (one leads to the slab, the other away from the slab):

_							
0.964183	-0.118589	-0.145118	-0.165069	0.157569	0.211670	0.127107	0.075936
0.067266	0.096249	-0.145056	0.177208	-0.232979	-0.268727	0.155706	-0.111904
0.934963	-0.287206	0.291491	0.057308	-0.265039	0.026983	-0.196747	0.203441
-0.132869	0.149022	0.068358	-0.198745	0.155249	0.179474	-0.054298	-0.005831
-0.067025	626090.0-	-0.100126	0.239972	-0.091285	-0.019682	-0.130268	0.346534
-0.288713	0.035317	0.045618	-0.011591	-0.222181	0.285709	0.265640	0.054032
0.027975	0.132861	0.162412	0.117841	-0.015392	-0.232763	-0.074793	0.191354
-0.191189	0.183104	-0.013370	-0.207570	0.006056	0.133303	-0.053613	-0.124375
-0.240149	0.255512	0.190381	-0.275834	0.193433	0.203858	0.031979	-0.249205
-0.018679	-0.161618	0.299513	-0.253573	0.221690	0.109032	-0.130380	-0.105436
<b></b>							
			W.C.1 =	• •			
			-	•			

and

 $WCO = \begin{bmatrix} 0.133173 & -0.128342 & -0.178770 & -0.34473 & -0.302709 & 0.119805 & 0.247879 & -0.193383 & -0.304841 \end{bmatrix}^T$ 

Fig. 26 Page 3 of 12

$$= 1, \ldots, 8, let$$

$$p_i = 1.0 - \exp \left[ -\left(\sum_{j=0}^{9} WCI_{i-1,j}y_j\right)^2 \right]$$

and

\_\_

 $p_0 = 1.0$ .

The input from the Gaussian Complement Slab to the output layer:

$$q = \sum_{j=0}^{8} W(O_j p_j).$$

### Output of the Output Layer of ANN No. 1 (Def:A1)

ANN\_It = 
$$[1/(1.0 + \exp{\{-(t+u+q)\}}) - 0.1] \cdot 0.6/0.8 + 0.7.$$

$$ANN_{-loutput} = \begin{cases} 1.3, & ANN_{-1}t > 1.3; \\ ANN_{-1}t, & 0.7 \le ANN_{-1}t \le 1.3; \\ 0.7, & ANN_{-1}t < 0.7. \end{cases}$$

## Calculation of Output of ANN No.2 (Def:P6)

The calculations within ANN No. 2 are similar to that in ANN No. 1 except that there are three hidden layer slabs and no jump connections:

### Output of the Gaussian Slab of hidden layer

The two weight matrices (one leads to the slab, the other away from the slab):

-0.214814 - 0.313690 - 0.306358 - 0.020778 - 0.023027 - 0.094503	0.031490  -0.094618  -0.083705  -0.056244  0.060931  -0.068565  0.208349	-0.149501  -0.121600  -0.201030  -0.105023  -0.208799  -0.244794  0.021268  -0.196617  -0.263198  0.019771  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196017  -0.196	0.027795 -0.093499
-0.02	-0.06	7 -0.26	
0.020778	0.060931	-0.19661	0.147091
-0.306358	-0.056244	0.021268	0.034158 0.147091
0.313690	-0.083705	-0.244794	-0.221456
-0.214814	-0.094618	-0.208799	0.232342  -0.288205  -0.158461  -0.221456
0.109730	0.031490	-0.105023	-0.288205
0.194150	0.139971	-0.201030	0.232342
4511 0.156860 0.194150	0.093666 -0.061205 0.139971	-0.121600	0.106471
-0.304511	0.093666	-0.149501	0.119571
	7.770	11	

Fig. 26 Page 4 of 12

 $WGO = \begin{bmatrix} -0.143488 & -0.114805 & -0.140507 & -0.073176 & -0.088738 \end{bmatrix}$ 

For  $i = 1, \ldots, 4$ , let

$$s_i = \exp \left[ -\left( \sum_{j=0}^9 W(jI_{i-1,j}y_j) \right)^2 \right]$$

and

 $s_0 = 1.0$ .

The input from the Gaussian Slab to the output layer:

$$l = \sum_{i=0}^{4} WGO_{i}s_{j}.$$

Output of the Gaussian Complement Slab of Hidden Layer

The two weight matrices (one leads to the slab, the other away from the slab):

			_
0.129406	-0.026505	-0.223848	-0.044218
-0.131120	0.037793	0.106783	0.143765
-0.204899		0.139959	-0.061872
0.184793	0.196205	0.188538	-0.009555
-0.151304	0.224609	0.197985	0.116539
-0.054465 -	-0.256382	0.263795	0.143128
-0.254746	0.238157	0.107662	-0.099885
0.135954	0.001408	-0.209015	0.289039
-0.140247	0.114792	0.012252	-0.376954
-0.110983	0.300111	0.132736	-0.163483
	= 1.5/11		

and

For  $i = 1, \ldots, 4$ , let

 $p_i = 1.0 - \exp \left[ -\left(\sum_{j=0}^9 WCI_{i-1,j}y_j\right)^2 \right]$ 

 $WCO = \begin{bmatrix} -0.168260 & -0.269478 & -0.054825 & -0.006776 & -0.263971 \end{bmatrix}^T$ 

 $p_0 = 1.0$ .

and

The input from the Gaussian Complement Slab to the output layer:

$$q = \sum_{j=0}^4 WCO_j p_j.$$

# Output of the Hyperbolic Tangent Slab of Hidden Layer

The two weight matrices (one leads to the slab, the other away from the slab):

0.190840	0.289061	-0.16937-1	-0.103554
0.286641 -	0.174769	-0.206334	0.036760 -0.103554
$\begin{bmatrix} 6 & -0.230415 & 0.286641 & -0.190840 \end{bmatrix}$	-0.023419	-0.089909	-0.035342
.10695	14801	0.122698	0.035409
0.246886	-0.050450	-0.096666	45 -0.191001 0.153561 -
-0.195091	0.277480	-0.148834	-0.191001
-0.152424	0.093208	-0.360955	-0.132545
0.293693	0.023314	-0.078117	0.177989  0.451628  -0.131347  -0.132545
0.016635	0.832558	0.545488	0.451628
-0.173508	0.104152	-0.101116	0.177989
	1.1.71	11	<b>,</b>

and

 $WTO = \begin{bmatrix} -0.452268 & -0.177084 & -0.942018 & -0.547621 & -0.360800 \end{bmatrix}^{T}$ 

$$p_i = \tanh\left(\sum_{j=0}^{9} WCI_{i-1,j}y_j\right)$$

and

 $p_0 = 1.0$ .

 $p = \sum_{j=0}^4 WCO_j p_j.$ The input from the Hyperbolic Tangent Slab to the output layer:

Output of the Output Layer of ANN No. 2 (Def:P6)

ANN\_2t = 
$$[1/(1.0 + \exp{\{-(t + u + q)\}}) - 0.1] \cdot 0.7/0.8 + 0.7$$
.  
**Fig. 26**

$$ANN_{-2output} = \begin{cases} 1.4, & ANN_{-2t} > 1.4; \\ ANN_{-2t}, & 0.7 \le ANN_{-2t} \le 1.4; \\ 0.7, & ANN_{-2t} < 0.7. \end{cases}$$

į

# Calculation of Output of ANN No.3 (Def:N5)

The calculations within ANN No. 3 are similar to that in ANN No. 2 except that the three hidden layer slabs each has eight neurons instead of four:

### Output of the Gaussian Slab of hidden layer

The two weight matrices (one leads to the slab, the other away from the slab):

_							_
•	-0.177731		•	•			
-0.290475	0.267778	-0.162243	-0.120797	0.046968	0.081106	0.221156	0.138115
-0.137408	-0.121494	0.203839	-0.284303	-0.069593	-0.193461	0.122095	-0.265594
0.228276	-0.153177	0.130587	0.226444	0.293456	0.273489	0.085274	-0.065739
0.227230	0.072183	0.298793	0.236341	0.027382	-0.258089	-0.060839	-0.150338
-0.046388	-0.091790	-0.220839	0.062109	0.169677	0.164094	-0.030668	-0.118489
-0.307765	-0.053571	0.013215	0.047468	0.059886	0.072129	-0.193265	0.100556
-0.243936	-0.084642	-0.212699	-0.203445	0.293139	-0.047854	-0.236940	-0.296463
0.252345	0.150768	-0.211585	0.206995	0.127987	-0.027361	-0.125573	-0.317035
-0.311499	0.078810	-0.185859	0.200236	0.047184	0.027520	-0.071331	0.242075
<u> </u>			- 15/11	1			<i>د</i>
			, E	:			

and

For  $i = 1, \ldots, 8$ , let

$$s_i = \exp \left[ -\left(\sum_{j=0}^9 WGI_{i-1,j}y_j\right)^2 \right]$$

 $s_0 = 1.0$ .

and

Fig. 26 Page 7 of 12

The input from the Gaussian Slab to the output layer:

The two weight matrices (one leads to the slab, the other away from the slab):

Output of the Gaussian Complement Slab of Hidden Layer

0.038780	-0.201101	0.129049	0.076636	0.158880	0.115886	0.242909	-0.228881
0.073614	0.297389	-0.141724	-0.177583	0.020285	0.105171	0.046325	-0.085953
0.218315	0.175038	0.069945	0.137789	0.060214	-0.062690	-0.164502	0.150861
0.008672	-0.147505	0.091588	0.071248	-0.064446	-0.031750	0.065611	0.086200
0.279037	-0.048020	0.258555	-0.338230	0.275712	-0.142208	-0.149832	0.142676
-0.172936	-0.113620	-0.206363	0.295630	0.050170	0.296799	-0.237874	0.054250
0.062804	0.035198	0.074748	-0.188968	0.013472	0.280413	0.119841	0.258346
0.021562	-0.249520	-0.036449	-0.183210	0.120204	-0.130094	-0.049205	-0.169709
-0.277972	-0.364681	0.055856	-0.292758	-0.357640	-0.014222	0.060385	0.121191
0.067068	0.167845	-0.156261	-0.168007	-0.358500	-0.243064	0.169814	0.235109
-			- 1	 !	•		

and

 $WCO = \begin{bmatrix} 0.083002 & 0.311966 & 0.332433 & 0.077694 & 0.166723 & -0.430216 & 0.069231 & 0.267888 & -0.151407 \end{bmatrix}^T$ 

$$p_i = 1.0 - \exp \left[ -\left(\sum_{j=0}^{9} WCI_{i-1,j}y_j\right)^2 \right]$$

and

For  $i = 1, \ldots, 8$ , let

 $q = \sum_{j=0}^{8} WCO_j p_j.$ The input from the Gaussian Complement Slab to the output layer:

## Output of the Hyperbolic Tangent Slab of Hidden Layer

The two weight matrices (one leads to the slab, the other away from the slab):

-0.200157	0.269297	0.051013	0.101512	0.257691	0.265290	-0.199601	-0.226321
-0.059755	0.006734	0.233317	-0.282981	0.310749	0.025718	-0.279324	0.014949
-0.130878	0.261437	-0.106213	0.133946	0.088958	-0.203203	0.160021	0.208754
0.260226	0.006474	-0.081970	-0.023025	-0.012403	0.164127	-0.127065	-0.029180
-0.084494	0.200133	-0.279220	0.011484	0.063174	-0.066137	-0.241044	0.273699
-0.081303	-0.064631	0.013150	0.104252	0.055028	0.160670	0.010181	-0.210456
0.044137	-0.159582	-0.205342	0.199160	-0.043531	-0.169181	0.009660	0.137650
-0.120407	-0.041711	-0.261471	0.282214	0.097794	-0.204849	0.226326	0.193063
-0.220642	-0.027158	0.061251	-0.217914	0.438317	-0.349119	0.166324	0.088718
0.181852	0.031246	0.288767	0.146882	-0.071505	-0.171471	0.107109	-0.003873
			14771	 			

and

For  $i = 1, \ldots, 8$ , let

and

$$p_i = \tanh\left(\sum_{j=0}^9 WCI_{i-1,j}y_j\right)$$

 $p_0 = 1.0$ .

 $p = \sum_{j=0}^{8} WCO_j p_j.$ The input from the Hyperbolic Tangent Slab to the output layer:

Output of the Output Layer of ANN No. 3 (def:N5)

ANN.3t =  $[1/(1.0 + \exp{\{-(t+u+q)\}}) - 0.1]/0.8 + 0.2$ .

 $ANN.3output = \begin{cases} 1.2, & ANN.3t > 1.2; \\ ANN.3t, & 0.2 \le ANN.3t \le 1.2; \\ 0.2, & ANN.3t < 0.2. \end{cases}$ 

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The calculations within ANN No. 4 (Def:W5) are similar to that in ANN No. 3 except that the weight matrices are different. These matrices are listed below:

Calculation of Output of ANN No.4 (Def:W5)

				•			
-0.026430	-0.189672	0.147912	-0.020266	-0.024098	0.280503	0.136861	-0.208586
		-0.154608					
-0.141339	-0.128922	0.205021	-0.285744	-0.066090	-0.208170	0.117392	-0.258460
0.226828	-0.162497	0.143333	0.213795	0.284708	0.274213	0.087271	-0.062647
0.233394	0.081330	0.296875	0.244261	0.032858	-0.252673	-0.069777	-0.153153
-0.048061	-0.106918	-0.229647	0.062354	0.164282	0.142592	-0.043574	-0.105907
-0.303867	-0.063621	0.015062	0.043847	0.056541	0.069085	-0.192264	0.098983
-0.244844	-0.087954	-0.210237	-0.202320	0.292321	-0.047488	-0.235887	-0.295168
0.297632	0.150609	-0.220458	0.210590	0.134480	-0.040319	-0.129254	-0.359633
-0.317581	0.078924	-0.194667	0.195683	0.039839	0.014776	-0.063509	0.250506
			- 1:5/11	! :			

rud

 $WGO = \begin{bmatrix} 0.058284 & -0.243129 & 0.150180 & 0.116091 & 0.030351 & -0.026612 & -0.171417 & -0.190026 & -0.175634 \end{bmatrix}$ 

						_					
0.015807	-0.212626	0.138350	0.057195	0.122110	0.111758	0.229180	-0.224271				
					0.108263						
0.216657	0.186887	0.068578	0.133413	0.073446	-0.073119	-0.167480	0.148260				
-0.005558	-0.152979	0.088367	0.068936	-0.042232	-0.034069	0.077819	0.091557				
-0.294179	-0.079907	0.260595	-0.342067	0.284020	-0.137515	-0.128281	0.141706				
-0.164530	-0.095066	-0.202998	0.280066	0.047677	0.290128	-0.237538	0.054606				
0.051869	0.025449	0.076077	-0.194276	0.009711	0.279919	0.119774	0.263776				
0.021459	-0.248818	-0.037628	-0.185023	0.132635	-0.131154	-0.038091	-0.167119				
-0.319349	-0.411242	0.067380	-0.297571	-0.424962	-0.006974	0.046483	0.125237				
0.089654	0.196057	-0.154878	-0.159035	-0.378611	-0.250513	0.146231	0.235577				
	= 124										

and

Fig. 26
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-0.188301 0.232018 0.061665 0.100589 -0.209581 0.226906 -0.216111
-0.056984 -0.002852 0.238246 -0.283984 0.322555 0.023265
-0.139769 0.278282 -0.109825 0.135741 0.072175 -0.192846 0.162878
0.256513 0.018605 -0.082866 -0.019705 -0.029228 0.182934 -0.123392
-0.087188 0.205380 -0.276603 0.007897 0.057143 -0.067412 -0.237530
-0.073055 -0.078024 0.015438 0.106940 0.064546 0.146292 0.004543
0.049680 -0.171640 -0.199921 0.198094 -0.030021 -0.181748 0.006443
-0.120221 -0.034853 -0.263217 0.283239 0.086551 -0.198701 0.229419
-0.223116 -0.072105 0.096301 -0.231894 0.510950 -0.402445 0.144808
0.185914 0.018800 0.287595 0.149936 -0.055912 -0.175119 0.100464
W777 =

and

#### Calculation of QuiOs<sup>TM</sup> Index

$$f_1 = \begin{cases} (ANN_{-1output} - 0.95)/0.09, & 0.95 \le ANN_{-1output} \ge 1.04; \\ 0.0, & ANN_{-1output} < 0.95. \end{cases}$$

$$f_2 = \begin{cases} (ANN_{-2output} - 0.85)/0.09, & 0.85 \le ANN_{-2output} \ge 0.94; \\ 0.0, & ANN_{-2output} < 0.94; \\ ANN_{-2output} < 0.94; \\ 0.0, & ANN_{-2output} < 0.85. \end{cases}$$

$$f_3 = \begin{cases} (ANN_{-3output} - 0.75)/0.1, & 0.75 \le ANN_{-3output} < 0.85; \\ 0.0, & ANN_{-3output} < 0.85; \\ 0.0, & ANN_{-3output} < 0.75. \end{cases}$$

$$f_4 = \begin{cases} (ANN_{-4output} - 0.75)/0.1, & 0.7 \le ANN_{-4output} < 0.75. \\ 0.0, & ANN_{-4output} < 0.75. \\ 0.0, & ANN_{-4output} < 0.75. \end{cases}$$

Fig. 26
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We define an additional variable  $T=\Lambda NN.3_{
m output}/\Lambda NN.4_{
m output},$  then

$$f_5 = \begin{cases} 1.0, & T < 1.0; \\ (1.24 - T)/0.24, & 1.0 \le T < 1.24; \\ 0.0, & T \ge 1.24. \end{cases}$$

$$Q_{\text{uiOs}}^{\text{TM}} = \frac{0.807413}{1.0 + \exp\left\{-1.1\left[\ln\left(1.0 + 10.0 \times \sum_{i=1}^{5} f_{i}\right) + 0.446843\right]\right\}}$$

Fig. 26
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#### INTERNATIONAL SEARCH REPORT

Internation Application No PCT/US 96/12177

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X	NEURAL NETWORKS, vol. 8, no. 2, 1995, TARRYTOWN pages 313 -319, XP000497809 BASSOE: "AUTOMATED DIAGNOSES CLINICAL NARRATIVES: A MEDICAL BASED ON COMPUTERIZED MEDICAL	FROM SYSTEM RECORDS,	1,2,4, 6-10	
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Furt	ther documents are listed in the continuation of box C.	Patent family	y members are listed in annex.	
'A' docum	ategories of cited documents:  nent defining the general state of the art which is not	or priority date a	ublished after the international filing da and not in conflict with the application nd the principle or theory underlying th	but
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